

INTEROFFICE CORRESPONDENCE

APPLIED STRATIGRAPHY
DATE June 23, 1982

TO P. A. Mundt

CC U. A. Franz
A. J. Miller - FRL
H. H. Mottun - Denver
W. F. Sinclair
M. J. Bender

THERMAL

ESC REQUEST NO. 311B54
MATURATION STUDIES
GULF COLVILLE DELTA
STATE #1, N. SLOPE
ALASKA

Thermal maturation studies (RO, TAI and T-max.) on the fifty three ditch and core samples from 300' to 9200 (T.D.), indicate that transitionally mature rocks (Ro=0.5 to 0.6) first occur between 5950' to 7000'. Poor sample quality due to caved and recycled or oxidized organics prevents exact determination of the depth of the initiation of thermal maturity (Ro=0.5). The broad polymodal Ro histograms, the scattered TAI values and the inconsistent T-max. measurements reflect this poor sample quality.

T-max. measurements suggest a thermal break between thermally immature sediments and transitionally mature sediments at about 6600'. TAI values indicate a probable thermal shift at 7000'. Vitrinite reflectance studies indicate a thermal shift between 5950' and 6680'.

Caved and recycled or oxidized vitrinite is very common in all the samples. Most of the samples contain less than fifteen percent indigenous vitrinite. Nine samples contain no indigenous vitrinite. I suspect that in an equal number of samples, caved vitrinite has been interpreted as the indigenous vitrinite. The interval from 5950' to 9200' TD was sampled very erratically. Some of the samples are less than fifty feet apart, and have Ro means that vary by as much as 0.06. The close sample intervals and wide range of Ro mean values between 5950' to 6680' allows for two interpretations for the initiation of thermal maturation (see figure 1). An excellent source rock will produce hydrocarbons in the transitionally mature range, while a poor source rock requires a higher thermal maturity.

Included in this report are copies of the Ro histograms, visual Kerogen work sheet, a plot of the mean Ro values, a plot of the TAI measurements, a copy of Brown and Ruth Laboratories Rock Eval Pyrolysis results which includes T-max values, and a table of maturation values and Kerogen types.

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Alaska Oil & Gas Cons. Commission
Anchorage

P. A. Mundt

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June 23, 1982

Vitrinite reflectance readings were taken by R. R. Taylor. If you have any questions concerning this report, please contact me.

R. J. Enrico

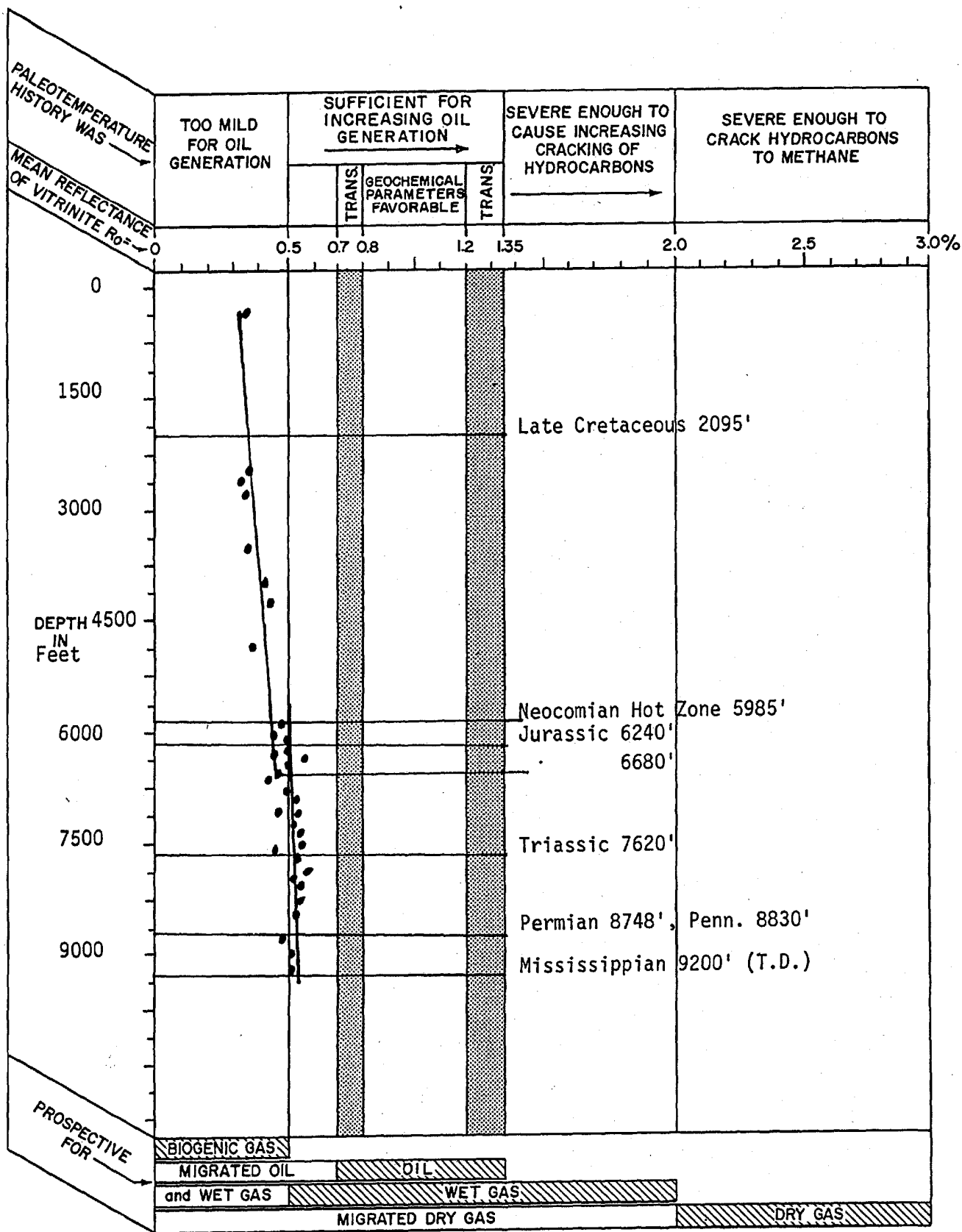
A handwritten signature in cursive script, appearing to read "R. J. Enrico".

RJE:mp

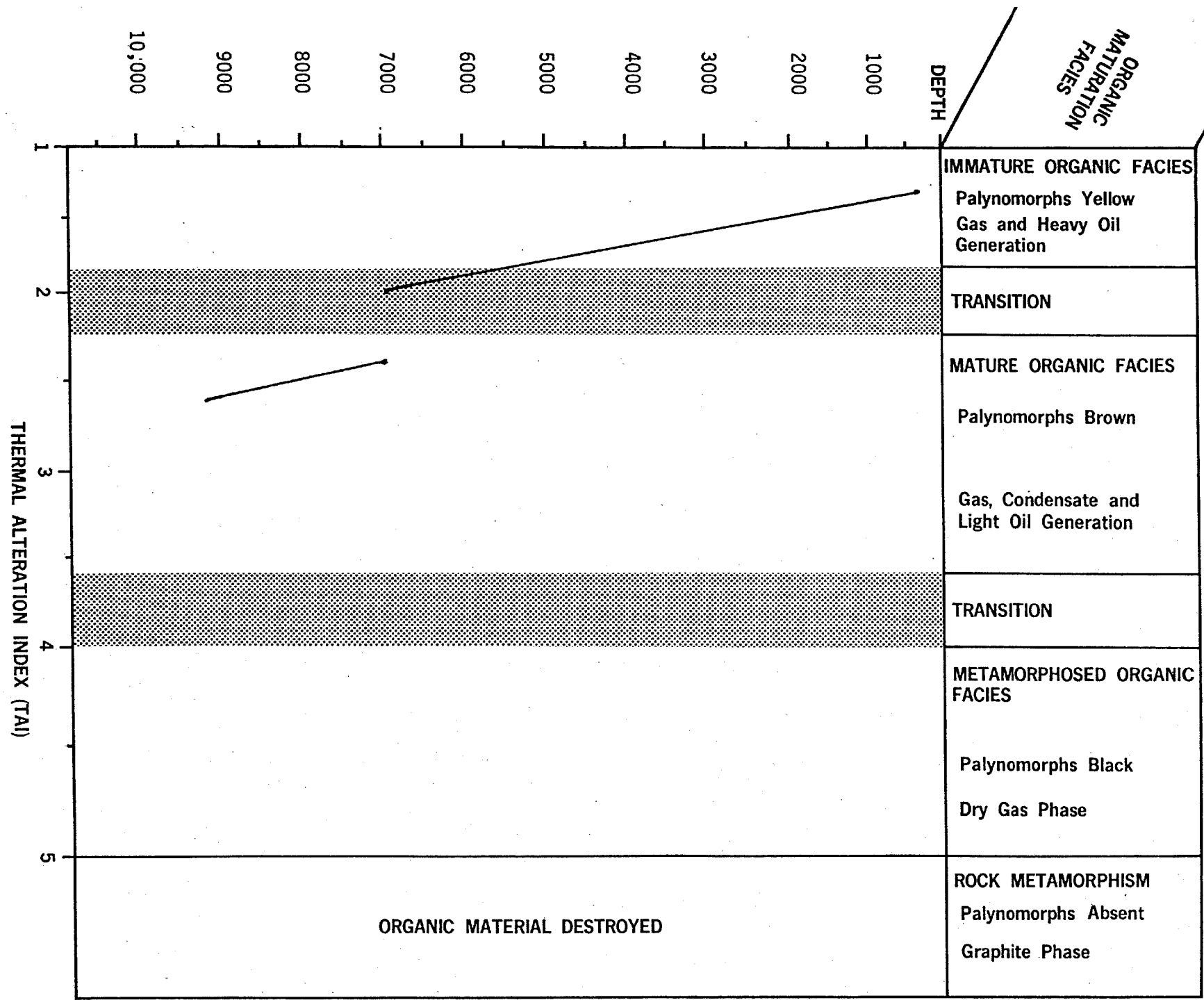
Attachments

Mean Ro Value
 Gulf Colville Delta State #1
 Figure 1

M-047
 (6-78)



