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# ALASKAN IC FUSIBILITY OF ASH OF UNITED STATES COALS

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# FUSIBILITY OF ASH OF UNITED STATES COALS<sup>1/</sup>

by

Roy F. Abernethy<sup>2/</sup> and Elsie M. Cochrane<sup>3/</sup>

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## INTRODUCTION

Laboratory determination of the fusibility of coal ash provides considerable information for the combustion engineer engaged in pulverized-coal firing and using underfeed and spreader stokers and hand-fired small industrial and domestic stokers. This information, and that obtained by trial tests, provides the essentials for procuring the best fuel for the particular installation. The continued increase in efficiently utilizing energy in coal has caused an increasing interest in the behavior of the ash or residue during combustion. This interest is shown not only in the larger electric generating plants but also in the domestic stokers, particularly the automatic types. Because there is considerable range in the fusibility of ash and there are various methods of combustion, it is not feasible to establish one set of specifications for coal based upon fusibility alone. The chemical and physical characteristics of the coal also must be considered for the best performance.

An earlier publication<sup>4/</sup> gave only the softening temperatures for mine samples and did not give the initial and fluid temperatures; therefore the fusibility intervals could not be determined. The intervals between the initial, softening, and fluid temperatures are, in many instances, more informative than the temperature at a deformation stage.

This publication includes all information on fusibility of coal-ash determinations of coal tested from 1921 to 1957. These data are, for the greater part, from tipple samples; the preceding publication contained information almost exclusively on mine samples. The data in this publication are of more

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<sup>4/</sup> Selvig, W. A., and Fieldner, A. C., Fusibility of Ash From Coals in the United States: Bureau of Mines Bull. 209, 1922, 119 pp.

practical value because the tipple samples<sup>5/</sup> represent the coal as used; whereas the mine samples<sup>6/</sup> were selected so that the coal was free of visual impurities.

This information should assist the consumer when procuring and utilizing coal.

#### COAL ASH AND ITS ORIGIN

By definition,<sup>7/</sup> coal ash is "inorganic residue remaining after ignition of combustible substances, determined by definite, prescribed methods."<sup>8/</sup> The ash may not be the same in composition or quantity as the mineral matter in the coal.

The temperature employed in ignition of the combustible matter is high enough to decompose minerals such as carbonates, sulfides (pyrite), shales, and clay.

Mineral matter in coal is the composite product of (1) the mineral matter as a constituent of the vegetal matter from which the coal was formed, (2) substances absorbed by the carbonaceous material from percolating water or crystallized therefrom, (3) clays and minerals deposited simultaneously with the vegetal matter, and (4) adventitious contaminants from roof and floor during mining.

Compounds of silicon, aluminum, iron, calcium, and magnesium are the principal constituents, with lesser amounts of titanium, sodium, potassium, and sulfur. In certain areas minerals containing various other elements are found from trace amounts to quantities large enough for economic commercial recovery.

#### METHOD OF ANALYSIS

Determination of the fusibility of ash is empirical; and factors such as rate of heating, atmosphere, and particle size of ash in test piece affect the results. Development of the method of analysis used to obtain the data in this report has been published.<sup>9/</sup>

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- <sup>5/</sup> Snyder, N. H., and Aresco, S. J., Coal Sampling (Revision of Tech. Paper 133): Bureau of Mines Handbook, 1957, 16 pp.
- <sup>6/</sup> Holmes, J. A., The Sampling of Coal in the Mine: Bureau of Mines Tech. Paper 1, 1918 (rev.), 22 pp.
- <sup>7/</sup> American Society for Testing Materials, Standard Definitions of Terms Relating to Coal and Coke (Designation D 121-30): ASTM Standards, 1954, p. 108.
- <sup>8/</sup> Fieldner, A. C., and Selvig, W. A., Methods of Analyzing Coal and Coke: Bureau of Mines Bull. 492, 1951, 51 pp.
- <sup>9/</sup> Fieldner, A. C., Hall, A. E., and Field, A. L., The Fusibility of Coal Ash and the Determination of the Softening Temperature: Bureau of Mines Bull. 129, 1918, 146 pp.

