

STATE OF ALASKA
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF GEOLOGICAL AND GEOPHYSICAL SURVEYS

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Report of Investigations 91-1
RESULTS OF AN AQUIFER TEST FOR
A PROPOSED WATER SUPPLY AT
ANCHOR POINT, ALASKA

By
W.A. Petrik and J.A. Munter

STATE OF ALASKA
Department of Natural Resources
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RESULTS OF AN AQUIFER TEST FOR A PROPOSED WATER SUPPLY AT ANCHOR POINT, ALASKA

By
W.A. Petrik¹ and J.A. Munter¹

INTRODUCTION

Nine private and public water supply wells within a single plume of contamination at Anchor Point, Alaska (fig. 1) have become contaminated with fuel products during the past 9 yr (Alaska Department of Environmental Conservation, 1988). In an effort to develop an alternate water supply for local residents and businesses, eight test wells were drilled nearby. An aquifer encountered at one of these sites is under serious consideration as a possible source of water. This report presents the results of an evaluation of that aquifer for use as a public water supply.

ACKNOWLEDGMENTS

Eileen Olson and Kirsten Ballard of the Alaska Department of Environmental Conservation (DEC) and Darrell Hill of The Water Company contributed substantially to data collection during this investigation. Funding for this report was provided by DEC and Alaska Department of Natural Resources (DNR). Scott Ray of the Division of Geological and Geophysical Surveys (DGGs) reviewed this report.

PHYSICAL SETTING

The 6-in.-diam steel-cased well used for aquifer testing was drilled at the location shown in figure 2. The well was drilled to a depth of 19 ft (see app., well 4). A gravel and sand aquifer was encountered at 9 to 19 ft below land surface. On November 7, 1988, the static water level was 9.5 ft below land surface. According to the log of an earlier exploration well drilled 3.5 ft away (see app., well 1), the aquifer is underlain by silty glacial or marine deposits to a depth of at least 61 ft. A review of area well records and conversations with local residents indicates that silty deposits extend to considerable depths, that well yields from deep wells are typically low, and that the quality of water from deep wells in this area is commonly poor, with high levels of dissolved minerals.

The well site is located on a terrace deposit of the Anchor River. A gravel pit located southeast of the well site is excavated to the approximate depth of the water table in sandy and gravelly materials. A review of available boring and well logs in the area and inspection of local exposures indicate that the aquifer may be 100 or more acres in areal extent. Near the aquifer test site, however, the maximum known thickness of the terrace deposits is 20 ft, and the maximum known saturated thickness of the deposits is 10 ft. Although the terrace deposits are thicker near the Sterling Highway, ground water is contaminated with fuel products in that area (Alaska Department of Environmental Conservation, 1988).