THERMAL ALTERATION INDEX
 Gulf of Mexico Delta State #1
 Figure



M-390(9/76)



BROWN & RUTH LABORATORIES, INC.
GEOCHEMICAL LOG

OPERATOR: Gulf Oil Corporation
 WELL NAME: No. 1 Colville Delta State
 LOCATION: North Slope, Alaska
 T.D.: 929'

DEPTH (ft.)	LITHOLOGY	SOURCE BED POTENTIAL				MATURITY			HYDROCARBON INDICATIONS		FORMATION	AGE		
		T.O.C. (wt. %)		S2 (mg/g)		S2 / S3		HYDROGEN INDEX					S1 (mg/g)	
		LOW	HIGH	POOR	FAIR	COOK-VERY COOK	GAS	IMMATURE	OK	GAS			0-5	15-25
1												TERTIARY		
2														
3												CRETACEOUS		
4														
5												HOT ZONE		
6														
7												KINCAID		
8														
9												SHALE		
10														
11												LAVIN		
12														
13												ALASKA		
14														
15												PENN.		
16														
17												MES		

LITHOLOGICAL LEGEND

- SANDSTONE
- LIMESTONE
- SHALE OR SILTSTONE
- COAL
- DOLOMITE
- CONGLOMERATE

PYROLYSIS TERMS

- S1 FREE HYDROCARBONS PRESENT IN ROCK
- S2 HYDROCARBONS FROM PYROLYSIS OF KEROGEN
- S3 = CO₂ FROM KEROGEN PYROLYSIS
- HYDROGEN INDEX S2/T.O.C.

TABLE
Gulf Colville Delta State #1
N. Slope Alaska

<u>DEPTH OR SPL. NO.</u>	<u>LOW-GRAY Ro MEAN</u>	<u>% POP.</u>	<u>FIRST HIGH-GRAY Ro MEAN</u>	<u>% POP.</u>	<u>TAI</u>	<u>THERMAL MATURITY</u>	<u>KEROGEN TYPE</u>	<u>HYDROCARBON POTENTIAL/REMARKS</u>
320'	0.37	30	0.79	43	-	Immature	Type IV	No source
930'	-	-	-	-	-	-	Type IV	No source
1440'	-	-	-	-	-	-	-	
2130'	-	-	-	-	-	Immature	Type III	Poor/Gas
2440	0.38	11	0.93	77	1	Immature	Type III	Poor/Gas
2620'	0.35	17	0.86	42	1	Immature	Type III	Poor/Gas
2770'	0.36	5	0.97	75	1	Immature	Type III	Poor/Gas
3580'	0.37	7	0.93	83	1+	Immature	Type III	Poor/Gas
3970'	0.43	15	0.97	76	-	Immature	Type III	Poor/Gas
4360'	0.44	14	0.92	68	1	Immature	Type III	Poor/Gas
5020'	0.39	12	0.92	71	1-1+	Immature	Type III	Poor/Gas
5950'	0.49	14	1.20	76	1+	Immature	Type III	Poor/Gas
6063'	0.47	21	1.14	51	1+	Immature	Type III	Poor/Gas
6120'	0.50	26	1.17	70	1-1+	Immature	Type III	Poor/Gas
6200'	0.50	11	1.03	71	1+	Immature	Type III	Poor/Gas
6280'	0.46	15	0.99	79	1+	Immature	Type III	Poor/Gas

TABLE
Gulf Colville Delta State #1
N. Slope Alaska

<u>DEPTH OR SPL. NO.</u>	<u>LOW-GRAY Ro MEAN</u>	<u>% POP.</u>	<u>FIRST HIGH-GRAY Ro MEAN</u>	<u>% POP.</u>	<u>TAI</u>	<u>THERMAL MATURITY</u>	<u>KEROGEN TYPE</u>	<u>HYDROCARBON POTENTIAL/REMARKS</u>
6360'	0.54	23	0.97	56	1+-2	Transi- tionally mature	Type IV	No Source
6440'	0.50	18	1.03	60	1+-2	Transi- tionally mature	Type III	Poor/Gas
6520'	0.48	18	1.05	67	1+-2	Immature	Type III	Poor/Gas
6600'	0.45	13	1.00	75	1+-2	Immature	Type III	Poor/Gas
6680'	0.47	11	1.00	77	1+-2	Immature	Type III	Poor/Gas
6760'	-	-	-	-	1+-2	Immature	Type III	Poor/Gas
6840'	0.50	16	1.04	68	1	Immature	Type II	Gas/Oil
6920'	0.51	8	1.11	77	1+ 2	Transi- tionally mature	Type II	Gas/Oil
7000'	0.48	20	1.00	60	1+-3-	Transi- tionally mature	Type II	Gas/Oil
7080'	0.52	16	1.07	64	1+-2+	Transi- tionally mature	Type II	Gas/Oil
7160'	0.51	11	1.09	82	2-2+	Transi- tionally mature	Type II	Gas/Oil

TABLE
Gulf Colville Delta State #1
N. Slope Alaska

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7240'	0.50	20	1.09	66	1+-2+	Transi- tionally mature	Type II	Gas/Oil
7300'	0.53	13	1.01	74	1+,2+	Transi- tionally mature	Type II	Gas/Oil
7350'	0.51	8	1.12	80	1+,2+	Transi- tionally mature	Type II	Gas/Oil
7400'	0.50	14	1.22	72	2,3 ⁻	Transi- tionally mature	Type II	Gas/Oil
7450'	0.50	16	1.17	78	2,3 ⁻	Transi- tionally mature	Type II	Gas/Oil
7500'	0.56	14	1.16	73	1+,2+	Transi- tionally mature	Type II	Gas/Oil
7550'	0.50	7	1.03	66	1+-2	Transi- tionally mature	Type II	Gas/Oil
7620'	-	-	-	-	1+	Immature	Type II	Gas/Oil
7650	-	-	-	-	-	-	-	-
7710'	-	-	-	-	1+-2	Transi- tionally mature	Type II	Gas/Oil

TABLE
Gulf Colville Delta State #1
N. Slope Alaska

<u>DEPTH OR SPL. NO.</u>	<u>LOW-GRAY Ro MEAN</u>	<u>% POP.</u>	<u>FIRST HIGH-GRAY Ro MEAN</u>	<u>% POP.</u>	<u>TAI</u>	<u>THERMAL MATURITY</u>	<u>KEROGEN TYPE</u>	<u>HYDROCARBON POTENTIAL/REMARKS</u>
7760'	-	-	-	-	2,3 ⁻	Transi- tionally mature	Type II	Gas/Oil
7800'	53	10	1.07	64	2	Transi- tionally mature	Type II	Gas/Oil
7800'	0.57	19	1.13	60	1+,2+	Transi- tionally mature	Type II	Gas/Oil
7890'	0.52	15	1.09	55	2-2+	Transi- tionally mature	Type II	Gas/Oil
8016'	-	-	-	-	-	-	-	Gas/Oil
8070'	0.55	17	0.93	72	2+	Transi- tionally mature	Type II-III	Marginal Gas/Oil
8242'	0.55	7	1.10	63	2-2+	Transi- tionally mature	Type II-III	Marginal Gas/Oil
8250	0.48	7	1.03	68	2	Transi- tionally mature	Type II-III	Marginal Gas/Oil
8990'	0.53	6	1.00	71	1+-2+	Transi- tionally mature	Type II-III	Marginal Gas/Oil

TABLE
 Gulf Colville Delta State #1
 N. Slope Alaska

<u>DEPTH OR SPL. NO.</u>	<u>LOW-GRAY Ro MEAN</u>	<u>% POP.</u>	<u>FIRST HIGH-GRAY Ro MEAN</u>	<u>% POP.</u>	<u>TAI</u>	<u>THERMAL MATURITY</u>	<u>KEROGEN TYPE</u>	<u>HYDROCARBON POTENTIAL/REMARKS</u>
8610'	-	-	-	-	-	-	-	- - -
8830'	52	14	1.13	56	1+,2+	Transi- tionally mature	Type II-III	Marginal Gas/0 ⁺
8964'	-	-	-	-	-	-	-	
8984'	-	-	-	-	-	-	-	
9100'	50	9	1.14	81	1+,2+	-	-	
9200' (T.D.)	50	7	1.23	71	1+-2+	-	Type IV	No source

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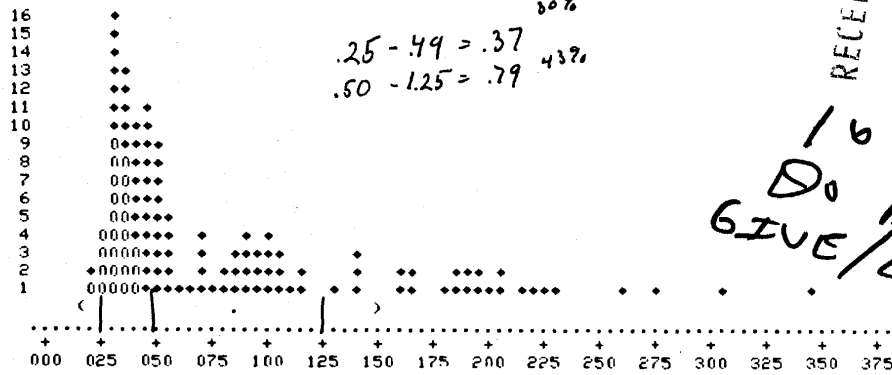
(Part of June 23, 1982 report)

R_o Histograms (original - do not give out)

