U.S.Geological Survey Open File Report No. 77-416

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Some physical properties of shelf surface sediments, Beaufort Sea, Alaska

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LAYMAN'S SUMMARY

Some physical properties of shelf surface sediments, Beaufort Sea, Alaska
by

Erk Reimnitz, Douglas Maurer, Peter Barnes, and Larry Toimil

The physical properties of sediments presented in this report include their resistance to deformation (shear strength) and penetration (penetration rate), and values of salinity within their pore water. This data, covering large areas of the Beaufort Sea shelf off Alaska, has been gathered over the years, but especially during the 1976 field season.

Shear strength and penetration rate, occasionally determined at the same station, are of value to the designer of offshore structures, in evaluating feasibility of dredging operations, the potential for slumping of sediments, and in studies of ice forces involved in producing the gouges found on the high latitude shelf areas. Shear strengths of surficial sediments were measured with a simple, hand-held shear vane, either on board ship from samples that appeared to be relatively undisturbed, or directly on the bottom by divers. The penetration rates were obtained during sediment sampling operations using a vibratory coring device with 2-m long core barrels. The resistance of sediments to shearing and penetration are not interpreted in this report, except by noting that ice-cemented sediments may occur at two shallow water stations.

Since the average annual water temperatures in the study area are below the freezing point of fresh water, the absence of ice-cemented surficial sediments may be explained by the presence of antifreeze in the form of sea salts within the sediments. Our study of the salinity of pore waters within the sediments was done to learn at what temperatures the sediments should freeze, and to evaluate in what environments and at what

times of the year this may occur. This problem is of utmost importance to many aspects of offshore developments, and to the study of related environmental problems. Using the relation between the salinity of sea water and its freezing point, most of the localities sampled should freeze during the winter. An equation from the Russian literature, using the salinity of pore water and moisture content, appears to give reasonable results on the temperature at which bottom sediments become ice cemented.

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So far almost no data on mass physical properties of shelf sediments in the Alaskan Beaufort Sea has been published. This type of data is important for several reasons. For example, Kovacs and Mellor (1974) attempted to calculate the driving forces on grounded ice producing gouges on the sea floor. Such calculations require knowledge of the mechanical properties of surface sediments encountered by the ice. An understanding of the mechanical properties is also valuable in dredging and offshore construction projects.

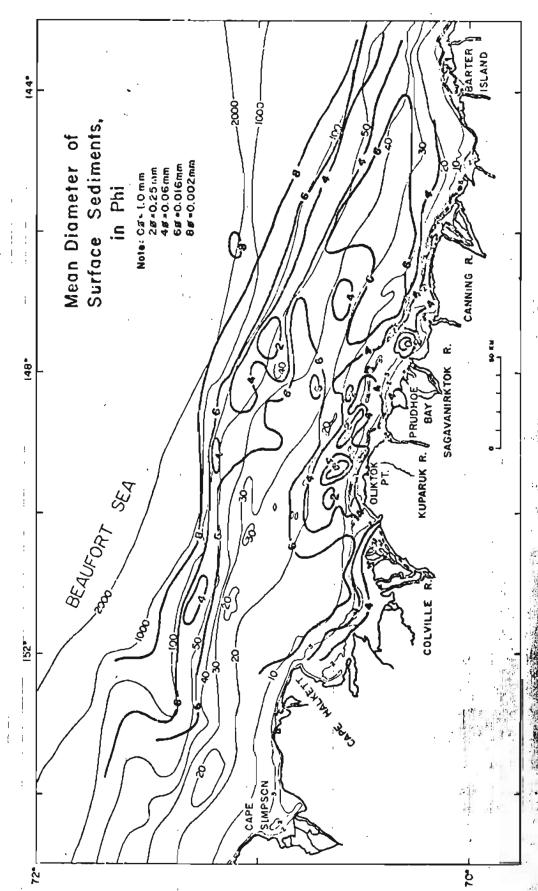
For these reasons we have compiled pertinent information obtained in previous operations, and made additional measurements on the physical properties of sediments during the 1976 field season. The data is reported herein withattempts to interpret the results. For a general description of sediment types found on the shelf within the study area the reader is referred to Barnes and Reimnitz (1974). A compilation of mean diameter particle size of the surficial sediments is shown in Figure 1.

Shear Strength Values from Bottom Samples

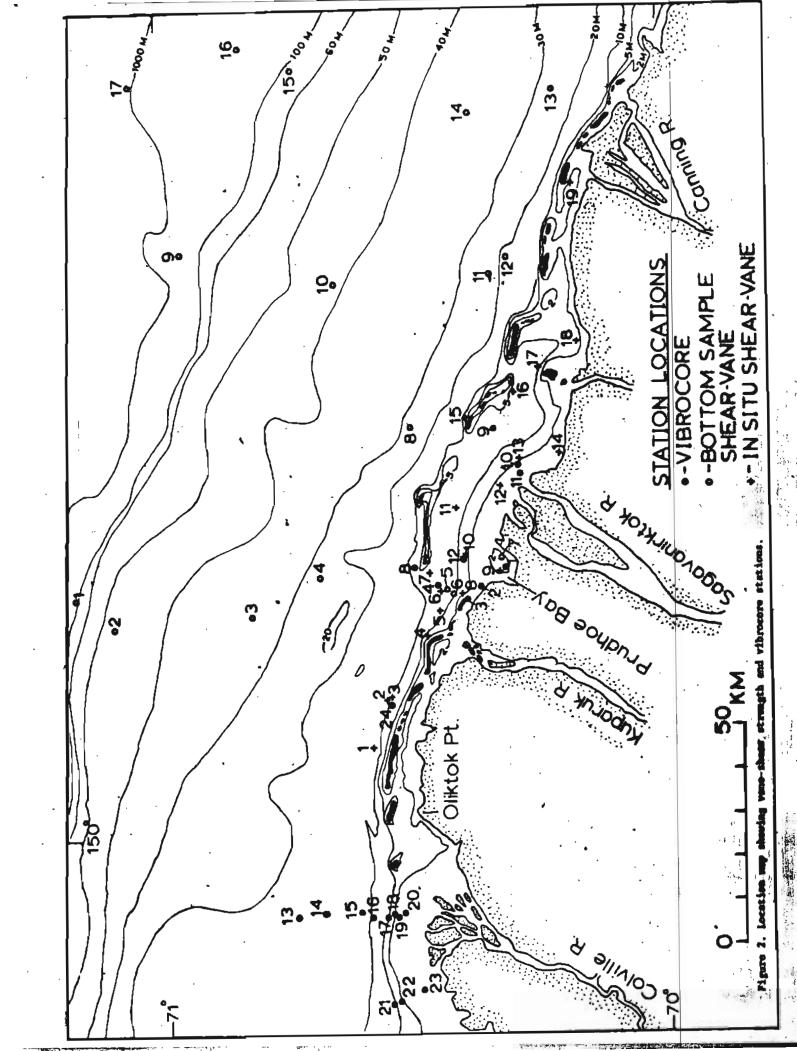
During bottom sampling operation in the past, undrained shear strength values (S_) of relatively undisturbed samples have been measured aboard ship a simple hand held vane shear device (Dill and Moore, 1965). These results, with on-site location, water depth, sampler type, and sediment type have been compiled in Table 1, The station locations are shown in Figure 2.