A detailed description of the method used to obtain the data in table 3 also has been published.<sup>10/</sup>

Coal ash ground to pass through a 74-micron (No. 200) sieve is molded into 3/4-inch-high triangular pyramids, referred to as cones. The side of the equilateral base is one-fourth inch. These cones are mounted vertically in a refractory base and heated in a natural gas-fired furnace at a rate between 5° and 10° C. per minute. The gas and air are adjusted to give the specified heating rate and also provide the required mildly reducing atmosphere around the cones. An optical pyrometer of the disappearing filament type was used in making the temperature measurements.

#### FUSIBILITY OF ASH

The fusibility of ash should not be confused with such terms as "fusion," "softening," and "melting" points. It includes a temperature range and deformation record of a specially designed and prepared cone of the ash heated under specified conditions.

The fusibility of ash includes:

1. Initial Deformation Temperature. - The temperature at which the first rounding or bending of the apex of the cone occurs.
2. Softening Temperature. - The temperature at which the cone has fused down to a spherical lump.
3. Fluid Temperature. - The temperature at which the cone has spread out over the base in a flattened layer.

Temperatures at which the above deformations occur are used to compute three temperature intervals — the difference between condition 1 and 2, 1 and 3, and 2 and 3. These temperature intervals are used to estimate roughly the flow properties of the ash. For instance, if the temperature interval or fusibility range between the initial and fluid temperature is 40° to 50° F., the ash acts as a compound; but if this fusibility range is 300° to 500° F., the ash behaves as a mixture of compounds, one acting as a fluxing agent for a more refractory component.

Considerable information on the industrial application of the fusibility of the ash has been summarized.<sup>11/</sup>

The average softening temperatures, ranges of softening temperatures, and fusibility ranges (temperature interval between the initial and fluid temperatures) by beds and States are given in table 1.

<sup>10/</sup> Work cited in footnote 8.

<sup>11/</sup> National Research Council, Chemistry of Coal Utilization: John Wiley & Sons, vol. 1, 1945, pp. 496-571.

## SOFTENING TEMPERATURE BY CLASS

In a previous publication<sup>12/</sup> the softening temperature of coal ash from coals of the United States had been arbitrarily divided into three classes:

Class I. - Softening above 2,600° F.

Class II. - Softening between 2,200° and 2,600° F.

Class III. - Softening below 2,200° F.

The softening temperatures in table 2 have been classified by the foregoing scheme according to beds and States.

## SOURCE OF INFORMATION

The analyses tabulated in this paper were made in the Analysis Section, Bureau of Mines, Pittsburgh, Pa., and represent those made from June 1, 1921, to June 30, 1957. All analyses were reviewed for this report, and those used represent the sizes of the coals produced. If the analytical results of repeated samplings from a mine agreed, only the latest analyses were given; if results of samplings varied, all analyses were given to show the range that could be expected.

Bureau of Mines engineers collected the tipple samples and obtained from mine officials pertinent information, such as mine name, bed, location, and preparation of the coal. Mine samples were collected by engineers and geologists of the respective States and of the Federal Geological Survey and Bureau of Mines.

These data, collected over a period of 36 years, may include some duplications due to changes in the name of the mine. The values reported are correct for the samples analyzed but do not necessarily represent the average for the mine or present-day production.

## EXPLANATION OF TABLE 3

Column 1 lists alphabetically the State, county, town, and mine. The names of the coalbeds in column 2 are those accepted by the several State geologists. In some districts a local bed name may be used and therefore may be improperly correlated. The letters M and T in column 3 indicate mine and tipple samples, respectively. The size and preparation of each sample are shown in column 4. When more than one mine sample from the same mine was tested, the results were averaged. Columns 6, 7, and 8 give the initial, softening, and fluid temperatures, respectively.

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<sup>12/</sup> Work cited in footnote 4, p. 1.

TABLE 2. - Percentage distribution of softening temperatures by class (Con.)