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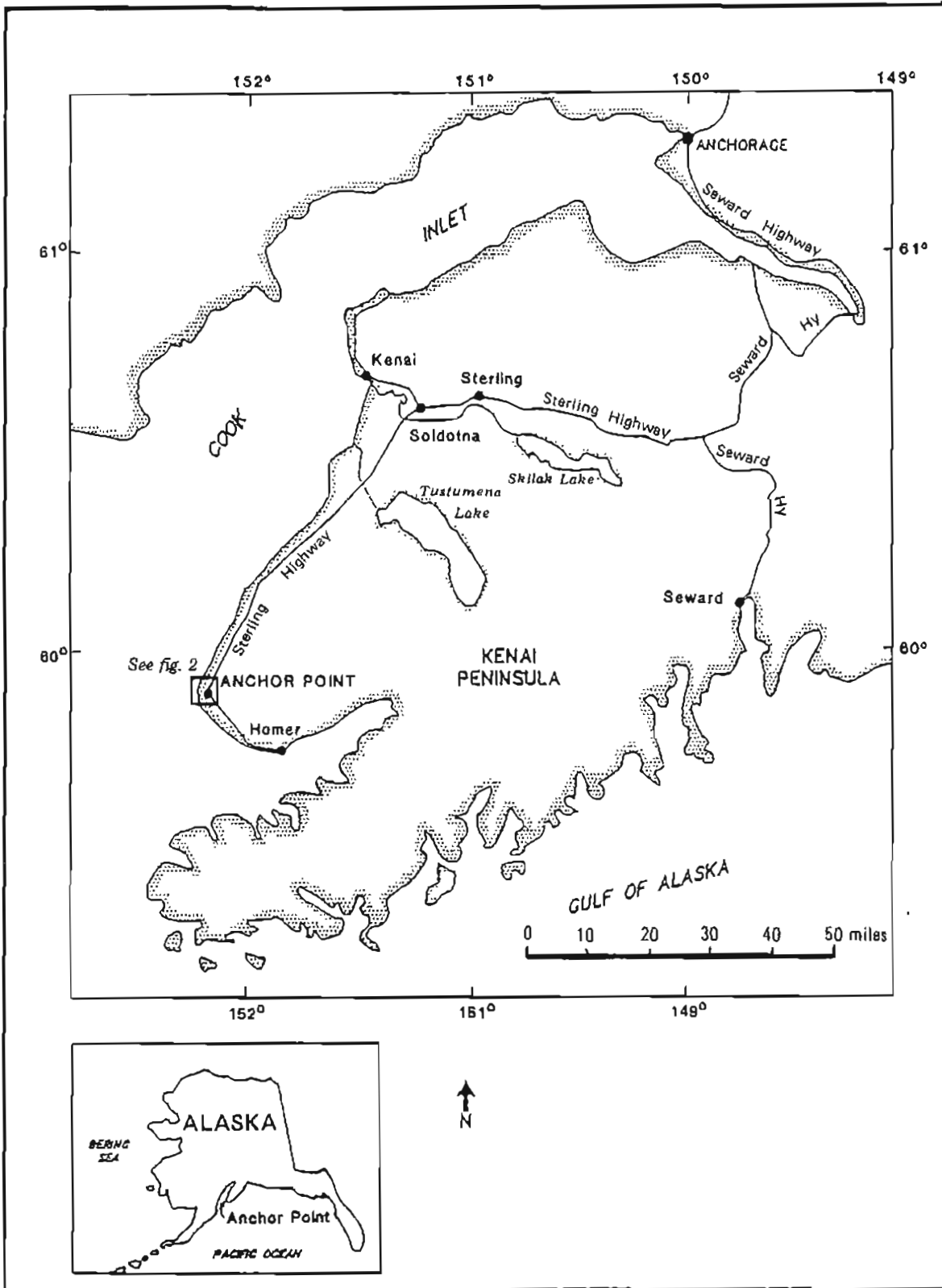


Figure 1. Map showing location of Anchor Point, Alaska. Base map modified from *Ecology and Environment* (1986).