In Situ Shear Strength Values Obtained by Divers

A few in situ vane shear measurements, using the same hand held instrument were obtained during diving operations in 1972. A number of additional measurements were made in the same way during summer 1976 diving operations.



From Barnes and diameter of surface sediments,



PSI - pounds per square inch
KN/M² - kilo newtons per square meter

Station Number		Water Depth(m)	Shear Str Peak PSI(KN/M ²)	Residual, m	epth of Measu ent, cm below ediment surf	•	Sediment Description
1	71*10.9'N 148"34.0'W	307	0 0.32(2.21)	<u>-</u> -	2 5	Van Veen Grab '	Soft mud Stiff mud
2	71°6,2'N 148°42,0'W	43	0.21(1.45) 1.33(9.17)	-	2 5	Van Veen Grab	Pebbly, sandy, sud Gravelly Mud
3	70°49.6'N 148°31.0'W	33	0.21(1.45) 2.01(13.79)	-	2 5	Van Veen Grab	Soft, fine-grained sandy mud Stiff, fine-grained sandy mud
4	70°41.6'N 148°30.0'W	27	0.01(0.69) 1.11(7.05)	-	2 5	Van Veen Grab	Soft, Fine-grained Mud Gravelly mud
5	70°26.05'N 148°29.26'W		1.11-1.33 (7.65-9.17)	0.1 - 0.21 (0.69-1.45)	6	Undisrupted snapper sample	Brown/grey, medium-grained silty sand w/worm tubes
6	70°25,25'N 148°30.15'W		1.11 (7.65)	0.1 - Q.21 (0.69-1.45)	2	Undisrupted snapper sample	Brown/grey medium-grained silty sand w/worm tubes
7	70°18.92'N 148°20.3'W	3.3	>2.67 (>10.39)	0.88-1.11 (6.07-7.65)	8	Gravity core	Dark grey silty clay
8	70°31.4'N 147°33.0'W	26	<0.10(<0.69) . 0.71(4.90)	-	2 5	Van Veen Grab	Fine-grained sandy mud Stiff medium to coarse-grained sandy mux
9	70°58.3'N 146°30.1'W	364	0 0.38(2.62) 0.66(4.55)	-	2 5 - 10	Van Veen Grab	Soft, brown mud Stiff, grey mud Stiff, grey mud
10	70°40.0'N 146°40.0'W	47	0.44(3.03)	-	2	Van Veen Grab	Muddy sand
ii	70°21.4'N 146°36.0'W	26	0 >2.67(>18.39)	, -	2 5	Van Veen Grab	Soft, fine-grained sandy mud Stiff, coarse-grained sandy mud
12	70°19.6'N 146°30.0'W	17	2.0 (13.79) 2.0 (13.79)	<u>.</u>	2 5	Van Veen Grab	Stiff, grey clay
13	70°13.2'N 145°31.0'W	25	0.88 (6.07) 1.33 (9.17) -2.0 (13.79)	-	2 5 5 - 10	Van Veen Grab	Soft, muddy sand Stiff, gravelly mud Muddy sand
14 .	70°23.4'N 145°34.0'W	37	0.10(0.69)	-	5	Van Veen Grab	Sandy, gravelly, mid w/coarse, 20 cm diameter rocks Stiff, sandy, gravelly, mid
15	70"44.8'M 145"31.0'W	67	0.21(1.45) 0.76(5,24)	-	~ 2 . 5	Van Veen Grab	Pebbly mud Mud
16	70*54.1*N 145*20.0*W	300	0.44(3.03) 0.76(5.24)		2 5	Van Veen Grab	Soft and
17	70°02,3'# 145°32.0'W		0 1,33(9.17) >2.67(>18,39)	-	2 5 5 - 10	77 Van Voon Grab	Pabbly mud Grey mud Stiff Clay

On a number of dives more than one reading was taken. This was done particularly in ice gouged areas, where differences are to be expected between flat, undisturbed bottom, gouge flanks, and gouge floors. At each site the maximum reading (peak) and the reading obtained during the shearing event (residual) were recorded by the diver. See Table II. All these values along with information on station location, water depth, depth below sea floor, bottom type, sediment type, etc. are presented in Table II. Station locations are shown in Figure 2.

Although care was taken by the divers to increase torque slowly and evenly to obtain reliable readings (Fig. 3), currents and other factors did not allow them to do so in all cases. These in situ shear strength values still are considered to be more accurate than those obtained from partly drained and possibly disturbed bottom samples aboard ship. It should be noted that vane shear readings obtained in sandy and gravelly sediments with little or no plasticity are not considered to be good tests due to particle interlocking and other factors.

Penetration Rates of Vibrocore Barrels

Twentyfour vibrocore samples were obtained during the summer of 1976 (Fig. 4), with core length of up to 1.80 m. The rates of penetration were recorded for most stations. These rates provide a qualitative measure of the soil properties in different environments of the inner shelf. In several instances divers using a vane shear measured in situ shear strength of surface sediments near vibrocore stations (Fig. 2).