MATURATION STUDIES - Gulf #1 Colville Delta State -

06/14/82 20305 50 320' 4 GULF #1 COLVILLE DELTA STATE+N.SLOPE

N = 125
 MEAN = 86
 STD. ERR. = 11
 STD. DEV. = 67
 PCT. POP. = 100



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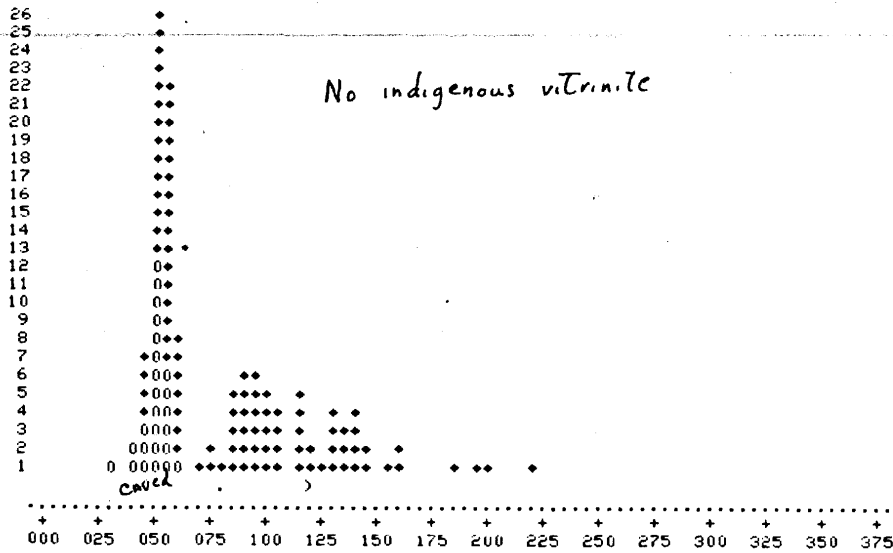
JUL 12 1982

Alaska Oil & Gas Cons. Commission
Anchorage

16 P.
Do NOT
GIVE/LOAN
OUT!

06/14/82 20306 50 930' 4 GULF #1 COLVILLE DELTA STATE+N.SLOPE

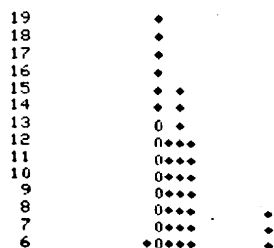
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 MEAN = 84
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 STD. DEV. = 39
 PCT. POP. = 99



No indigenous vitrinite

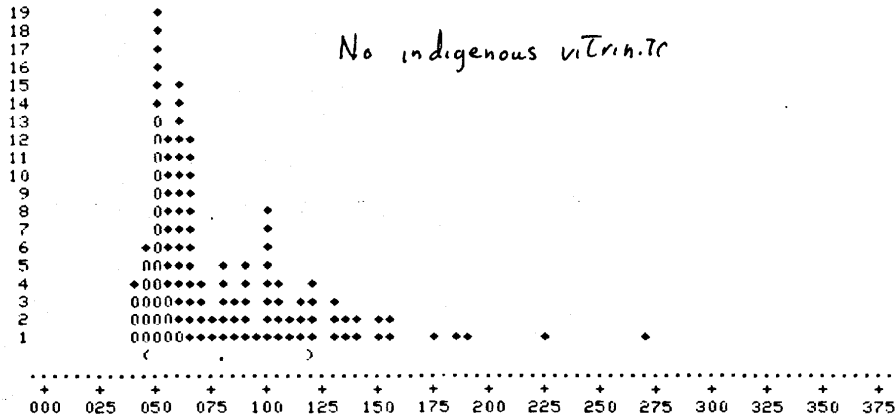
06/14/82 20307 50 1440' 4 GULF #1 COLVILLE DELTA STATE+N.SLOPE

N = 125
 MEAN = 84
 STD. ERR. = 6
 STD. DEV. = 39
 PCT. POP. = 100



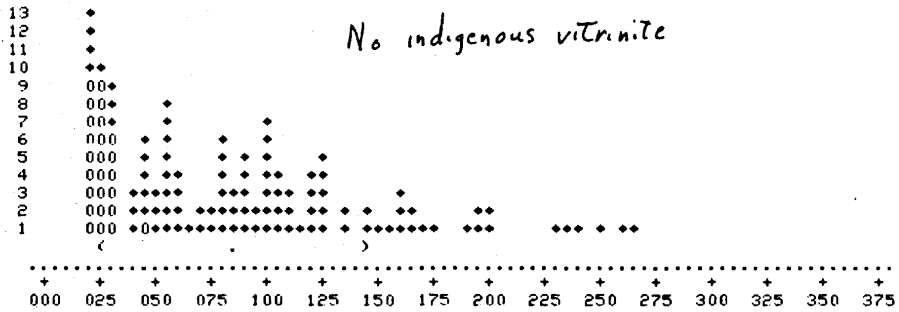
No indigenous vitrinite

STD. DEV. = 39
 PCT. POP. = 100



06/14/82 20308 50 2130' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

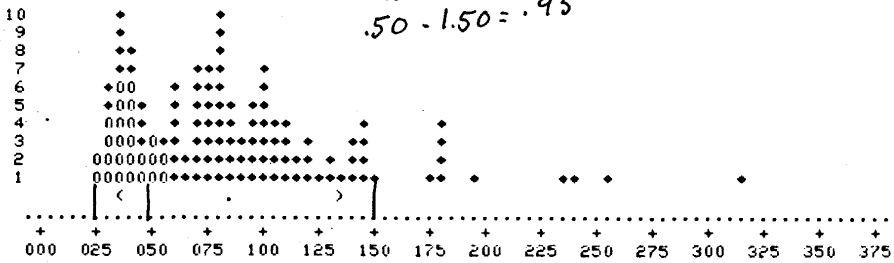
N = 125
 MEAN = 89
 STD. ERR. = 10
 STD. DEV. = 60
 PCT. POP. = 100



06/14/82 20309 50 2440' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 124
 MEAN = 89
 STD. ERR. = 8
 STD. DEV. = 50
 PCT. POP. = 99

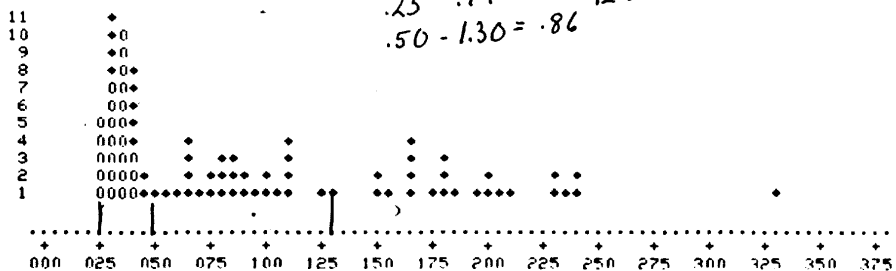
$.25 - .49 = .38$ 11%
 $.50 - 1.50 = .93$ 77%



06/14/82 20310 50 2620' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

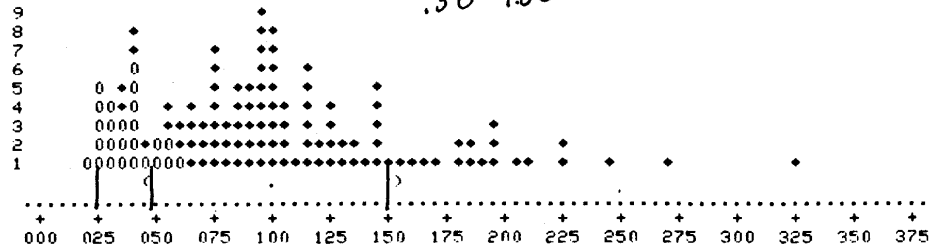
N = 87
 MEAN = 95
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 STD. DEV. = 69
 PCT. POP. = 96

$.25 - .49 = .35$ 17%
 $.50 - 1.30 = .86$ 42%



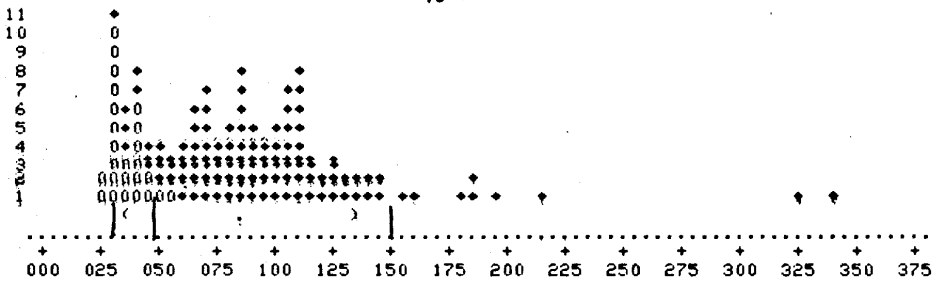
N = 125
MEAN = 101
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STD. DEV. = 56
PCT. POP. = 100

$.25 - .49 = .36$ 5%
 $.50 - 1.50 = .97$ 75%



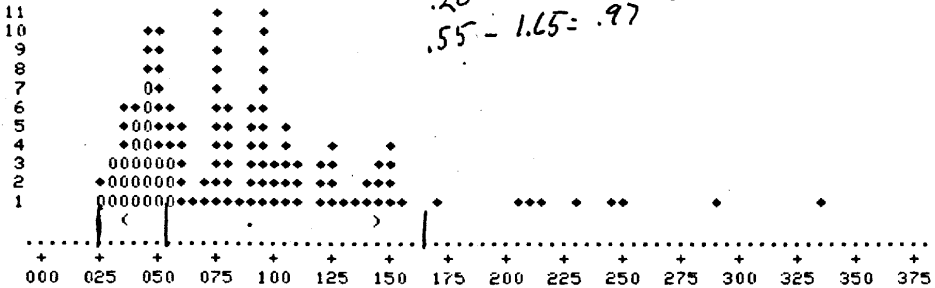
N = 126
MEAN = 88
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STD. DEV. = 50
PCT. POP. = 100