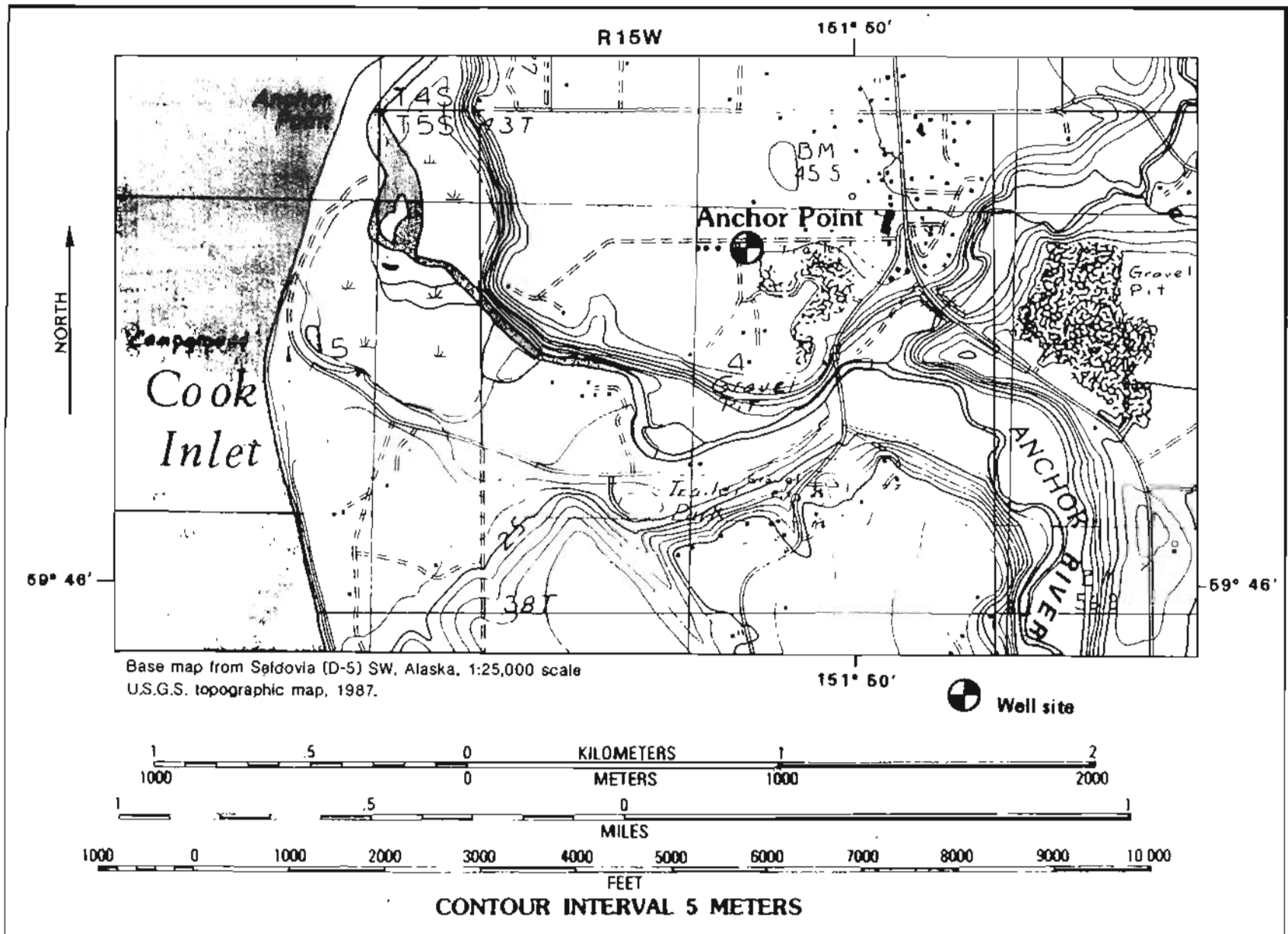


Figure 2. Location map of aquifer test well site.

AQUIFER TEST CONDITIONS AND METHODS

The production well used for the aquifer test was screened from a depth of 14 to 19 ft, with a 1 horsepower submersible pump installed at a depth of 13.6 ft below land surface (to the top of the pump). The pump was powered by an 8.8 kilowatt diesel generator. The wellhead was equipped with a pressure gage, a discharge valve, and a totalizing flow meter. Discharge was routed through a 2 in. flexible hose into a gravel pit pond located 370 ft southeast of the production well. Water levels in the production well were measured through a 3/4 in. diam perforated PVC tube extending from the wellhead to the well bottom.

Water levels were also measured in a 2 in. diam observation well located 15.4 ft south-southwest of the production well (see app., drilled 10-22-88). Water levels in both wells were measured throughout the test with dedicated two-conductor electric water level indicators and 10 ft steel tapes.

On October 28, 1988, a step drawdown test was conducted (Eileen Olson, Alaska Department of Conservation, written commun., 1988). The flow rate varied from 12 to 60 gallons per minute (gpm) with a total pumping duration of pumping of 4.4 hr.

On November 7, 1988, a constant-rate aquifer test was initiated at a flow rate of 24 gpm. Pumping continued for 64.6 hr with two interruptions totalling 16 min. Flow rates were verified with a bucket and watch. After 64.6 hr of pumping, the pump was shut down for 48 min, restarted, and run for another 191 min prior to final shutdown.