The vibrocorer is driven by two electric motors producing a combined driving force of 700 kg at a rate of 2,840 impulses/min. Square steel barrels and tubular fiberglass barrels were used in all instances. The steel barrels propagated the vibratory impulse more efficiently to the core nose than the fiberglass barrels, because of the greater damping characteristics associated

TABLE 11 IN SITU SHEAR STRENGTH VALUES

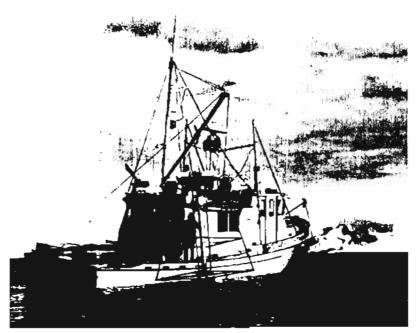
average of several readings
 PSI = pounds per square inch
 XN/M² - Kilo Newtons per square meter

SHEAR STRENGTH

				STRENGTH				
Dive Eite		Water Depth(m)	Peak PSI(XN/M ²)			Bottom description at point of measurement	Sediment description	Comments
1	70°35,6°M 149°27.1'W	12	1,55(10.69) 2,55(17,58)		5	Bioturbated flat bottom	Bioturbated mad	Soft to 10 cm stiffer below
ż	70*33.2'N 149*11.0'W	11.5	1,38 (9.52)	0,69(4.76)	2 .	Seaward foot of major shoel, between gouges	Huddy Band	
3	70°33.12°W	5	0.23(1.59)	0.11(0.76)	2	Flat bottom on major shoel	Clean, medium-grained sand w/clam fragments	Intensely gouged
4	70*28.4'N		A 74/2 241	A 24/2 241	2	Undisturbed sediment near gouge	Muddy sand	Trough of gouge .
'	148°47.2'W	4.5	0.34(2.34)		15	Plat bottom near gouge flank	Sandy, muddy gravel	impenetrable with voins
5	70"26.9"N 148"37.5"W	6.4	>1.38(>9.52) >1.38{>9.52}>		15	Flat bottom	Gray, cohesive mud Very stiff, muddy, sandy gravel w/some shells	
6	70*25.9'X 148*30.5'W	8.5		0-0.34 (0 34)	2	Ploor of gouge	Very soft surficial sediment underlain	
'	240 2010 "	1 1	>1.38(>9.52)		2	Flat bottom	by fairly stiff	
			1.03(7.10)		2	Flat bottom	layer	
7	70*28.1'N		1.03(7.10)	0.46(3.17)	2	Floor of gouge		Stiff boundary at
1 . 1	148*24.0'W	8.5		0,34(2,34)	2	Gouge trough		2.5 om depth
			0.69(4.76)		2	Gouge flank	l., .	covered by fairly
•				0-0.34*			Nod .	most mad w/homezone
				(0-2.34)	2	Gouge flank		clame
		į į	0.69(4.76)	0.23(1.59)	2	Flat bottom		
1 1		r I	>1.38(>9.52)>		5	Plat bottom		
8	70*24.2'N 148*31.5'W	3.0	1.03(7.10)		2 15	Plat bottom	Fine, moddy sand	
9	70°19.8'X 148°23.5'W	2,5	0.54(3.72)	0.44(3.03)	В	Plat bottom	Pine, middy sand	
10	70°24,0'N 148°17.3'W	3.1	1.15(7.93) >1,38(>9,52)>		2 15	Flat hottom	Slightly muddy medium- fine grained sand	
11	70°24.9'# 148°01.0'W	7.0	>1,38(>9,52)>	L,38(>9.52)	2	Rippled flat bottom	Muddy sand	Ripples of 15 cm wavelength
12	70°19.5'N		<u>></u> 1.38{>9.52 >1	38/39 531	2	Flat bottom with ripples	Middy sand	Ripples of 15-20 cm
	147*51.5'W	2,5	>1,38(>9,52)>1 >1,38(>9,52)>1	1.38 (>9.52)	3	Flat bottom with ripples	Very stiff mud	wavelength, 1-2 cm high
73	70*17.2'N 147*42.8'W	3	1.09(7.52) (>1.38(>9.52) >	1.38(>9.52)	2 15	Ripple field-flat bottom	Muddy sand	Ripples of 20 cm wave- length. 2-3 cm height.
			0.69(4.76)	7.46 (3,17)	2.	Exposed underlying gravel on flat bottom	Angular, pea-size gravel	cld, weathered gouges creating broad bottom undulations
14	70°12.8'% 147"41.0'W	1.6	1.15(7.93)	0.92(6.34)	6.5	Flat bottom	Highly moddy, medium grained sand	
15	70*23,8'H	1.5	0.69(4.76)	0.46(3.17)	2	Flat bottom	Sand	
	147*28.7'		₹0.34 (<2.34) <(24/10 241	· 2	Gouged flank and floor	Sand	, ·
			1,38 (9,52)		2		Muddy sand	
1 1		[1.03(7.10)		2	Flat bottom	Huddy sand	
		[1.03(7.10)	71 (4.90)	10	Γ	Pea-size gravel	
16	70*18.2'H	6	0.34(2.34)	,	2	High ground covered by	Soft and	Hummodky relief rela- ted to distribution
	# #		>1.38 (>9.52} >)	1.38 (>9.52)	2	Depression between work tube patches	Muddy sand	of worm tube petches
17	70°14.7'H 147°10.5'W	5.5	>1.38(>9.52) 1	(7.52)	2	Flat bottom	Sandy Bud	Dive site is marked by exposure of firm gravel in depressions
79	70'10.3'N 147'01.0'\	4,5	>1,38(>9.52)>1	1.38(>9.52)	2	Flat bottom with decayed ripple train	Sandy mud	Barrowing activity
19	70°10.8'M	2,5	>1.38(>9.52)	1.15(7.93)	2	Slightly undulating bottom	Sandy mod	Small scale relief from bioturbation



Floure 3. Diver taking in tity sheer vane measurements,



Compared the state of the state

with the fiberglass barrels. Along with the penetration rates, the barrel type used at each station is shown in Figure 5. Station locations and water depths are listed in Table 3.