Region and state	Class			Number of samples
	1	2	3	
	More than 2600 °F.	2200 to 2600 °F.	Less than 2200 °F.	
1	2	3	4	5
COAST				
Oregon	-	40	60	10
Washington	32	65	3	182
Region average Number of analyses for region	30	64	6	192
ALASKAN				
Alaska	40	51	9	70
Region average Number of analyses for region	40	51	9	70
Average for United States	26	44	30	
Number of analyses in report				13,110

S-106 O-60-3

do.	do.	M	5	2,770	2,820	2,910+	13.1	.8	C52300 to C52304	
Busby	America	T		2,780	2,890	2,910+	12.1	1.6	D73524	
do.	do.	T		2,100	2,620	2,840	9.3	1.8	D73525	
Lost Creek No. 1	do.	T		Run-of-mine	2,540	2,810	18.2	2.0	E55356	
New America	do.	T		3- by 1-1/2-inch (W)	2,680	2,730	2,840	11.0	1.6	C34827
do.	do.	T		1-1/2-inch by 0 (W)	2,680	2,730	2,840	12.2	1.6	C34828
Paynes Bend										
Paynes Bend No. 1	Pratt	M	5	2,450	2,530	2,600	6.9	1.5	87206 to 87210	
Prospect										
Mammoth	Mary Lee	T		7- by 2-inch	2,910+	-	13.2	.7	D71233	
do.	do.	T		5-inch by 0	2,890	2,910+	13.4	.8	D71234	
do.	do.	T		4-inch by 0	2,710	2,860	2,910+	11.9	.7	D84805
do.	do.	T		7- by 2-inch	2,710	2,860	2,910+	12.2	.7	D84806
do.	do.	T		do.	2,740	2,860	2,910+	12.4	.6	D85376
do.	do.	T		4-inch by 0 (W)	2,680	2,840	2,910+	12.1	.6	D85377
Sipsey										
Sipsey	Black Creek	M	4	2,200	2,470	2,600	3.6	.9	A57572 to A57575	
Summiton										
Drummond Hollow No. 4	do.	T		3-1/2-inch lump	2,680	2,760	2,890	1.6	.6	D47818
do.	do.	T		3-1/2- by 1-1/4-inch	2,800	2,910+	-	1.7	.6	D47819
do.	do.	T		1-1/4- by 1/2-inch (W)	2,750	2,800	2,890	2.9	.6	D47820
do.	do.	T		1/2-inch by 0	2,620	2,780	2,860	9.8	.7	D47821
Prospect	Jefferson	M	1	2,110	2,200	2,510	4.5	2.4	B94219	
Summiton	Black Creek	T		5-inch lump	2,210	2,380	2,640	1.8	.7	D47483
do.	do.	T		5- by 3-inch	2,450	2,570	2,680	3.6	.7	D47484
do.	do.	T		3- by 1-1/2-inch (W)	2,230	2,420	2,570	1.8	.6	D47485
do.	do.	T		1-1/2-inch by 0 (W)	2,260	2,540	2,680	2.7	.7	D47486
Summit		M	5	2,220	2,430	2,610	2.5	.7	A85876 to A85880	
do.	do.	T		3-inch lump	2,220	2,370	2,620	1.8	.7	A85882
do.	do.	T		3- by 1-1/2-inch (W)	2,350	2,490	2,730	1.7	.6	A85883
do.	do.	T		1-1/2-inch by 0 (W)	2,230	2,480	2,620	2.5	.7	A85884
Townley										
Galloway No. 15	Jagger	M	4	2,280	2,580	2,630	15.2	1.7	80119 to 80122	
Townley	do.	T		5-inch lump	2,350	2,540	2,770	9.7	1.0	B17575
do.	do.	T		5- by 4-1/2-inch	2,390	2,580	2,790	11.4	1.3	B17576
do.	do.	T		4-1/2-inch by 0 (W)	2,590	2,700	2,810	12.5	1.3	B17577
do.	Mary Lee	T		4- by 1-1/2-inch	2,780	2,890	2,910+	12.7	.7	D40050
do.	do.	T		1-1/2-inch by 0 (W)	2,730	2,860	2,910+	12.3	.8	D40051
do.	Corona	T		4- by 1-1/2-inch	2,150	2,180	2,520	8.5	3.9	D44148
do.	do.	T		1-1/2-inch by 0 (W)	2,000	2,150	2,470	9.3	3.8	D44149
Townley No. 1	Jagger	M	5	2,260	2,410	2,540	14.3	1.5	A21139 to A21143	