RESULTS

Figure 3 presents the results of the step drawdown test conducted on October 28, 1988. Although the maximum total drawdown during the test was only 2.1 ft in the production well and 0.85 ft in the observation well, drawdowns did not stabilize at each flow rate as normally occurs. Calculations of specific capacity ranged from 20 to 29 gpm/ft of drawdown during the test. Although the data are somewhat irregular, the well efficiency is in the range of 80 to 116 percent according to the method of Todd (1980, p. 152-159).

At the termination of the constant rate test, maximum drawdowns in the pumped well was 1.79 ft, and in the observation well, 1.17 ft. Figure 4 illustrates the trend of the drawdown data collected in the pumped well, and table 1 summarizes the results of analyses performed on data collected during the drawdown and recovery phases of the test. A particularly important feature of the data shown in figure 4 is the increasing slope of the data correlating with the increasing time of pumping. This is interpreted to be a result of aquifer boundaries encountered by the cone of depression during pumping. Transmissivity values calculated from the recovery data (table 1) were found to be somewhat lower than comparable values calculated from the drawdown data. After three days of recovery, water levels in the aquifer were 0.2 to 0.3 ft below pre-pumping water levels.

DISCUSSION

The aquifer test results show a relatively large range of transmissivity values for wells located only 15.4 ft apart. We interpret this to result from the relatively high-transmissivity deposits in the immediate vicinity of the production well, with a substantial decrease in permeability or saturated thickness (or both) in one or more radial directions from the well. The near-complete recovery of water level three days after pumping ceased indicates that the aquifer receives recharge from surrounding deposits.

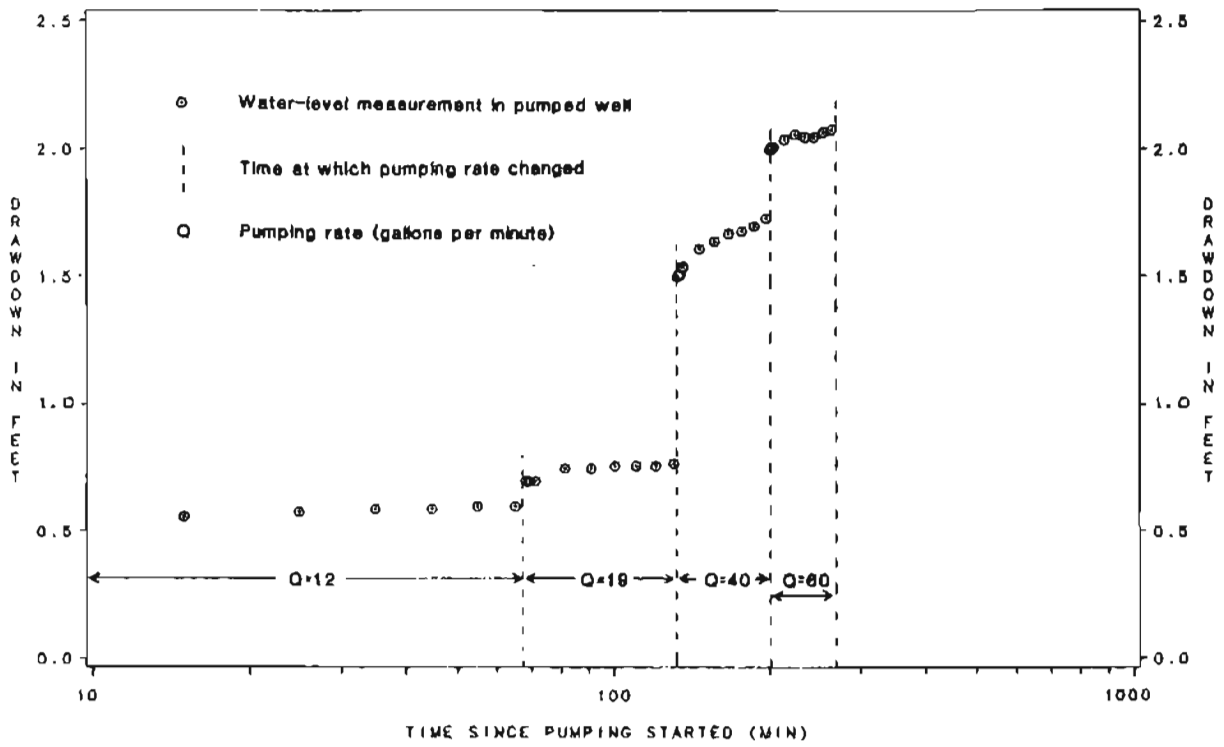


Figure 3. Plot of step-drawdown data collected at pumped well.