Only preliminary core studies have been performed so far and we therefore did not include sediment descriptions with the penetration rates. However, by comparing sediment characteristics in the penetrated section with penetration rates, we feel fairly certain that cores 19 and 20 from the Colville Delta were stopped at the top of the underlying ice bonded sediments.

Salinity of Insterstitial Water, Sea Floor Temperatures, and Sediment Freezing

Points

A variety of data pertinent to offshore permafrost problems has been gathered by our Beaufort Sea project over the years. During the 1976 summer field season on the R/V KARLUK we made a special effort to obtain reliable data on the salinity of interstitial waters in surficial sediments on the inner shelf.

Our main objectives in this study are to gain an understanding of the sedimentary environment on the arctic shelf. The shelf surface is affected and modified by waves, currents, strudel scour, ice gouging, small critters, and many other factors. Our thinking about bottom processes has been based on the assumption that the sediment surface is unfrozen (Reimnitz and Barnes, 1974). There is some justification for this assumption, at least for summer conditions. In our sampling, driving of thermoprobes, diving, boat anchoring, etc., we apparently have never encountered ice bonded sediments, (except possibly at several vibrocoring stations in very shallow water near the Colville River, as stated earlier in this report. Even during the driving of a thermoprobe in bottom-fast ice off the Kuparuk River, when some of the data reported herein was obtained, penetration was not prevented or retarded by ice bonding within the sediment, as far as we can determine.

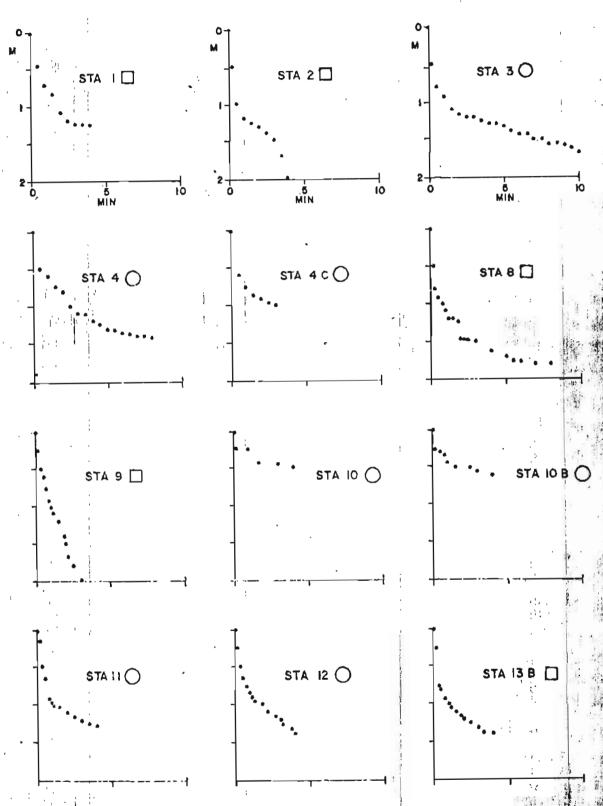


Figure 5. Penetration rates of vibrocore barrels. Barrel type used (square steel or round fiberglass) identified by symbol.

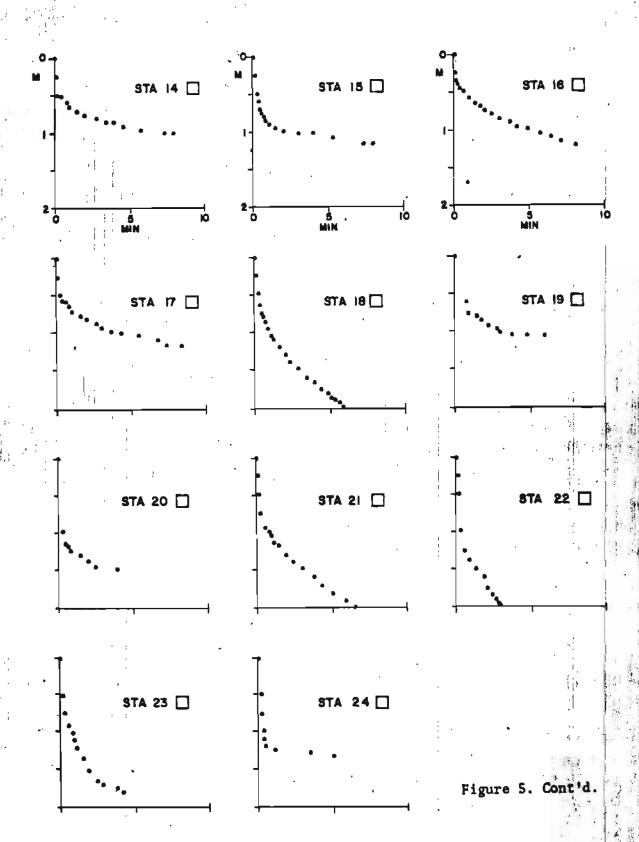


TABLE III VIBRO CORE STATIONS

Station Number	Location	Water Depth(m)	Station Number	Location	Water Depth(m)
1	70°19.0'N 148°22.0'W	3	15	70°37.0'N 150°27.0'W	12.4
2	70°22.3'N 148°28.4'W	1.7	16	70°36.3'N 150°28.2'W	11.5
з.	70°24.0'N 148°33.2'W	1.5	17	70 ⁰ 34.0'N 150 ⁰ 28.2'W	8.5
4	70 ⁰ 27.3'N 148 ⁰ 28.2'W	6.5	18	70°33.3'N 150°27.9'W	3.3
8	70°29.8'N 148°20.8'W	8	19	70°33.6'N 150°28.1'W	2
9	70°20.1'N 147°31.1'W	6.5	20	70°32.7'N 150°27.5'W	1.5
10	70°17.1'N 147°44.3'W	2.7	21	70°33.8'N 151°01.0'W	4
• 11	70°17.7'N 147°47.0'W	1	ⁱ 22	70 ⁰ 32.5'N 150 ⁰ 59.6'W	0.6
12	70 ⁰ 24.1'N 148 ⁰ 18.5'W	, 3	23	70 ⁰ 29.5'N 150 ⁰ 55.9'W	i.
13	70°44.8'N 150°28.1'W	19	24	70°33.2'N 149°11.2'W	17.5
14	70 ⁰ 41.5'N 150 ⁰ 27.2'W	15			