ALASKA

Northern Alaska Region									
Ikpikuk River									
Outcrop	-	M	2	2,380	2,510	2,640	13.9	.5	A6847 and A6849
Kiana	-	M	1	2,360	2,560	2,830	20.5	.5	A52083
Kilik River	-	M	1	2,290	2,340	2,360	14.1	.3	A6848
Outcrop	-	M	3	2,340	2,420	2,670	4.9	.1	C61130 to C61132
Kukpowruk	-	M	2	2,140	2,210	2,420	4.6	.7	C27944 and C27945
Outcrop	-	M							
Meade River	-	M							
Meade River Prospect	-	M							

L/ M, mine sample; T, tipple sample. 2/ W, washed.



TABLE 3. - Fusibility of ash of United States Coals (Con.)

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State, county, town, and mine	Bed	Kind of sample <sup>1/</sup>	Size of coal <sup>2/</sup>	Number of samples averaged	Fusibility of Ash			Percent, dry basis		Laboratory No.
					Initial deformation temperature, ° F.	Softening temperature, ° F.	Fluid temperature, ° F.	Ash	Sulfur	
1	2	3	4	5	6	7	8	9	10	11
ALASKA (Con.)										
<u>Northern Alaska Region (Con.)</u>										
Peard Bay	-	M		1	2,460	2,570	2,850	12.0	.4	C27946
Peard Bay Outcrop	-	M		1	2,470	2,570	2,840	7.7	.7	C27948
Prospect Kugrua Inlet	-	M		1	2,300	2,430	2,470	3.1	.4	C61139
Point Lay	-	M		1	2,300	2,430	2,470	3.1	.4	C61139
Prospect Tepsako River	-	M		1	2,300	2,430	2,470	3.1	.4	C61139
Wainwright	-	M		1	2,300	2,430	2,470	3.1	.4	C61139
Kuk River No. 1	-	T	Run-of-mine	1	2,050	2,140	2,810	2.7	.3	C61137
Kuk River No. 2	-	M		2	2,450	2,570	2,780	2.9	.4	C61133 and C61134
Kuk River No. 3	-	M		1	2,080	2,200	2,650	3.1	.3	C61135
Kuk River Outcrop	- (Bottom)	M		1	2,150	2,190	2,290	3.7	.4	C27947
Do.	- (Top)	M		1	2,230	2,590	2,670	4.4	.5	C27949
Jarvis Creek Field										
Gerstle River District										
Outcrop S.E. of Donnelly	A	M		1	2,580	2,660	2,710	13.0	.3	C71481
<u>Yukon Region</u>										
Broad Pass Field										
Broad Pass										
Prospect	-	M		2	2,320	2,370	2,560	19.7	.3	D94465 and D94466
Colorado Station	-	T	Run-of-mine	1	2,800	2,860	2,910+	17.6	.5	D93273
Colorado Station	-	M		2	2,430	2,470	2,660	9.3	.7	C1804 and C1806
Costello Creek	Dunkle	M		1	2,020	2,090	2,480	7.6	.6	C1805
Do.	Stevens	M		1	2,480	2,520	2,800	9.3	.6	C1807
Do.	Billie	M		1	2,680	2,730	2,840	15.6	.6	D90444
Do.	-	M		1	2,450	2,490	2,590	9.0	.4	D93272
Do.	-	M		1	2,180	2,220	2,440	8.5	.7	B67785
Dunkle Camp Creek	No. 8	M		1	2,180	2,220	2,440	8.5	.7	B67785
Galena	-	M		1	2,290	2,370	2,640	2.8	.4	C36293
Galena Outcrop	-	M		1	2,290	2,370	2,640	2.8	.4	C36293
Kaltag	-	M		1	2,910+	-	-	23.1	.5	A15869
Adolph Muller	-	M		1	2,910+	-	-	23.1	.5	A15869
Kaltag Prospect	-	M		1	2,680	2,740	2,910	9.5	.4	C36295
Mt. McKinley National Park	-	M		1	2,060	2,230	2,520	7.3	.6	B16186
Alaska Road Commission	-	M		1	2,060	2,230	2,520	7.3	.6	B16186
Prospect	-	M		1	2,150	2,240	2,340	9.6	.3	94109
Menana Field										
Healy Fork										
Arctic Coal Co.	Basal	M		1	2,360	2,400	2,440	13.4	.5	E44121
Do.	do.	T	Run-of-mine	1	2,200	2,260	2,490	8.6	.3	E63869
Cripple Creek	No. 1	M		3	2,250	2,350	2,450	11.5	.3	D64036 to D64038
Do.	do.	T	Run-of-mine	1	2,500	2,550	2,730	12.4	.2	D77713