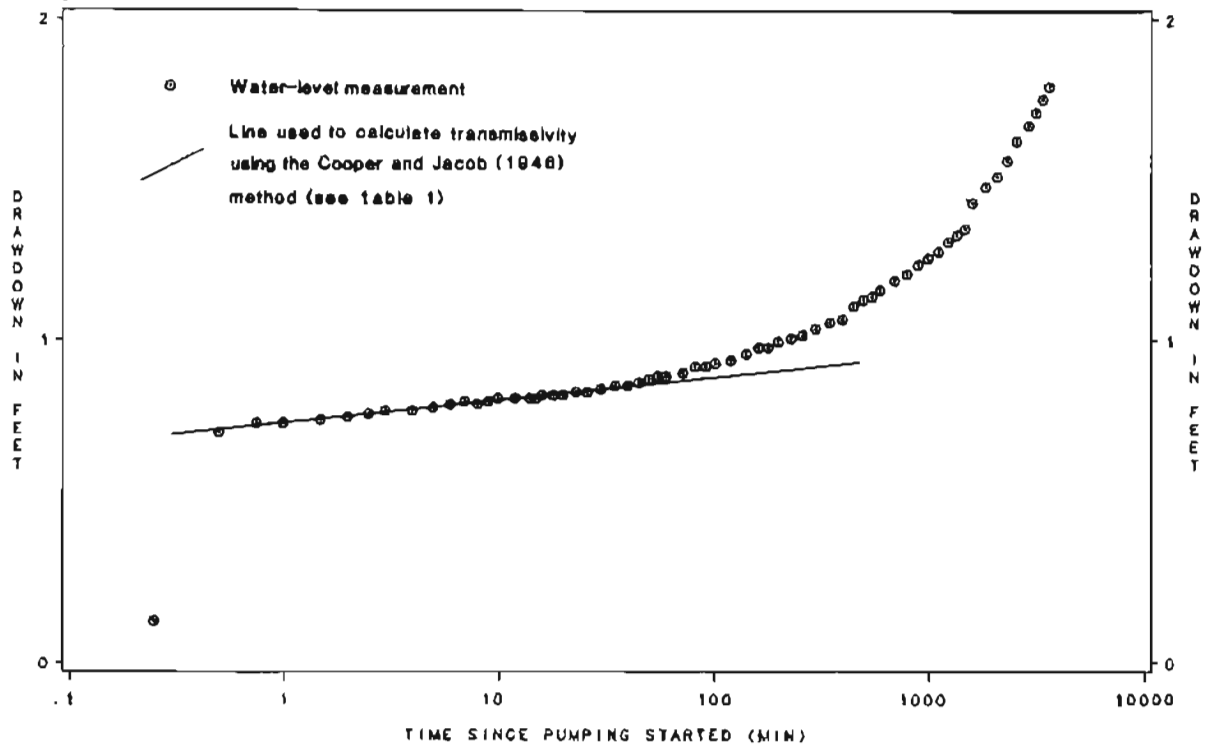


Figure 4. Plot of drawdown data collected during the constant rate test at pumped well.

Table 1. Summary of analyses of aquifer test data

Well	Type of data	Data used (t = time since pumping started/ stopped, in min)	Calculated transmissivity (ft ² /day)	Calculated specific yield	Method
Pumped	drawdown	0.5 < t < 70	11,000	-	Copper & Jacob (1946)
Observation	drawdown	5 < t < 150	5,000	0.037	Theis (1935)
Pumped	recovery	8 < t < 123	4,400	-	Calculated recovery, Johnson Division (1966)
Observation	recovery	10 < t < 150	3,400	0.025	Calculated recovery, Johnson Division (1966)