ments during the peak of the winter, this would be very important for studies of bottom processes, for biological studies of bottom dwelling organisms, and for offshore construction projects. For example, high flow velocities recorded by current meters could indicate that sediment transport is taking place, while in fact the seabed may actually be frozen. An example of potential environmental impact may be envisioned by considering the influence of a cold pipe line carrying natural gas buried on the shelf. If the shelf sediments are close to the freezing point, the cooling effect of such a pipe line may result in the freezing of overburden. Bedload transport of sediment might be affected such that individual grains in transit, temporarily contacting the bottom, may become adfrozen. This in turn could result in the formation of a sediment dike along the pipeline corridor.

Sediment Salinity

Interstitial salinities were determined from sediment samples collected in 1972 and 1976. In 1972, deep water samples were obtained by gravity corers on the outer shelf (Table IV, stations 1-5). From these cores 10 cm sub-samples were taken, squeezed, and processed on board by diluting 40 ml of interstitial water to 200 ml, on which the conductivity was measured. The 1976 values (Table IV, stations 6-21) were obtained from samples collected in plastic tubes by divers, and stored at 0°C until processing. Since these inner shelf samples were quite variable in composition, different methods had to be used for waters extraction and salinity determination. Some of the samples were centrifuged for 15 minutes at 15,000 rpm. 20 ul of interstitial water were titrated against a Copenhagen Standard seawater of known chlorinity, using a London Co. Automatic Chloride Titrator. Values obtained by this method are given in Table IV.

The remainder of the samples required a dilution method to obtain an adequat volume for titration. A portion of the subsample was oven-dried at 110 C to

PREEZING TEMPERATURE OF BOTTOM SEDIMENTS

- Conductivity Method Dilution Method
- Centrifuge Hethod
- 1. Molochushin & Gauvliev (1970)
 2. Doherty & Rester (1974)
 8-Assumed Moisture Content
 = 50% dry weight.