$.30 - .49 = .37$ 7%
 $.50 - 1.50 = .93$ 83%



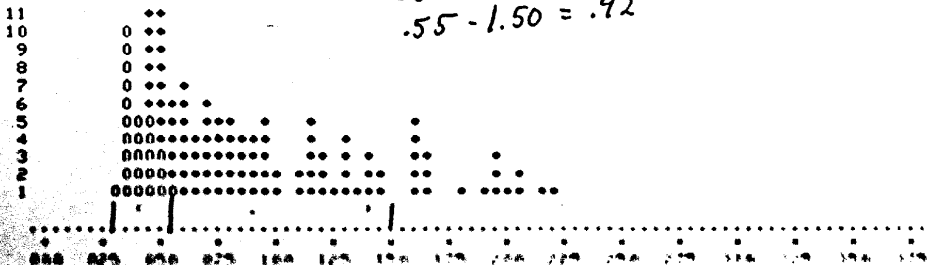
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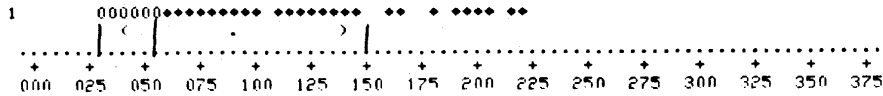
$.25 - .54 = .43$ 15%
 $.55 - 1.65 = .97$ 76%



N = 125
MEAN = 91
STD. ERR. = 8
STD. DEV. = 49
PCT. POP. = 100

$.30 - .54 = .44$ 14%
 $.55 - 1.50 = .92$ 68%

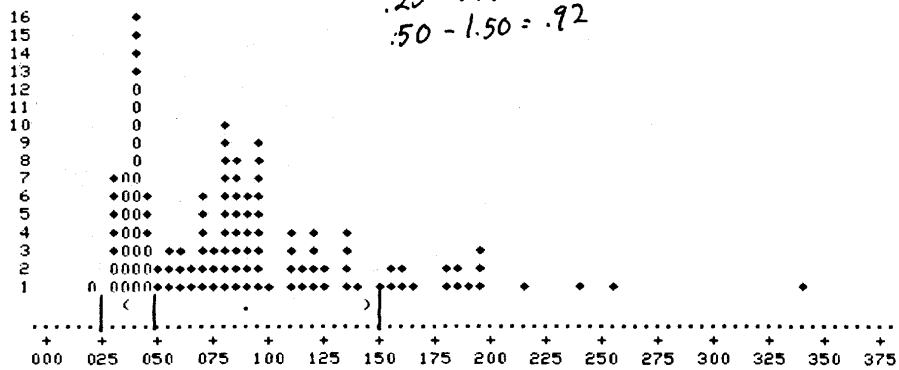




06/14/82 20315 50 5020' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 125
 MEAN = 91
 STD. ERR. = 9
 STD. DEV. = 54
 PCT. PDP. = 100

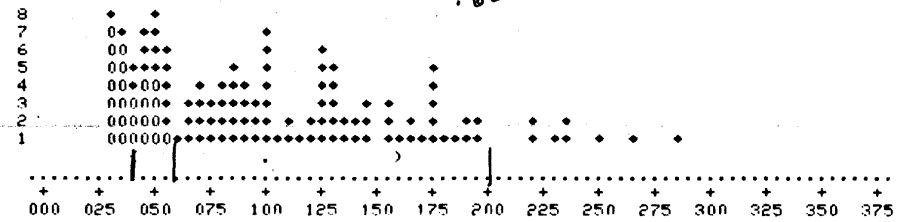
$.25 - .49 = .39$ 12%
 $.50 - 1.50 = .92$ 71%



06/14/82 20316 50 5950' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 125
 MEAN = 103
 STD. ERR. = 10
 STD. DEV. = 59
 PCT. PDP. = 100

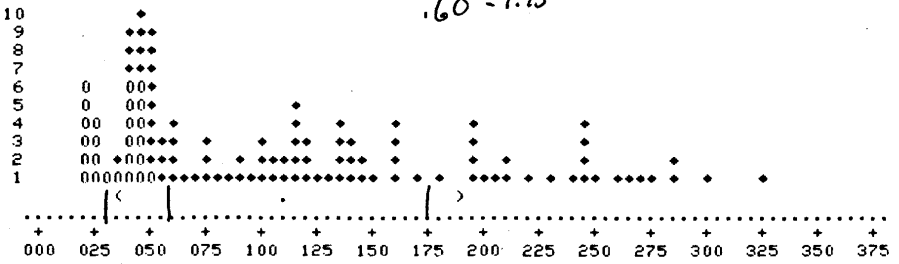
$.40 - .59 = .49$ 17%
 $.60 - 2.00 = 1.20$ 72%



06/14/82 20317 50 6030' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 115
 MEAN = 114
 STD. ERR. = 14
 STD. DEV. = 78
 PCT. PDP. = 100

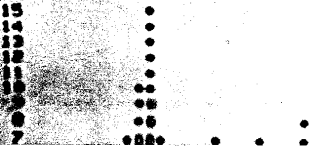
$.30 - .59 = .47$ 21%
 $.60 - 1.75 = 1.14$ 51%

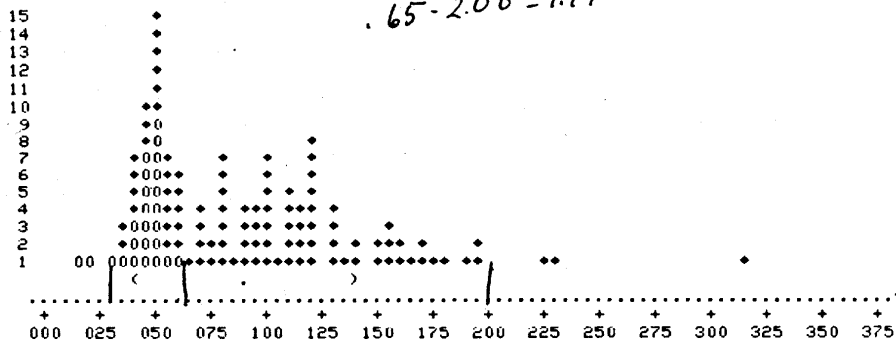


06/14/82 20318 50 6120' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 124
 MEAN = 92
 STD. ERR. = 8
 STD. DEV. = 49
 PCT. PDP. = 99

$.30 - .64 = .50$ 26%
 $.65 - 2.06 = 1.17$ 70%

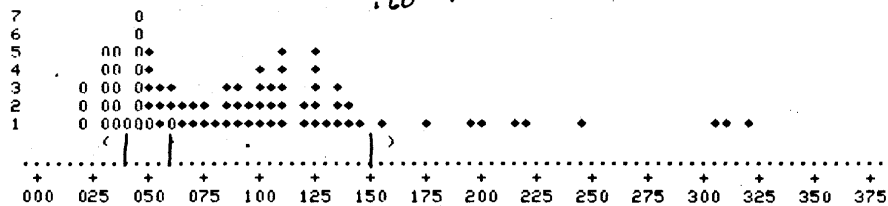




06/14/82 20319 50 6200' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 83
 MEAN = 98
 STD. ERR. = 13
 STD. DEV. = 64
 PCT. POP. = 100

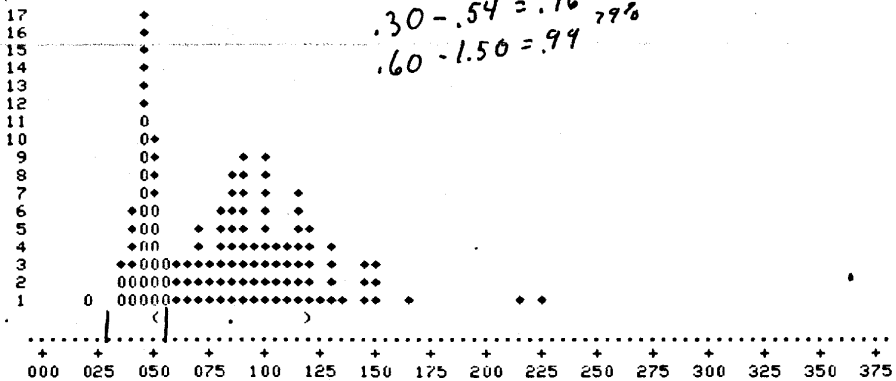
$.40 - .59 = .50$ 11%
 $.60 - 1.50 = 1.03$ 71%



06/14/82 20320 50 6280' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 125
 MEAN = 86
 STD. ERR. = 6
 STD. DEV. = 36
 PCT. POP. = 100

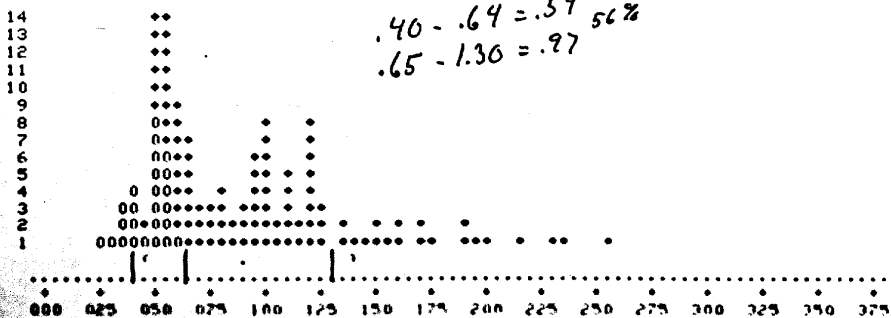
$.30 - .54 = .46$ 15%
 $.60 - 1.50 = .94$ 79%

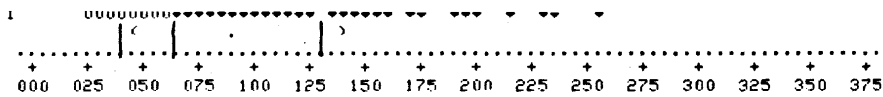


06/14/82 20321 50 6360' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 124
 MEAN = 93
 STD. ERR. = 8
 STD. DEV. = 47
 PCT. POP. = 99