LONG-TERM PROJECTIONS

As a result of the presence of aquifer boundaries and the lack of information about their exact location, specific projections of drawdown in response to long-term pumping cannot be made. However, by extrapolating the drawdown curve as shown in figure 5, a general indication of aquifer performance is possible. By assuming an initial available drawdown of 4 ft and a continuation of the steepening drawdown trend exhibited by the late-time drawdown data, the aquifer is projected to be able to sustain a yield of 24 gpm for 11 days. Alternatively, by assuming a semi-logarithmically linear rate of drawdown (as would be expected in the absence of aquifer boundaries), a 24 gpm aquifer yield would continue for 6 months. In consideration of actual aquifer conditions, the former set of assumptions can be considered conservative, and the latter should not be considered realistic. Both scenarios assume the absence of recharge to the aquifer from precipitation or snowmelt.

Because of the shallow depth of the aquifer and the seasonal pattern of available recharge at Anchor Point, the aquifer yield may vary significantly during the year. At the time of testing, water levels in the aquifer were probably near their annual maximum. In consideration of these factors, and the previously described information about the thickness, permeability, and lateral extent of the aquifer, we suggest that an average long-term potential yield of the aquifer to be in the range of 5 to 15 gpm at the tested site. An important but unknown factor in refining estimates of potential yield is the natural fluctuation of water levels during various seasons of the year. Late winter and mid-to-late summer will likely be the seasons with lowest water levels (Brunett, 1986; Still and Brunett, 1987).

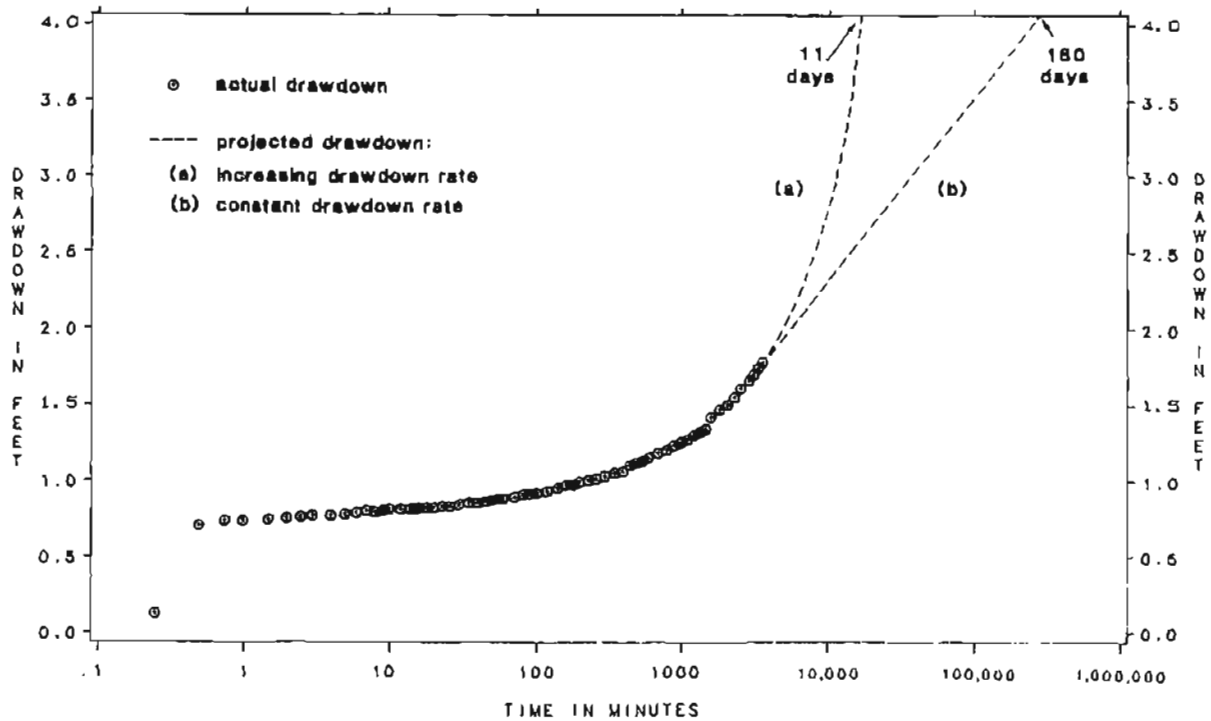


Figure 5. Projection of possible water-level responses to long-term pumping at a rate of 24 gpm. Well located at Anchor Point.