Arctic Coal Co.	Basal		M										
Do.			T	Run-of-m	1	2,360	2,400	2,440	13.4	.5	E44		
Cripple Creek	No. 1	do.	M		2	2,200	2,260	2,490	8.6	.3	E63869		
Do.		do.	T	Run-of-mine	3	2,250	2,350	2,450	11.5	.3	D64036	to D64038	
						2,500	2,550	2,730	12.4	.2	D77713		
Diamond	-		M		1	2,190	2,260	2,320	8.0	.3	C83485		
Diamond Coal Co.	-		M		2	2,250	2,420	2,480	9.2	.4	D4909 and D4910		
Healy Creek	-		M		2	2,290	2,360	2,480	12.5	.4	D4907 and D4908		
Outcrop	No. 6		M		2	2,190	2,260	2,490	17.8	.3	C30893 and C30894		
Do.	No. 3		M		1	2,420	2,470	2,510	6.2	.2	C30892		
Do.	do.		M		1	2,520	2,560	2,610	5.5	.1	C30895		
Roth-Taylor	Mammoth		M		1	2,370	2,410	2,430	4.6	.1	A11088		
Usibelli	No. 1		T	6- by 2-inch		2,450	2,490	2,700	10.9	.2	D77711		
Do.	do.		T	2-inch by 0		2,330	2,390	2,620	9.7	.2	D77712		
Do.	do.		T	Run-of-mine		2,100	2,180	2,420	7.6	.2	R65840		
Do.	do.		T	2- by 5/8-inch		2,100	2,190	2,340	7.6	.2	R65841		
Do.	do.		T	Run-of-mine		2,120	2,330	2,510	9.1	.3	R65842		
Do.	do.		T	6- by 2-inch		2,130	2,270	2,460	10.1	.3	R65843		
Do.	do.		T	Run-of-mine		2,190	2,360	2,520	9.6	.2	R65844		
Lignite Creek	-		M		1	2,230	2,360	2,760	5.0	.9	C36294		
Nulato Prospect	-		M		1	2,230	2,360	2,760	5.0	.9	C36294		
Lignite	-		M		1	2,230	2,360	2,760	5.0	.9	C36294		
Outcrop Teklanika River	No. 3		M		1	2,340	2,380	2,470	13.5	.4	C64415		
Do.	No. 4		M		1	2,110	2,160	2,260	8.0	.3	C64416		
Outcrop Sanctuary River	Upper		M		1	2,420	2,460	2,520	18.5	.4	C64417		
Do.	Lower		M		1	2,470	2,510	2,560	19.1	.4	C64418		
Outcrop Susnana River	-		M		1	2,130	2,190	2,290	8.2	.3	C64419		
Outcrop Savage River	Top		M		1	2,380	2,440	2,470	19.6	.4	C64420		
Outcrop Savage River	Middle		M		1	2,390	2,420	2,470	20.0	.4	C64421		