Tacking & Location Location Supplies Design Solid Solid Construction C					- Cantriride We	thod	- 50	e dry wei	.ght.
1 150 00.0 to 5 17.5 - 27.5 3 27.7	Station #	location		ment Surface (C)	() . Balinity (0/00)			z, ² (°C)	Sediment Description
71 13.2 '' 22.5 - 4.3 32.5 74.10 7-78 7-7	1	151°00.0'W	53	12.5 - 22.5	37.7		8-4.34 8-3.88	-2.07 -1.95	Sandy Hud
70°50.8°8 40 10 10 33.8° 4-3.57 -1.8° 30 10 10 10 33.8° 4-3.57 -1.8° 310°70.8°8 44 10 -20 39.8° 4-4.57 -2.21 30 10 10 10 10 10 10 10 10 10 10 10 10 10		71°12.2'N		42.5 - 52.5	33,61		1-3.90	-1.84	Towns of the second of the sec
10 20 27:1 10 20 27:3 27:10 28:4 27:10 28:4 28:3	3 2 .	150°58.0°N 70°58.8'E	19	12.5 - 22.5	24.4'		\$-2.89	-1.32	Stiff clay with Sand Pochete
150 00.0 19 28 30 - 50 33.0 1	3	149 ⁰ 37.1'W 71 ⁰ 07.8'W	146	10 - 20	39.9		1~4.57	-2.21	Nud with Fine Sand Patches - Scattaged public
5 136°00.0°w 24	4.3	150°00.0°W	28	10 - 20	33.0'		0-3.84	-1.01	
6 149°11.0'W 11.5 15 26.5° 21.99 -6.61 -1.44 Very clean medium grained sand 70°33.2'W 4.5 10 20.8° 26.35 -4.50 -1.11 Moddy, grayally sand with sub-remoded grained and 70°24.4'W 4.5 10 20.8° 26.35 -4.50 -1.12 Moddy, grayally sand with sub-remoded grained and 70°26.9'W 6.4 13 26.8° 35.73 -4.15 -1.16 failf, very fine sandy med 70°26.9'W 1.5 6.5 24.7° 35.73 -4.15 -1.12 Dark gray med 70°26.9'W 2.5 6.5 24.7° 35.27 -4.06 -1.34 Fine grained modely sand 70°36.9'W 2.5 6.5 24.7° 35.27 -4.06 -1.34 Fine grained modely sand 70°36.28'W 2.5 - 22.1° 40.59 -1.21 -1.20 Fine-grained modely sand 70°36.28'W 2.5 - 22.1° 40.59 -1.21 -1.20 Fine-grained modely sand 70°36.28'W 2.5 - 24.0° 40.79 -1.52 Fine-grained modely sand 70°36.28'W 2.0 - 24.0° 40.79 -1.50 Light gray very fine modely sand 70°36.28'W 2.0 - 24.0° 40.79 -1.05 Light gray very fine modely sand 70°310.0'W 2.0 - 34.4° 41.71 4.75 -1.91 Fine-grained modely sand 70°310.5'W 2.5 14 16.9° 40.79 -1.05 Light gray very fine modely sand 70°310.5'W 2.5 14 16.9° 40.79 -1.05 Light gray very fine modely sand 70°310.5'W 2.5 14 16.9° 24.36 -4.66 -1.00 Clean fine sand 70°310.5'W 2.5 14 16.9° 24.36 -4.66 -1.00 Clean fine sand 70°310.5'W 2.5 14 16.9° 24.36 -4.66 -1.00 Clean fine sand 70°310.5'W 2.5 14 16.9° 27.3° -1.03 Light gray very fine grained sand 70°310.5'W 2.5 14 16.9° 27.3° -1.03 Light gray very fine modely sand 70°310.5'W 2.5 14 16.9° 27.3° -1.03 Light gray very fine modely sand 70°310.5'W 2.5 14 16.9° 27.3° -1.05 Light gray very fine modely sand 70°310.5'W 2.5 14 16.9° 27.3° -1.05 Light gray fine modely sand 70°310.5'W 2.5 15 14 16.9° 27.3° -1.05 Light gray fine modely sand 70°310.5'W 2.5 14 16.9° 27.3° -1.05 Light gray fine modely sand 70°310.5'W 2.5 14 16.9° 27.3° -1.05 Light gray fine modely sand 70°310.5'W 2.5 14 16.9° 27.3° -1.05 Light gray fine modely sand 70°310.5'W 2.5 14 16.9° 27.3° -1.05 Light gray fine modely sand 70°310.5'W 2.5 14 16.9° 27.3° -1.05 Light gray fine modely sand 70°310.5'W 2.5 14 16.9° 27.3° -1.05 Light gray fine modely sand 70°310.5'W 2.5 14 16.9° 27.3° -1.	5	730°00°0,M	24	0 - 10	33.1'		6-3.85 -3.87	-1.81 -1.62	Pine and grading into very sticky and with w
148 0 1 2 1 2 1 2 2 2 1 2 2 2 2 2 2 2 2 2 2	6	149 ⁰ 11.0'W	11.3		<u> </u>	21.99			Very clean medium grained send
8 148 37.3 1 6.4 5 21.3 74.83 -1.66 -1.13 Grey Mad 159 70 26.5 1 6.4 15 26.8 7 35.93 -4.15 -1.46 Entit, very fine sandy mad 70 26.5 1 8.5 6.5 24.7 35.93 -3.83 -1.20 Dark grey mod 70 26.5 1 8.5 6.5 24.7 35.27 -4.06 -1.34 Fine grained middy and with sood Fragment 10 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	7	70°33.2'N		10		26.35		1	· · · · · · · · · · · · · · · · · · ·
10				5	21.3*	74.83			Grey Mad
10: 146°24.0'W 8.5 - 22.1° 40.59 -3.21 -1.20 Fine-grained middy and with each framework. 11: 148°31.5'W 3.0 15 27.9 6-3.28 -1.52 Fine-grained middy and of the each framework. 12: 148°22.5'W 2.0 - 24.0- 8-2.80 -1.30 Very fine-grained middy and m		70°26.9'N		-	24.34	36.89	-3.83		Dark grey med
11 148°21.5'W 2.0 - 24.0"	11	70°26.9'W	8.5	6.5	24.74	35.27	-4.06	·-1.34	
12 148°21.2'N 2.0 - 24.0" 8-2.80 -1.30 vary fine-grained middy sand 18.9" 40.79 -2.85 -1.03 Light grey vary fine middy sand 70°20.2'R 2.0 - 34.4	· · · · · · · · · · · · · · · · · · ·		1, -	+		40.59	-3.21	-1.20	
18.9° 40.79 -2.85 -1.05 Light grey very fine middy sand 18.9° 24.46 74.45 -1.98 -1.28 Grey mid 147°51.5°W 70°19.5°N 2.5 14 18.9° 24.36 -4.46 -1.03 Clean fine mand 15.9° 24.36 -4.46 -1.35 Clean fine mand 15.9° 24.36 -4.46 -1.35 Clean fine mand 15.9° 24.36 -4.46 -1.36 Clean fine mand 24.36 -1.46 -1.36 Clean fine mand 15.9° 24.36 -1.46 -1.36 Clean fine mand 24.36		70°24.2'N	+	1			-		
14	12	70°20.2'K	2.0			-40.79			Light grey very fine middy sand
15 147°42.8'W 3.0 16 25.5" 9-3.01 -1.39 Medium grained Modely Seed with shell 16 167°41.0'W 70°12.8'B 1.6 20 27.3" 9-3.21 -1.43 Modely fine grained send 18 147°22.8'W 1.5 10 22.3° 9-2.65 -1.21 Clean medium-grained send 18 147°10.7'W 16-0 14 30.2° 8-3.53 -1.65 Grey mid 18 147°10.5'W 2.5 5 24.9° 25.66 -5.46 -1.35 Fine-grained send 20 24.9° 25.66 -5.46 -1.35 Fine-grained send 20 147°01.0'W 4.5 17 29.4° 8-3.45 -1.60 Dark gray fine sendy mid 21.7° 9-2.81 -1.29 Medium grained Modely Seed with shell 25.5° 24.9° 25.66 -5.46 -1.35 Fine-grained send 20 20 20 20 20 20 20 2	713	70°19.0'm	2:0	′ ⊢ ——					なるない はない ない な
16	14	70°19.5'N	2.!	3 14	18.9*	24.36	4.46	-1.03	
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21 146°03.4'W 2.5 14 23.7' 0-2.81 -1.29 modium to construction and the second s	·:	70014.71%		_	24.9	25.66			A Line the real Life with the sufficient
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The same of the sa	<u>}</u> 21	70°10.8'%	2.9	5 14	23.7		0-2.81	-1.29	Madille to coarse-oreined mildy cand

determine moisture content. The remainder was diluted with 2 ml of distilled water, shaken on a wrist action shaker for 20 minutes, and centrifuged for 15 minutes at 2,000 rpm. Again, 20 µl were titrated using the automatic titrator. The values obtained by this technique are identified in Table IV by asterisks (*). Chlorinities were converted to salinities using the relation

Salinity($^{\circ}$ /oo) = 0.03 + 1.805 x Chlorinity ($^{\circ}$ /oo).