SUGGESTIONS FOR AQUIFER DEVELOPMENT

1. If feasible, water levels should be measured monthly at the pumped well or observation well through the late winter and late summer seasons. If water levels drop more than 2 ft from early November conditions, additional aquifer testing should be considered. Due to aquifer boundaries, the test should be conducted for at least a week at a constant rate in the range of 10 to 15 gpm using automatic water level recording equipment. This equipment can be installed on the observation well to monitor both pre- and post-development water levels in the aquifer.
2. Should aquifer development proceed and the existing well prove insufficient to meet demand, supplemental water could probably be developed by constructing additional wells or infiltration galleries in the area. In order to design an optimal system, further test drilling or excavation may be needed, and records would need to be maintained on water use and water levels in the aquifer. Depending on property accessibility, a shallow resistivity or seismic reflection survey may be warranted in order to identify favorable locations for additional exploratory holes.
3. Detailed information about peak short-term or seasonal water use may be critical to successful development of the aquifer. Although summertime demand may be substantially higher than year-round use, water availability, especially in early summer, may also be higher. The aquifer would be expected to respond rapidly to recharge events, minimizing concerns about long-term declining water level.

4. The aquifer may be vulnerable to contamination because of its shallow depth. An assessment of existing and future land uses and the local direction of ground-water flow in the vicinity of the well field would aid planning for ground-water protection.

SUMMARY AND CONCLUSIONS

A shallow sand and gravel aquifer at Anchor Point, Alaska, was evaluated for suitability as a public water supply. Although the aquifer yield is likely to be seasonally variable, the source may be suitable for year-round local residential and light commercial use in the range of 5 to 15 gpm (or 7,200 to 22,000 gal/day). The aquifer does not appear to be a viable long-term source of water at the tested flow rate of 24 gpm (or 35,000 gal/day). Final decisions regarding development of the aquifer should be based on current or alternate potential sources of water, development costs, natural seasonal water-level fluctuations, and contingency plans in the event that the source fails to meet demands.

REFERENCES

- Alaska Department of Environmental Conservation, 1988, Anchor Point groundwater contamination investigation, final report: Juneau, Alaska Department of Environmental Conservation, Division of Environmental Quality, 41 p.
- Brunett, J.O., 1986, Ground-water levels in Alaska, water year 1983: U.S. Geological Survey Open-file Report 86-56, 225 p.
- Cooper, H.H., Jr, and Jacob, C.E., 1946, A generalized graphical method for evaluating formation constants and summarizing well field history: Transactions American Geophysical Union, v. 27, p. 526-534.
- Ecology and Environment, Inc., 1986, Sterling Special Waste Site field investigation, Sterling, Alaska: Seattle, Prepared for U.S. Environmental Protection Agency, 59 p.
- Johnson Division, Union Oil Products Co., 1966, Ground water and wells: St. Paul, Minnesota, 440 p.
- Still, P.J., and Brunett, J.O., 1987, Ground-water levels in Alaska, water year 1984: U.S. Geological Survey Open-file Report 87-230, 308 p.
- Theis, C.V., 1935, The relation between the lowering of the piezometric surface and the rate and duration of discharge of a well using ground-water storage: Transactions American Geophysical Union, v. 16, p. 519-524.
- Todd, D.K., 1980, Groundwater Hydrology, (2nd ed.): New York, John Wiley and Sons, 535 p.

APPENDIX
Well Logs

WATER WELL DRILLING
AND PUMP SUPPLY AND REPAIR



JIM HOOVER
Owner

(907) 776-8443

P. O. BOX 1292
KENAI, ALASKA 99611

LOCATION OF WELL (Please complete either 1a, 1b or 1c.)