$.40 - .64 = .54$ 23%
 $.65 - 1.30 = .97$ 56%

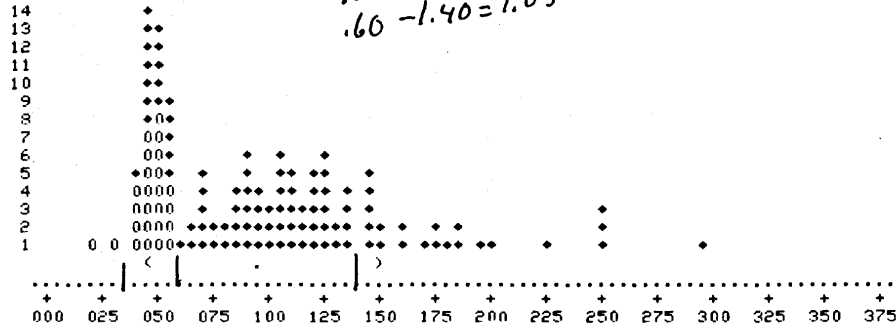




06/14/82 20322 50 6440' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 125
 MEAN = 99
 STD. ERR. = 9
 STD. DEV. = 52
 PCT. PDP. = 100

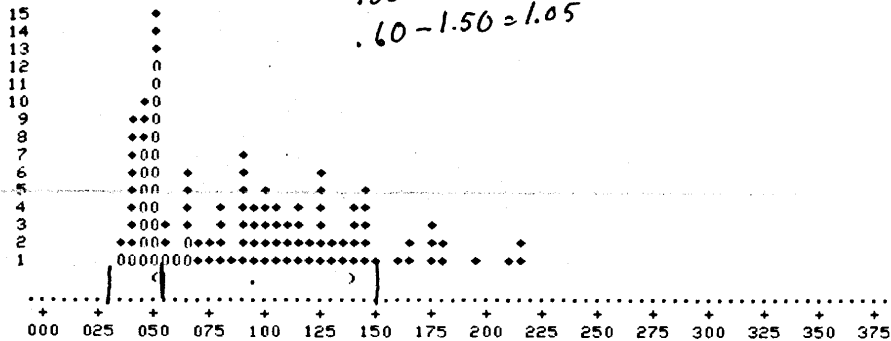
$.35 - .59 = .50$ 18%
 $.60 - 1.40 = 1.03$ 60%



06/14/82 20323 50 6520' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 116
 MEAN = 95
 STD. ERR. = 8
 STD. DEV. = 45
 PCT. PDP. = 100

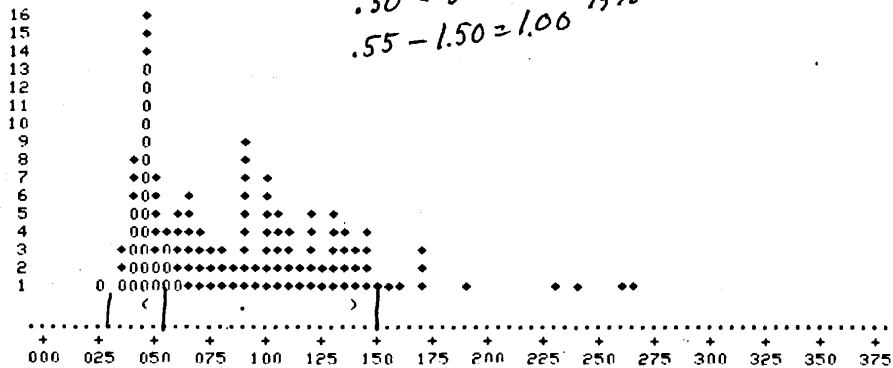
$.30 - .59 = .48$ 18%
 $.60 - 1.50 = 1.05$ 62%



06/14/82 20324 50 6600' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 125
 MEAN = 93
 STD. ERR. = 8
 STD. DEV. = 47
 PCT. PDP. = 100

$.30 - .54 = .45$ 13%
 $.55 - 1.50 = 1.00$ 75%

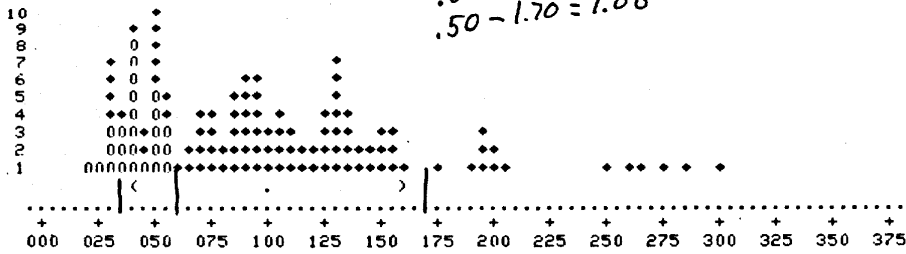


06/14/82 20325 50 6680' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

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 MEAN = 102
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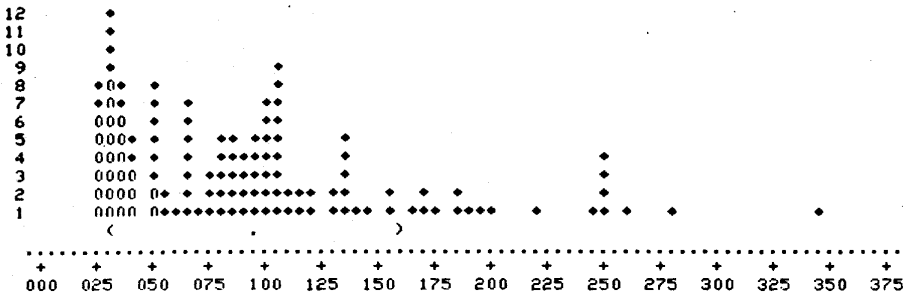
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MEAN = 102
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STD. DEV. = 40
PCT. POP. = 99

$.35 - .59 = .47$ 11%
 $.50 - 1.70 = 1.00$ 77%



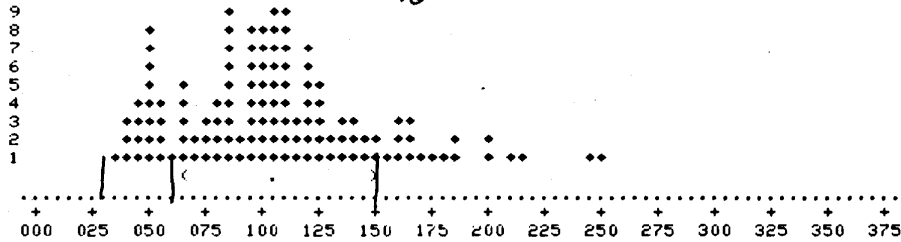
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PCT. POP. = 100

No indigenous



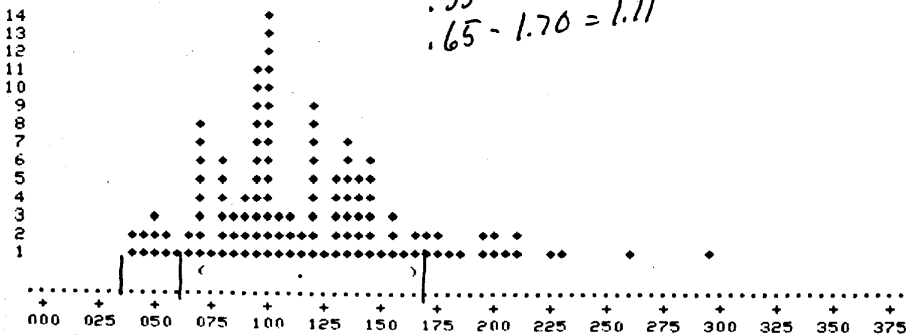
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STD. DEV. = 43
PCT. POP. = 100

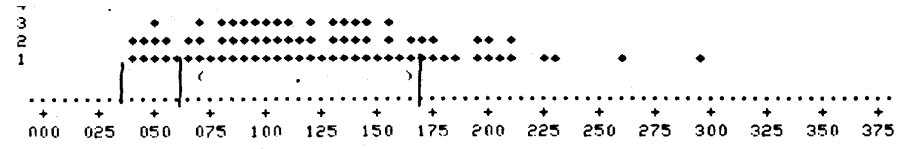
$.30 - .59 = .56$ 16%
 $.60 - 1.50 = 1.04$ 68%



N = 124
MEAN = 119
STD. ERR. = 8
STD. DEV. = 46
PCT. POP. = 99

$.35 - .64 = .51$ 8%
 $.65 - 1.70 = 1.11$ 77%

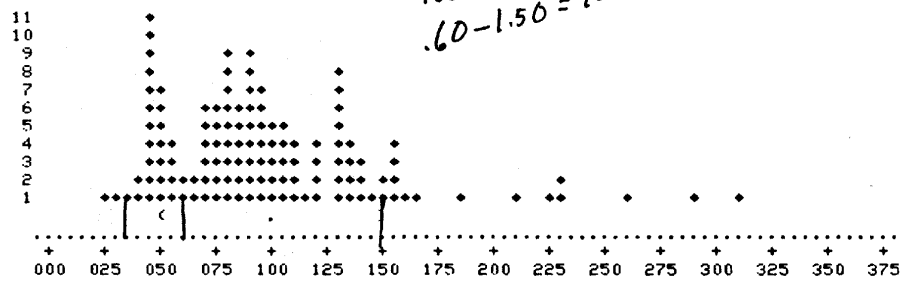




06/14/82 20329 50 7000' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 125
 MEAN = 101
 STD. ERR. = 8
 STD. DEV. = 50
 PCT. POP. = 100