Using the salinity values of interstitial water, we calculated the hypothetical freezing temperatures of the sediment from two different relationships:

1) Molochushkin and Gavuliev (1970) show that:

$$T_f = 28.4 \times (e^{0.22} \times S/W - 1) - 5e^{-35} \times (W - 0.035)$$

where T_f is the freezing temperature in degrees Centigrade, S is the salinity of pore water in parts per hundred, and W is the moisture content in "relative units" (from our translation), and e = 2.7. For the simple-minded geologist this relation has only one minor problem: it gives positive freezing temperatures. Changing the term

$$e^{0.022} \times S/W$$
 to $e^{-0.022} \times S/W$

we obtain what appear to be reasonable values for freezing temperatures, and therefore assume a printing error was made. The equation now reads:

-0.022 x S/W -35 x (W - 0.035)

$$T_f = 28.4 \text{ x } (e^{-0.022 \text{ x S/W}} - 1) - 5e^{-35 \text{ x } (W - 0.035)}$$

Only for the samples processed by the dilution method did we obtain value for moisture content (Table IV). In our calculations of freezing temperature we assumed a moisture content of 50% for the remaining samples. This assumed value was slightly greater than the measured, which averaged between 35 and 40% in moisture content. Possible deviation of \pm 20% in moisture content from the assumed 50% value would result in freezing point errors of \pm 1.5° C for the most saline samples to \pm 1.0° C for the least saline samples.

2) Osterkamp and Harrison (1976), working on offshore permafrost problems in the Prudhoe Bay area, calculated the freezing temperature of sediments using an equation that applies to seawater alone (Doherty and Kester, 1974), and disregards the fact that the deposit is a mixture of water and sediment:

$$T_f = 1.37 \times 10^{-2} - 5.199 \times 10^{-2} s - 7.225 \times 10^{-5} s^2$$

Where S is salinity in parts per thousand. For the soil samples they obtained, the error in this procedure was estimated to be less than 20%.

A two-meter long thermoprobe, with thermistors, coupled to a Wheatstone Bridge, was used in two different field operations to measure sea floor temperatures. Nine measuring stations occupied by the R/V LOON during the middle of September in 1976 are shown in Figure 6 (inset, black dots). The values obtained at these stations, shown in Figure 7, represent sea floor conditions close to the end of the open water period, probably slightly past the time ##80 when the sea floor is the warmest. The measurements around the mouth of the Kuparuk River were made in late May, 1972, using the sea ice as a base of operations. These values represent temperature conditions just prior to river flooding of the sea ice, shortly after the temperature-low of the winter. Thus, the temperature data shown in Figure 7 does not represent the extremes encountered from winter's low to summer's peak. The sediment surface temper were extrapolated and the results are shown in Table V. These extrapolated sea floor temperatures are plotted with the respective station locations in Fig. Sea floor temperatures extrapolated by Lachenbrach and Marshall (1977) from May, 1976, data are in general agreement with these values.

Speculating on the implications of the presented data, we sketched in Figure 8. This is based on the assumption that the average annual temperature and environmental conditins fro the thermoprobe stations off the Kuparuk River are rather similar to those in the Prudhoe Bay vicinity, occupied at a different time of the year. From this assumption, we sketched a hypothetica cross-section through a shallow lagoon or bay across a sill with a depth less than the maxi-

mum fast ice thickness (approx. 2 m), and into the open ocean (Fig. 8).

Winter and summer bottom temperatures (Fig. 8) measured in the very shallow lagoon, in the deepest part of the lagoon, at the shallow sill, and at several water depths offshore are shown. Note that no values are available for the shallow sill during winter conditions. In the deepest part of Prudhoe Bay and near the sill, the summer temperatures show a considerable range of values. These are shown as vertical bars in Figure 8. Also shown in Figure 8 are the freezing temperatures for the seabed calculated from our data on salinity of interstitial waters and moisture content, using the two different equations.

Freezing temperatures calculated from the equation applying to pure sea water suggest that the seabed from shore to a water depth of about 7 m would become ice-bonded during the winter. This equation therefore probably should not be used. The equation from Molochushkin and Gavuliev (1970) shows that only those areas shallower than 2 m of water depth are close to the freezing point during the winter, and this seems reasonable.

Plans are being made to obtain more of this type of data during the coming field season.

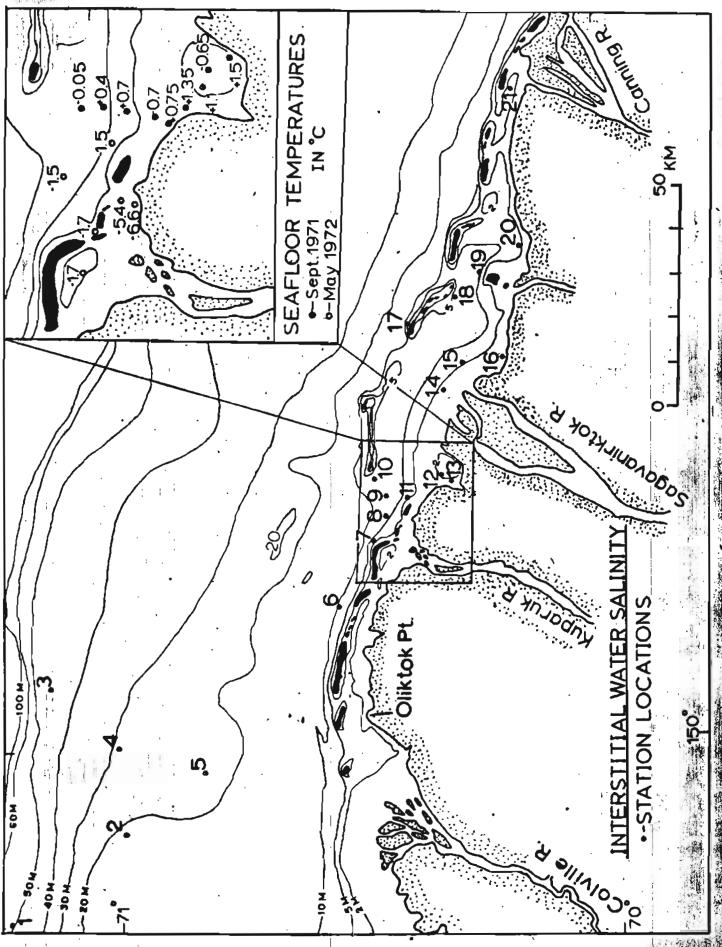
ACKNOWLEDGMENT

This study was supported by the Bureau of Land Management through interagency agreement with the National Oceanic and Atmospheric Administration, under which a multi-year program responding to needs of petroleum development of the Alaskan continental shelf is managed by the Outer Continental Shelf Environmental Assessment Program (OCSEAP) Office.