Do.	Lower		M		1	2,480	2,540	2,580	10.2	.3	C64422		
Do.	-		M		1	2,820	2,910+	-	22.3	.5	C64423		
Do.	-		M		1	2,510	2,570	2,620	5.9	.2	C64424		
Do.	-		M		1	2,470	2,520	2,580	18.4	.6	C64425		
McKinley	-		M		1	2,260	2,300	2,380	13.6	.5	C64413		
Outcrop Sable Pass	-		M		1	2,260	2,300	2,380	13.6	.5	C64413		
Outcrop Toklat River	-		M		1	2,410	2,470	2,520	9.9	.6	C64414		
Suntrana	-		M		1	2,410	2,470	2,520	9.9	.6	C64414		
Suntrana New	"B"		M		1	2,130	2,180	2,230	6.8	.3	C9526		
Do.	"C"		M		1	2,380	2,430	2,580	15.8	.3	C9525		
Do.	"D"		M		1	2,360	2,400	2,710	16.5	.4	C9530		
Do.	"E"		M		1	2,250	2,300	2,500	13.8	.5	C9524		
Do.	"F"		M		1	2,280	2,350	2,530	12.0	.3	C9527		
Suntrana Old	No. 3		M		1	2,180	2,370	2,440	7.2	.2	B67589		
Do.	do.		M		3	2,340	2,390	2,510	6.3	.2	B80608 to B80610		
Do.	No. 4		M		1	2,130	2,160	2,370	11.6	.2	C9528		
Do.	No. 6		M		1	2,180	2,270	2,400	9.2	.1	C9529		
Unalakleet	-		M		1	2,060	2,140	2,180	8.2	.5	B64867		
Unalaklett	-		M		1	2,090	2,160	2,480	4.7	.4	C36296		
Do.	-		M		1	2,090	2,160	2,480	4.7	.4	C36296		
<u>Kuskokwim Region</u>													
Nelson Island	-		M		4	2,400	2,500	2,680	23.0	.5	C29496 to C29499		
Nelson Island	-		M		4	2,400	2,500	2,680	23.0	.5	C29496 to C29499		
<u>Cook Inlet Region</u>													
Cook Inlet Field													
Bluff Point	-		M		3	1,950	1,970	2,030	11.8	.4	81606 to 81608		
Bluff Point	Cooper		M		3	1,950	1,970	2,030	11.8	.4	81606 to 81608		
Homer	do.		M		1	2,780	2,840	2,910+	14.5	.5	C61783		
Homer Coal Corp.	-		M		2	2,040	2,090	2,280	21.5	.4	C61954 and C61955		
Do.	-		M		2	2,040	2,090	2,280	21.5	.4	C61954 and C61955		
Outcrop	-		M		1	2,380	2,410	2,440	4.5	.2	C83515		