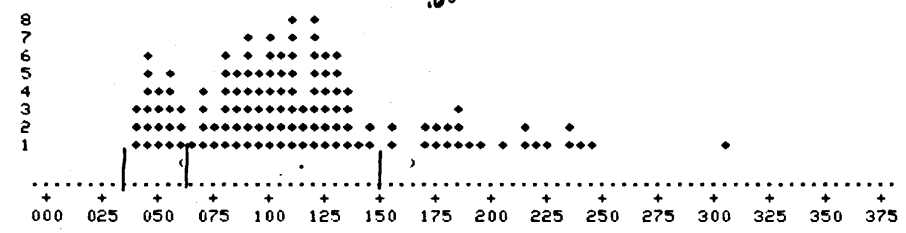
$.35 - .59 = 48$ 20%
 $.60 - 1.50 = 1.00$ 60%



06/14/82 20330 50 7080' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 125
 MEAN = 115
 STD. ERR. = 9
 STD. DEV. = 51
 PCT. POP. = 100

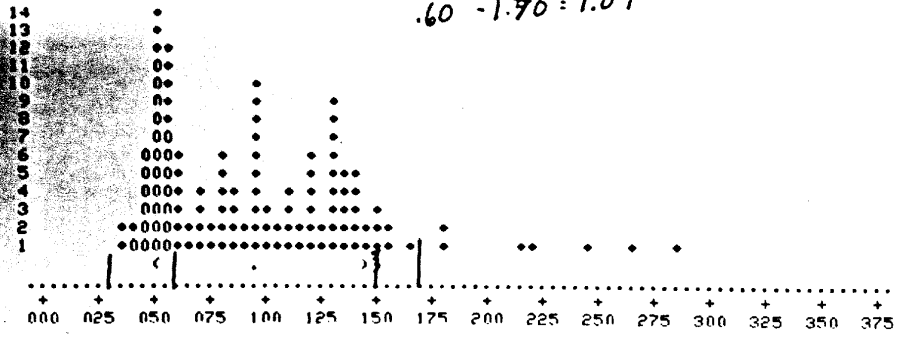
$.35 - .64 = .52$ 16%
 $.65 - 1.50 = 1.07$ 64%



06/14/82 20331 50 7160' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 125
 MEAN = 99
 STD. ERR. = 8
 STD. DEV. = 47
 PCT. POP. = 100

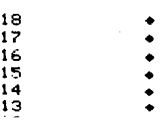
$.30 - .59 = .51$ 17%
 $.60 - 1.70 = 1.09$ 92%

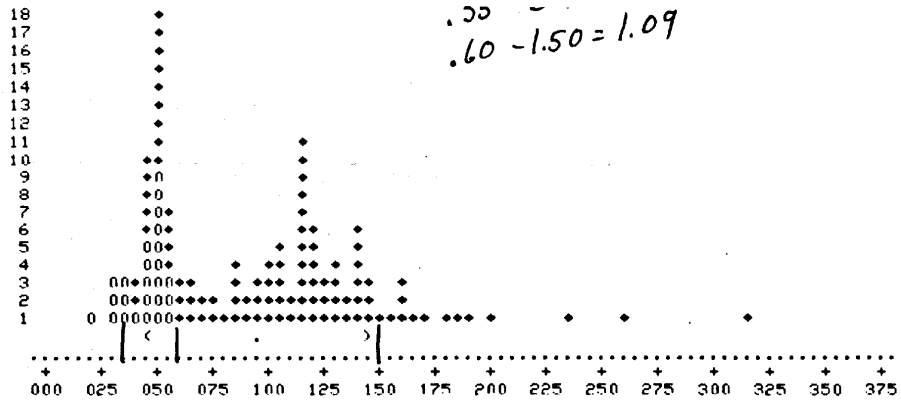


06/14/82 20332 50 7240' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 125
 MEAN = 97
 STD. ERR. = 8
 STD. DEV. = 50
 PCT. POP. = 100

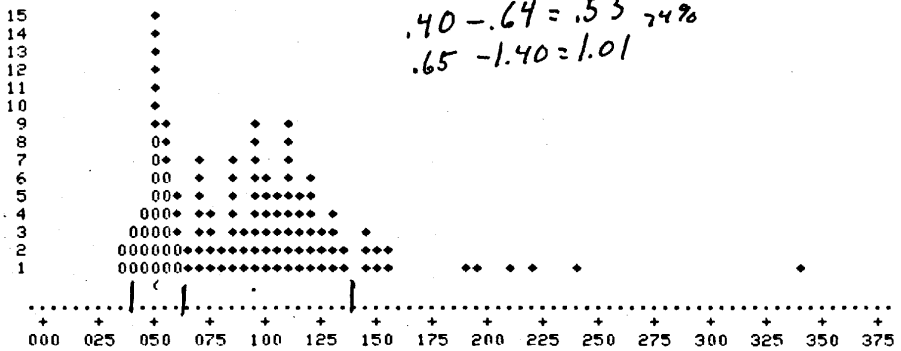
$.35 - .59 = .50$ 20%
 $.60 - 1.50 = 1.09$ 66%





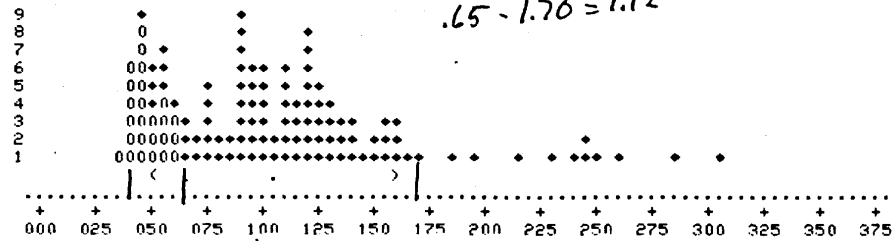
06/14/82 20333 50 7300' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 125
MEAN = 95
STD. ERR. = 8
STD. DEV. = 45
PCT. POP. = 100



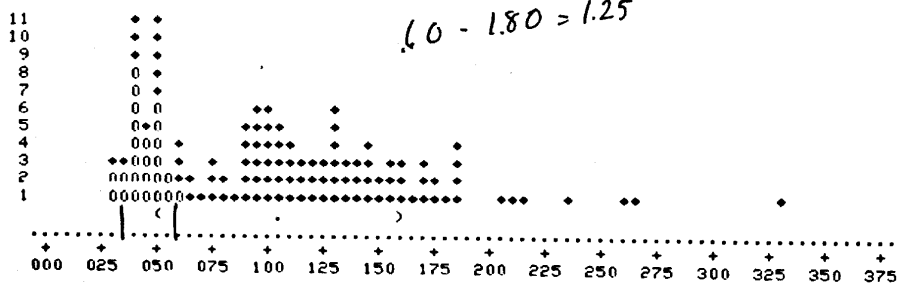
06/14/82 20334 50 7350' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

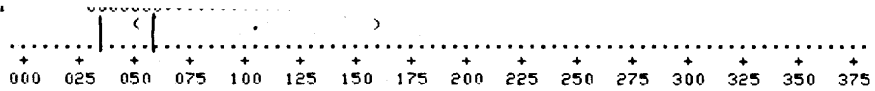
N = 125
MEAN = 108
STD. ERR. = 9
STD. DEV. = 55
PCT. POP. = 100



06/14/82 20335 50 7400' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 125
MEAN = 107
STD. ERR. = 9
STD. DEV. = 56
PCT. POP. = 100

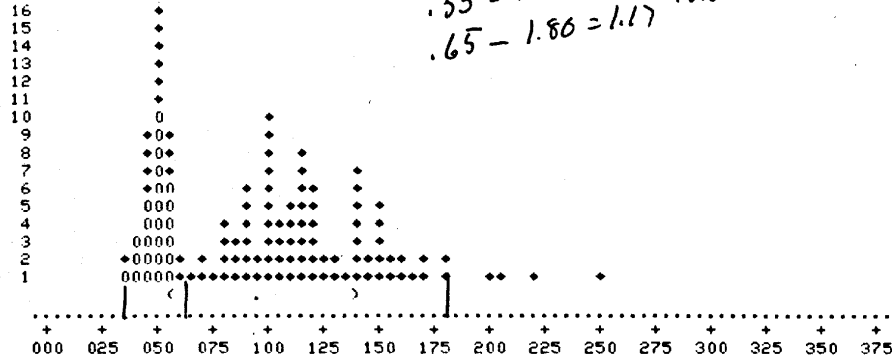




06/14/82 20336 50 7450' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 125
 MEAN = 99
 STD. ERR. = 7
 STD. DEV. = 44
 PCT. POP. = 100

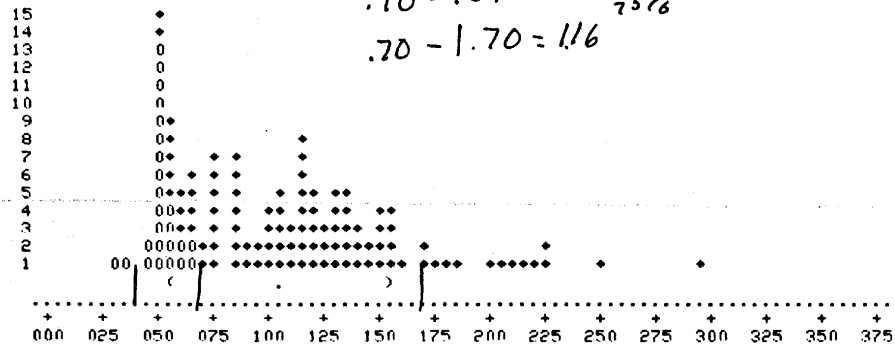
$.35 - .64 = .50$ 16%
 $.65 - 1.80 = 1.17$ 78%



06/14/82 20337 50 7500' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 125
 MEAN = 107
 STD. ERR. = 8
 STD. DEV. = 50
 PCT. POP. = 100

$.40 - .69 = .56$ 14%
 $.70 - 1.70 = 1.16$ 73%



06/14/82 20338 50 7550' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 124
 MEAN = 113
 STD. ERR. = 10
 STD. DEV. = 60
 PCT. POP. = 99