TABLE V
Thermoprobe Stations:

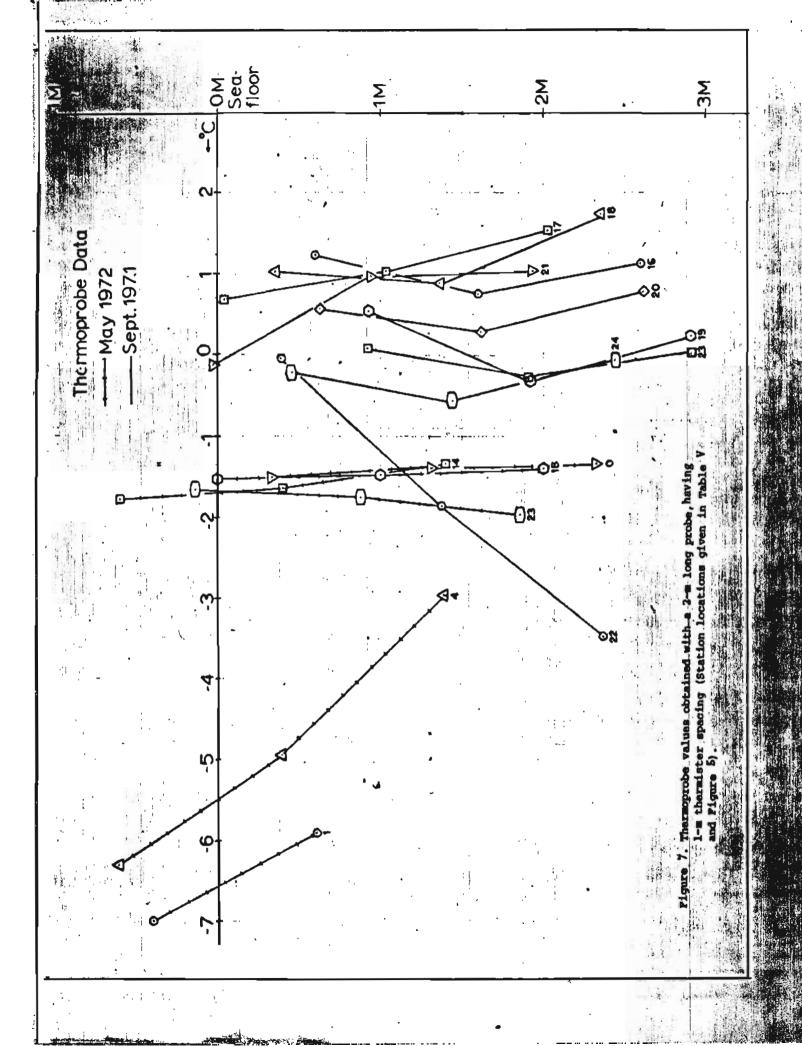
*May, 1972 'Sept., 1971

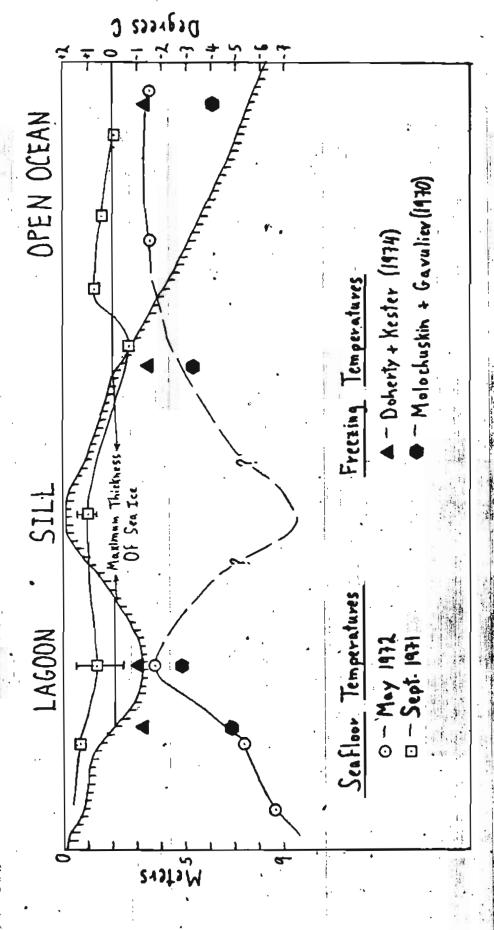
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Station	Location	(M)Water Depth	(°C)Sea Floor Temperature				
0*	70°25.0'N 148°30.8'W		-1.5				
1*	70°23.8'N 148°41.0'W		-6.6				
4*	70°24.4'N 148°40.5'W		-5.4				
14* /4	70°25.9'N 148°45.3'W	3.2	-1.7				
18*	70°27.4'N 148°34.0'W		-1.5				
23*	70°26.6'N 148°50.2'W		-1.7				
16'	70°18.2'N 148°19.0'W	3.2	+1.5				
17.	70°19.2'N 148°20.5'W		-0.65				
18'	70°19.9'N 148°23.0'W	2.7	+1.1				
19'	70°20.6'N 148°26.0'W	1.5	+1.35				
201	70°21.6'N 148°28.5'W	1.7	+0.75				
21'	70°22.4'N 148°27.6'W	2.6	-0.7				
221	70°24.7'N 148°26.0'W	4.1	+0.7				
23'	70°25.0'N 148°25.1'W	5.5	+0.4				
241	70°26.1'N 148°25.1'W	6.8	-0.05				



o Location map for stations at which the sailuity of inter-

extrapolated seab





re 8. Hypothetical seafloor profile extending from beach through a lagoon or bay, across a shallow sill to the open ocean.

Representative extrapolated bottom temperature values during the purmer and values during a summer and values conditions and calculated seabed freezing.

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