1a. Borough	Subdivision	Lot	Block	1b. 1/4 acre.	Section No.	Township N <input type="checkbox"/>	Range E <input type="checkbox"/>	Meridian W <input type="checkbox"/>
				— of — of — of —		S <input type="checkbox"/>	W <input type="checkbox"/>	

1c. DISTANCE AND DIRECTION FROM ROAD INTERSECTIONS

well # 1

Street Address and Area of Well Location

3. OWNER OF WELL: *Anchor Point*

Address

E. WELL LOG

Material Type	Feet Below Surface	
	Top	Bottom
<i>Top soil</i>	<i>0</i>	<i>3</i>
<i>sand</i>	<i>3</i>	<i>4</i>
<i>sand & gravel</i>	<i>4</i>	<i>10</i>
<i>gravel w/ sandstone Rock w/ traces of Brown clay</i>	<i>10</i>	<i>15</i>
<i>gravel w/ sand traces of water</i>	<i>15</i>	<i>20</i>
<i>Rock & clay</i>	<i>20</i>	<i>43</i>
<i>Blue clay & silt</i>	<i>43</i>	<i>61</i>

** Note: Abundant water present 12-20" based off as drilling progressed 2/12-1-88*

4. WELL DEPTH: (ft.) *61*

5. DATE OF COMPLETION *10-12-88*

6. Cable tool Rotary Driven Dug
 Auger Jetted Bored Other

7. USE: Domestic Public Supply Industry
 Irrigation Recharge Commercial
 Test Well Other: *monitor well*

8. CASING: Threaded Welded
diam. *6* in. to *6 1/2* in. Depth *17* ft. Weight *17* lbs./ft.
diam. _____ in. to _____ in. Depth _____ ft. Slickun *2* ft.

9. FINISH OF WELL

Type: *dry* Diameter: _____
Blot/Block Size: _____ Length: _____
Set between _____ ft. and _____ ft.
Backfilling _____ Gravel pack _____

10. STATIC WATER LEVEL: _____ ft. *1/1*
 Above or Below land surface Date _____
Equipment used: _____

11. PUMPING LEVEL below land surface and YIELD
_____ ft. after _____ hrs. pumping _____ g.p.m.
_____ ft. after _____ hrs. pumping _____ g.p.m.

12. GROUTING Well Grouted: Yes No
Material: Neat Cement Other: *Bitarite*

13. PUMP: (If available) HP _____
Length of Drop Pipe _____ ft. capacity _____ g.p.m.
 Subm. Jet Centrifugal Other

14. REMARKS: *installed locking cap*

15. WATER WELL CONTRACTOR'S CERTIFICATION:

15. Water Temperature _____ ° F C

This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.

Northland Drilling
Registered Business Name

AA4201
Contract License Number

Address: *PO Box 1292 Kenai AK 99611*

and: *James Hoover* Date: *10-21-88*
Authorized Representative

11-22-88

OBSERVATION WELL DRILLED 10-20-88

(AS PER PHONE CONVERSATION W/ HART-CROWSER'S STEVE ROG- ON 11-22-88) by Eileen Olson, DEC

2" PVC 0'-20'
SLOTTED 5'-20' INTERVAL : .020 SLOTS, 20 SLOTS / FT
FLUSH THREADED PVC
SAND PACKED W/ # 16 SILICA SAND
4' BURIED 6" CASING W/ VOLCLAY SURFACE SEAL 0'-4'

0-1.5 SURFACE ORGANIC LAYER & GRASS

1.5-5 TAN SILT, MOIST, SOFT

5-6.5 BROWN SAND (SP-SM)
MOIST, MED. DENSE
(GRAVELLY DRILLING FROM 6.5)
(LOBBLES @ 9.5' & 10.0')

WATER TABLE
= WD @ 9.5'

6.5-15.5 BROWN GRAVELLY SAND (SP)
WET

15.5-20 BROWN SANDY GRAVEL
WET, DENSE

(EASY DRILLING AFTER 18') → H-C'S S. ROG SAYS PROBABLY BECOMING SILTY

20-21 GRAY SANDY SILT OR SILTY SAND
SATURATED, MEDIUM STIFF, TRACE CLAY

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²Section chief.