$.30 - .59 = .50$ 7%
 $.60 - 1.50 = 1.03$ 16%



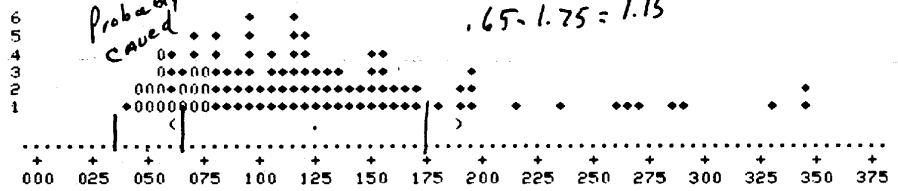
06/14/82 20339 50 7620' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 104
 MEAN = 120
 STD. ERR. = 12
 STD. DEV. = 65
 PCT. POP. = 96

$.35 - .64 = .46$
 $1.15 - 1.15 = 0$

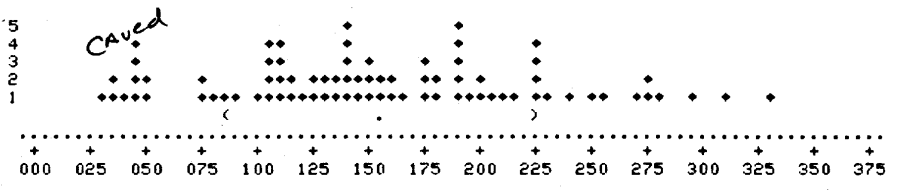
N = 104
 MEAN = 128
 STD. ERR. = 12
 STD. DEV. = 65
 PCT. PDP. = 96

$.35 - .64 = .46$
 $.65 - 1.75 = 1.15$



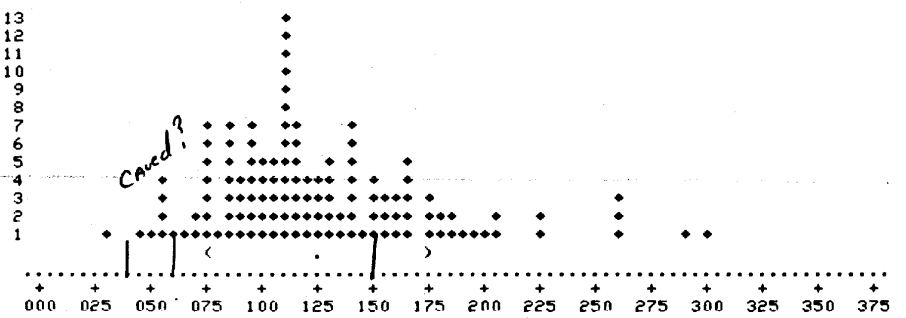
06/14/82 20340 50 7650' 2 GULF #1 COLVILLE DELTA STATE+N.SLOPE

N = 79
 MEAN = 155
 STD. ERR. = 15
 STD. DEV. = 70
 PCT. PDP. = 97



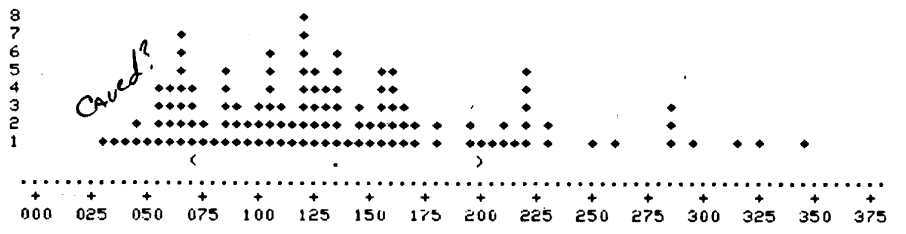
06/14/82 20341 50 7710' 4 GULF #1 COLVILLE DELTA STATE+N.SLOPE

N = 124
 MEAN = 127
 STD. ERR. = 8
 STD. DEV. = 49
 PCT. PDP. = 99



06/14/82 20342 50 7760' 4 GULF #1 COLVILLE DELTA STATE+N.SLOPE

N = 121
 MEAN = 136
 STD. ERR. = 11
 STD. DEV. = 66
 PCT. PDP. = 96



06/14/82 20343 50 7800' 4 GULF #1 COLVILLE DELTA STATE+N.SLOPE

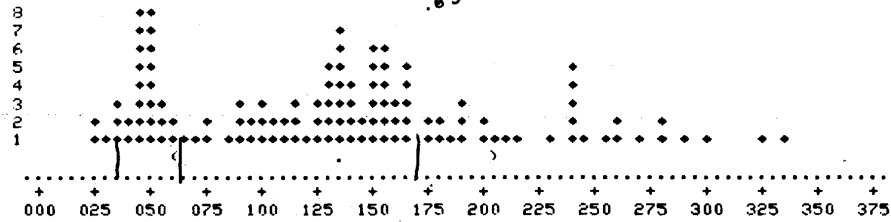
N = 121
 MEAN = 136
 STD. ERR. = 12
 STD. DEV. = 72
 PCT. PDP. = 96

$.35 - .64 = .53$ ^{10%}
 $.65 - 1.70 = 1.17$ ^{6%}



STD. DEV. = 72
PCT. POP. = 96

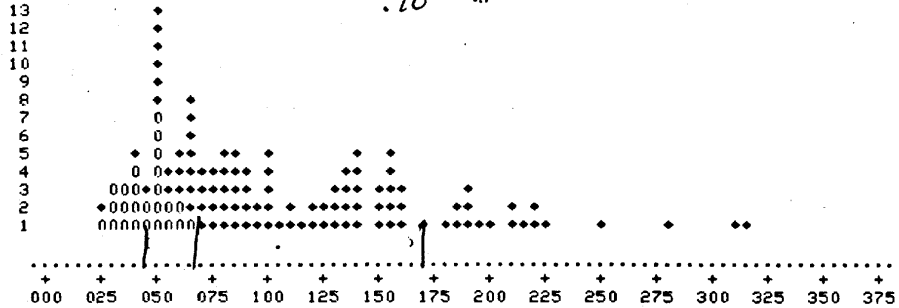
$.65 - 1.70 = 1.17$



06/14/82 20344 50 7800' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 125
MEAN = 106
STD. ERR. = 10
STD. DEV. = 61
PCT. POP. = 100

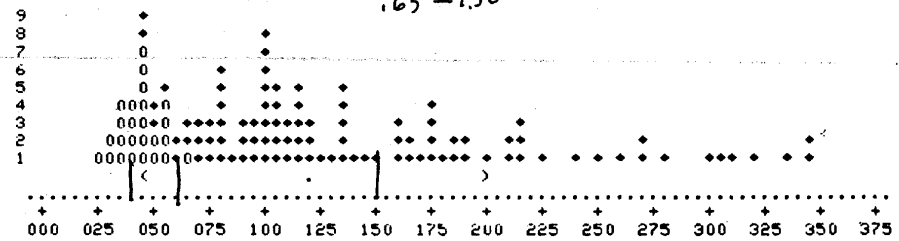
$.45 - .69 = .57$ 11%
 $.70 - 1.70 = 1.13$ 60%



06/14/82 20345 50 7850' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 122
MEAN = 124
STD. ERR. = 13
STD. DEV. = 77
PCT. POP. = 97

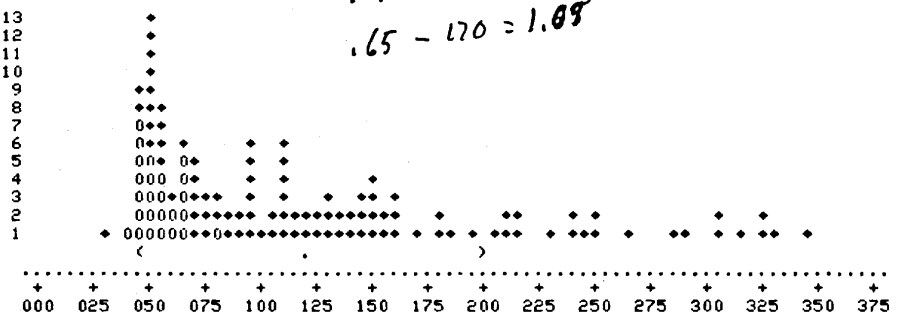
$.40 - .64 = .50$ 7%
 $.65 - 1.50 = 1.03$ 55%



06/14/82 20346 50 7890' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 122
MEAN = 123
STD. ERR. = 13
STD. DEV. = 78
PCT. POP. = 97

$.40 - .64 = .52$ 15%
 $.65 - 1.70 = 1.05$ 55%



06/14/82 20347 50 8016' 2 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 125
MEAN = 37