1/ M, mine sample; T, tipple sample.

2/ W, washed.

TABLE 3. - Fusibility of ash of United States Coals (Con.)

State, county, town, and mine	Bed	Kind of sample <sup>1/</sup>	Size of coal <sup>2/</sup>	Number of samples averaged	Fusibility of Ash			Percent, dry basis		Laboratory No.
					Initial deformation temperature, ° F.	Softening temperature, ° F.	Fluid temperature, ° F.	Ash	Sulfur	

## ALASKA (Con.)

Cook Inlet Region (Con.)										
Matanuska Field										
Anthracite Ridge Prospect										
	No. 2	M		1	2,250	2,330	2,420	6.5	.6	A3538
	Do.	M		1	2,230	2,280	2,330	4.2	.3	A3539
	Do.	M		1	2,240	2,320	2,680	6.5	.6	A3540
Chickaloon										
	No. 1	M		2	2,720	2,830	2,880	16.2	.7	83981 and 83982
	Do.	M		1	2,150	2,450	2,570	14.2	.6	83174
	Do.	M	do.	3	2,060	2,270	2,370	12.5	.7	85745 to 85747
	Do.	M	do.	2	1,960	2,100	2,220	9.9	.7	85283 and 85284
	Do.	M	No. 4	1	2,660	2,830	2,880	27.8	.5	83983
	Do.	M	No. 5	1	2,740	2,850	2,900	30.1	.5	83173
	Do.	M	do.	5	2,430	2,600	2,700	16.6	.6	85749 to 85753
	Do.	M	No. 6	1	2,240	2,340	2,390	10.1	.8	85285
	Do.	M	No. 8	4	2,200	2,410	2,580	17.4	.6	85740 to 85743
	Do.	M	No. 10	1	2,200	2,280	2,390	12.5	.7	83984
	Do.	M	do.	1	2,740	2,850	2,900	24.0	.6	85755
Coal Creek										
	Bardin	M		1	2,720	2,830	2,880	23.3	.8	85282
	Do.	M	North Spalding	1	2,340	2,450	2,570	5.9	.6	83985
	Do.	M	do.	2	2,130	2,360	2,430	16.8	.6	85277 and 85278
	Do.	M	do.	2	2,040	2,140	2,210	9.0	.5	85279 and 85280
	Do.	M	do.	1	2,390	2,740	-	16.5	.4	80607
	Do.	M	North Tierney	2	2,440	2,580	2,640	9.6	.6	83986 and 83987
	Do.	M	Olson	1	2,440	2,620	2,740	17.7	.6	85640
Eskola										
	Upper Shaw	M		1	2,400	2,570	2,890	11.3	.5	B67588
	Do.	M	-	1	2,040	2,070	2,260	11.6	.4	C61784
Mrak										
	No. 4	T	2-1/4-inch by 0	1	2,870	2,910+	-	14.2	.9	E1851
	Do.	T		1	2,660	2,790	2,910+	16.9	.4	E69152
Houston										
	No. 00	M		1	2,050	2,310	2,470	22.5	.5	A11087
	Do.	M		1	2,720	2,740	2,800	24.5	.4	A11083
	Do.	M		1	2,400	2,580	2,680	19.7	.3	A11084
	Do.	M		1	2,150	2,370	2,460	22.1	.3	A11086
	Do.	M		1	2,680	2,740	-	15.6	.3	A11085
	Do.	M		1	2,960+	-	-	19.8	.5	A98201
	Do.	M		2	2,650	2,790	2,920+(1)	16.4	.5	B25076 and B25077
	Do.	M		1	2,910+	-	2,830 (1)	19.1	.3	B56286
	Do.	M		1	2,910+	-	-	22.8	.4	B56287
	Do.	T	No. 3	1	2,450	2,490	2,700	27.1	.2	D92251
	Do.	T	do.	1	2,520	2,600	2,780	22.6	.2	D92252
	Do.	T	do.	1	2,680	2,750	2,890	16.6	.2	D92253
	Do.	T	No. 5	1	2,910+	-	-	21.3	.1	D92256
	Do.	T	3- by 1-1/2-inch (W)	1	2,910+	-	-	19.7	.3	D92257
	Do.	T	1-1/2-inch by 0 (W)	1	2,890	2,910+	-	17.9	.2	D92258
	Do.	T	do.	1	2,840	2,910+	-	14.2	.3	E128
	Do.	M	do.	1	2,440	2,610	2,810	8.6	.3	E129
	Do.	M	do.	1	2,780	2,850	2,910+	9.1	.3	E130
	No. 6	M		1	2,840	2,910+	2,810	8.6	.3	E129
	No. 7	M		1	2,440	2,610	2,910+	9.1	.3	E130
	No. 7A	M		1	2,780	2,850	2,910+	9.1	.3	E130
	Do.	M		3	2,140	2,200	2,250	7.5	.3	85511 to 85513
	Do.	M		3	2,720	2,800	2,910+	13.0	.5	B48926
	Do.	M		1	2,720	2,800	2,910+(1)	6.9	.4	B48927 and B48928