N = 125
 MEAN = 37
 STD. ERR. = 0
 STD. DEV. = 4
 PCT. POP. = 100

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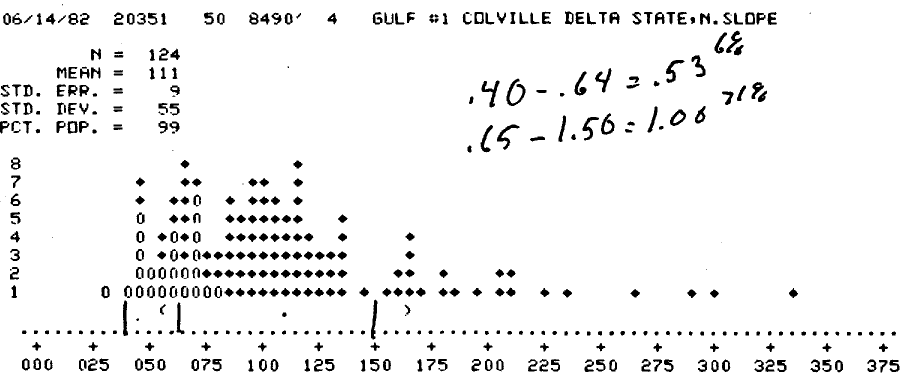
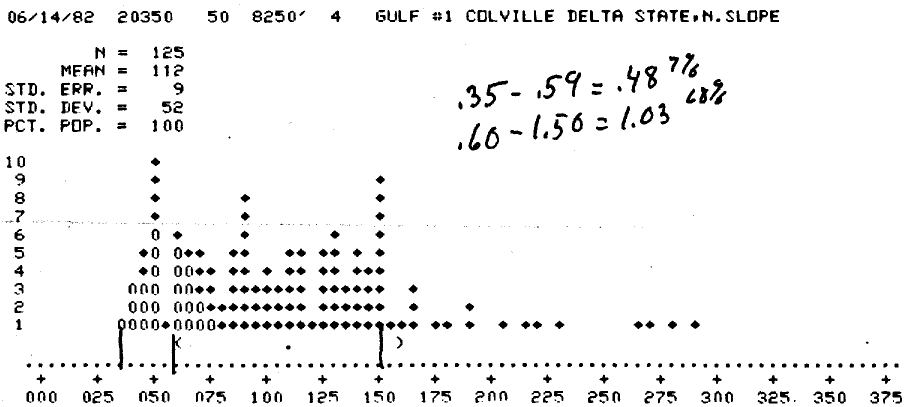
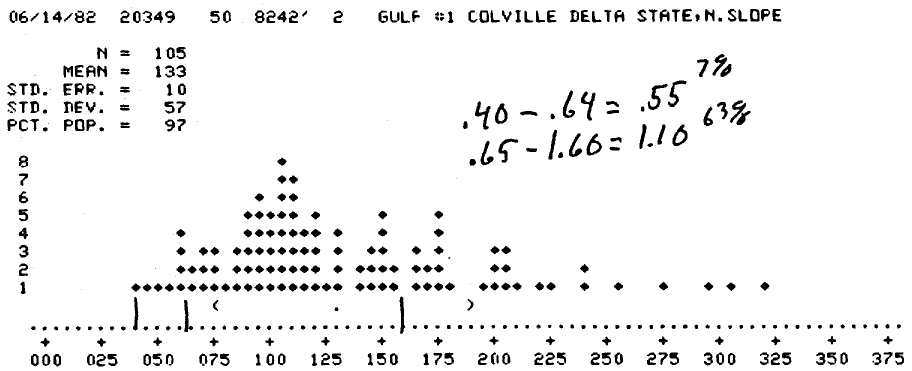
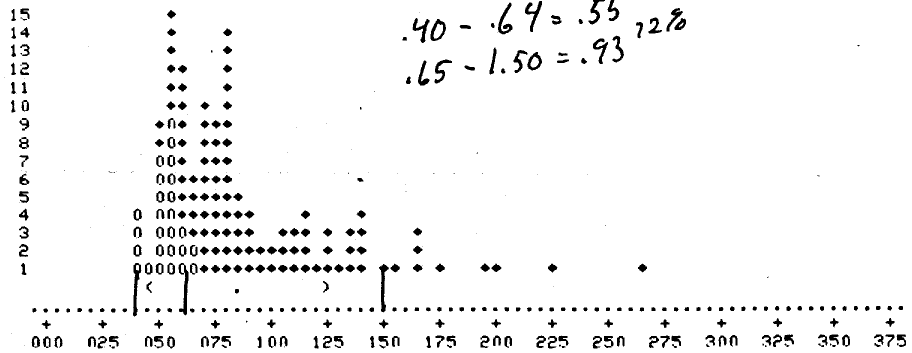
Contamination ?

.....
 + 000 + 025 + 050 + 075 + 100 + 125 + 150 + 175 + 200 + 225 + 250 + 275 + 300 + 325 + 350 + 375

N = 125
 MEAN = 88
 STD. ERR. = 6
 STD. DEV. = 39
 PCT. POP. = 100

15 ♦
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 13 ♦ ♦
 12 ♦♦ ♦
 11 ♦♦ ♦
 10 ♦♦ ♦
 9 ♦♦♦ ♦♦
 8 ♦♦♦ ♦♦

.40 - .64 = .55^{17%}
.65 - 1.50 = .93^{72%}



06/14/82 20352 50 8610' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

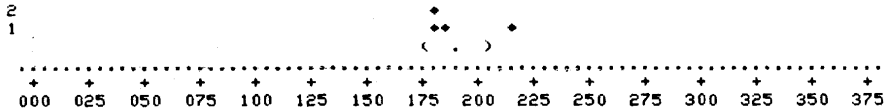
N = 4
 MEAN = 193
 STD. ERR. = 13
 STD. DEV. = 14
 PCT. POP. = 100

No indigenous vitrimite

06/14/82 20352 50 8610' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 4
MEAN = 193
STD. ERR. = 13
STD. DEV. = 14
PCT. POP. = 100

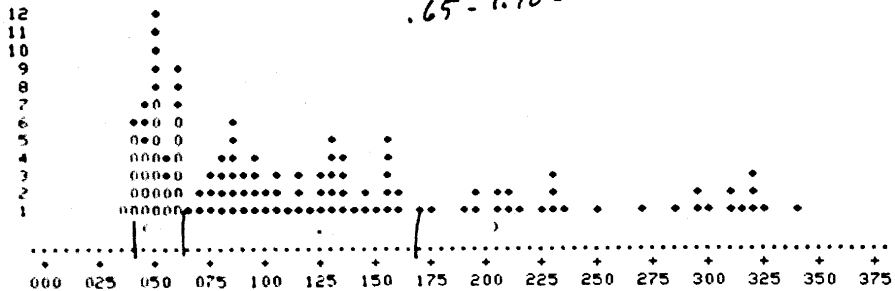
No indigenous vitrinite



06/14/82 20353 50 8830' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 124
MEAN = 127
STD. ERR. = 14
STD. DEV. = 82
PCT. POP. = 99

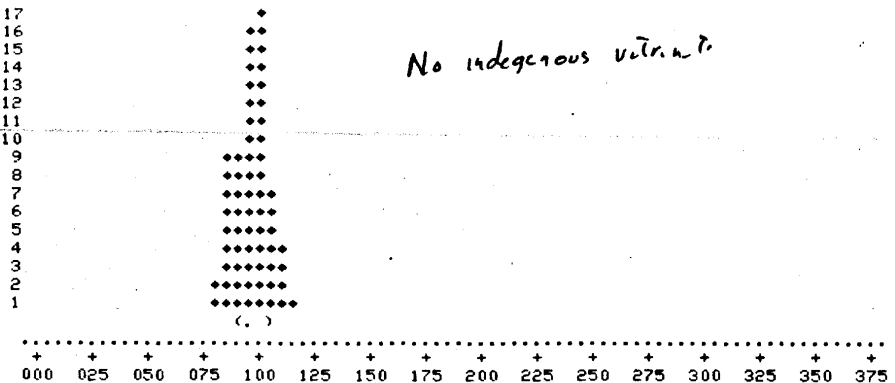
*.40 - .64 = 52^{14%}
.65 - 1.70 = 113⁵⁶*



06/14/82 20354 50 8964' 2 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 65
MEAN = 98
STD. ERR. = 1
STD. DEV. = 7
PCT. POP. = 100

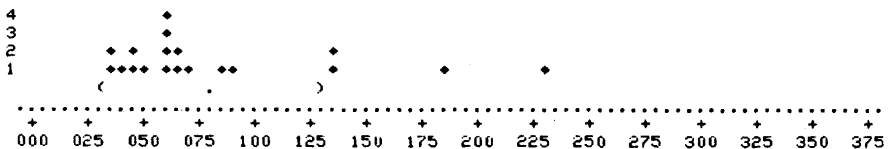
No indigenous vitrinite



06/14/82 20355 50 8984' 2 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 19
MEAN = 83
STD. ERR. = 23
STD. DEV. = 51
PCT. POP. = 100

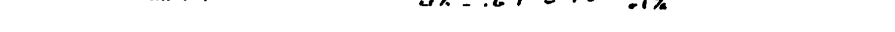
1454 FF. spl.



06/14/82 20356 50 9100' 4 GULF #1 COLVILLE DELTA STATE,N.SLOPE

N = 125
MEAN = 113
STD. ERR. = 8
STD. DEV. = 50
PCT. POP. = 100

.44 - .64 = .50^{2%}



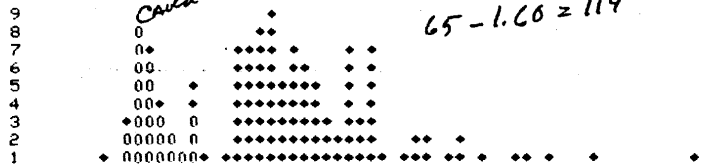
000 025 050 075 100 125 150 175 200 225 250 275 300 325 350 375

06/14/82 20356 50 9100' 4 GULF #1 COLVILLE DELTA STATE+N.SLOPE

N = 125
MEAN = 113
STD. ERR. = 8
STD. DEV. = 50
PCT. POP. = 100

Caused?

$.46 - .64 = .50$ 2%
 $65 - 1.60 = 114$ 11%



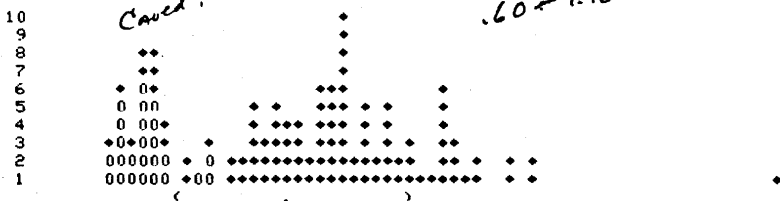
000 025 050 075 100 125 150 175 200 225 250 275 300 325 350 375

06/14/82 20357 50 9200' 4 GULF #1 COLVILLE DELTA STATE+N.SLOPE

N = 125
MEAN = 114
STD. ERR. = 9
STD. DEV. = 54
PCT. POP. = 100

Caused?

$.45 - .64 = .50$ 71%
 $.60 - 1.70 = 1.23$



000 025 050 075 100 125 150 175 200 225 250 275 300 325 350 375

♦♦COMMAND =