

••COMMAND = LD
••FIRST SAMPLE NO. = 18715
••LAST SAMPLE NO. = 18742
••LOAD NUMBER = LT

1 18715 50 1300 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
2 18716 50 4500 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
3 18717 50 5000 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
4 18718 50 1000 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
5 18719 50 1500 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
6 18720 50 1400 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
7 18721 50 2500 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
8 18722 50 27400 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
9 18723 50 5100 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
10 18724 50 5400 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
11 18725 50 2000 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
12 18726 50 4100 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
13 18727 50 4540 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
14 18728 50 4400 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
15 18729 50 5820 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
16 18730 50 5820 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
17 18731 50 5820 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
18 18732 50 5340 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
19 18733 50 5170 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
20 18734 50 7060 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
21 18735 50 7420 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
22 18736 50 7780 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
23 18737 50 2140 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
24 18738 50 5320 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
25 18739 50 5000 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
26 18740 50 5020 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
27 18741 50 7705 4 STANDARD OF CALIF.CAPE ET PENREP601.BK
28 18742 50 8361 4 STANDARD OF CALIF.CAPE ET PENREP601.BK

••COMMAND = LD
••FIRST SAMPLE NO. = 18715
••LAST SAMPLE NO. = 18742
••LOAD NUMBER = LT

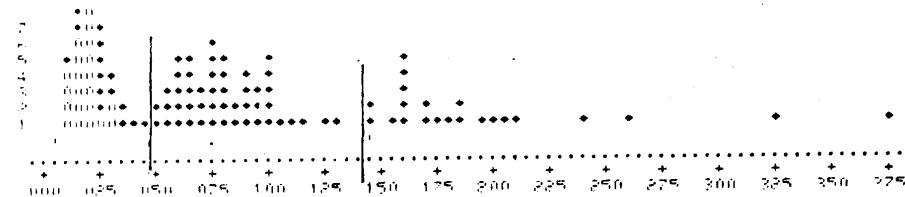
11 13 11 18715 50 1300 4 STANDARD OF CALIF.CAPE ET PENREP601.BK

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TH100, PDP100 = 1.0

$$000 - 049 = \underline{0.22} \quad (28\%)$$

$$050 - 144 = 0.81 \quad (78\%)$$

$$145 - 375 = 1.89 \quad (21\%)$$



11 13 11 18716 50 4500 4 STANDARD OF CALIF.CAPE ET PENREP601.BK

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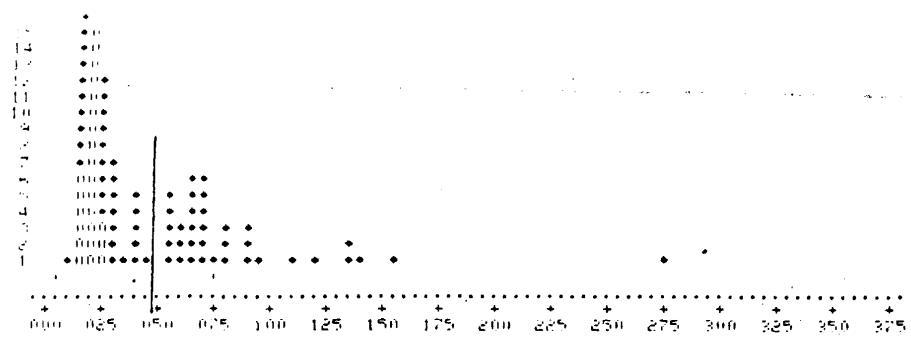
$$000 - 049 = \underline{0.23} \quad (65\%)$$

$$050 - 375 = 0.87 \quad (35\%)$$

ORIGINAL

NOV 3 0 1981

RECEIVED
Alaska Oil & Gas Cons. Commission
Anchorage

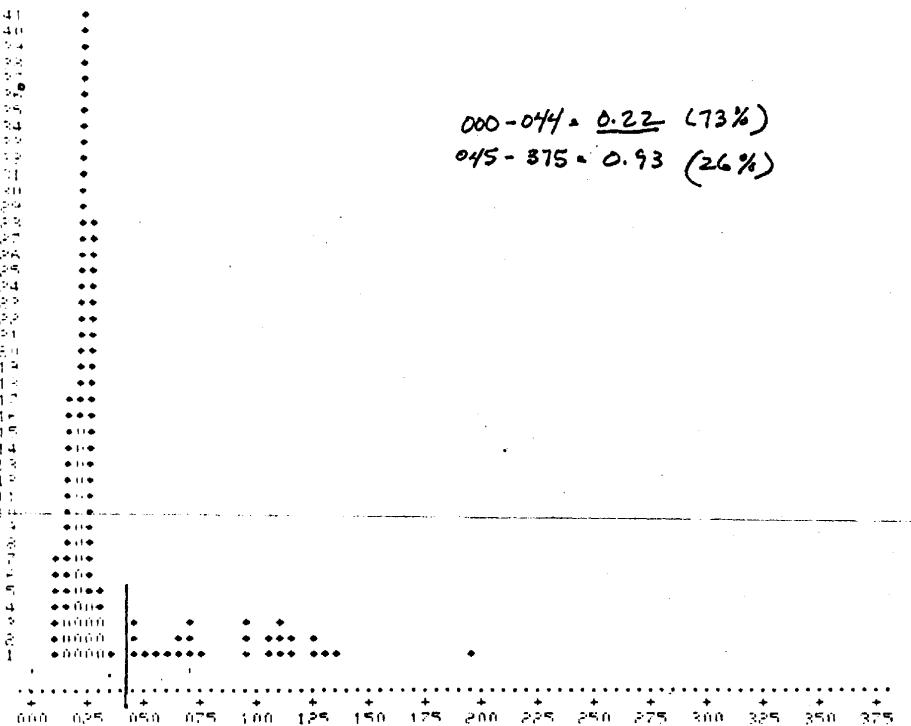


11-13-81 18717 50 8501 4 STANDARD OF FAULT, CAPE EISCHENBERG, AR

$N = 126$
MEAN = 0.7
STD. ERR. = .5
STD. DEVI. = .33
PCT. FDP. = 100

$$000 - 044 = \underline{0.22} (73\%)$$

$$045 - 375 = 0.93 (26\%)$$

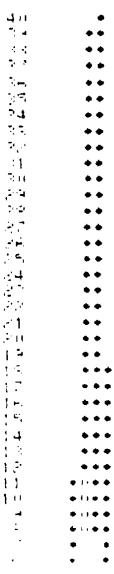


11-13-81 18718 50 12107 4 STANDARD OF FAULT, CAPE EISCHENBERG, AR

$N = 126$
MEAN = 0.8
STD. ERR. = .2
STD. DEVI. = .14
PCT. FDP. = 100

$$000 - 049 = \underline{0.25} (92\%)$$

$$050 - 375 = 0.76 (8\%)$$



11-12-81 18714 50 15700 4 STANDARD OF CALIF. CAPT. EXPERIMENTAL

N = 167
 MEAN = 42
 STD. ERR. = 7
 STD. DEVI. = 40
 PCT. POP. = 100

$$\begin{aligned} 000-049 &= 0.26 \text{ (75\%)} \\ 050-375 &= 1.13 \text{ (24\%)} \end{aligned}$$

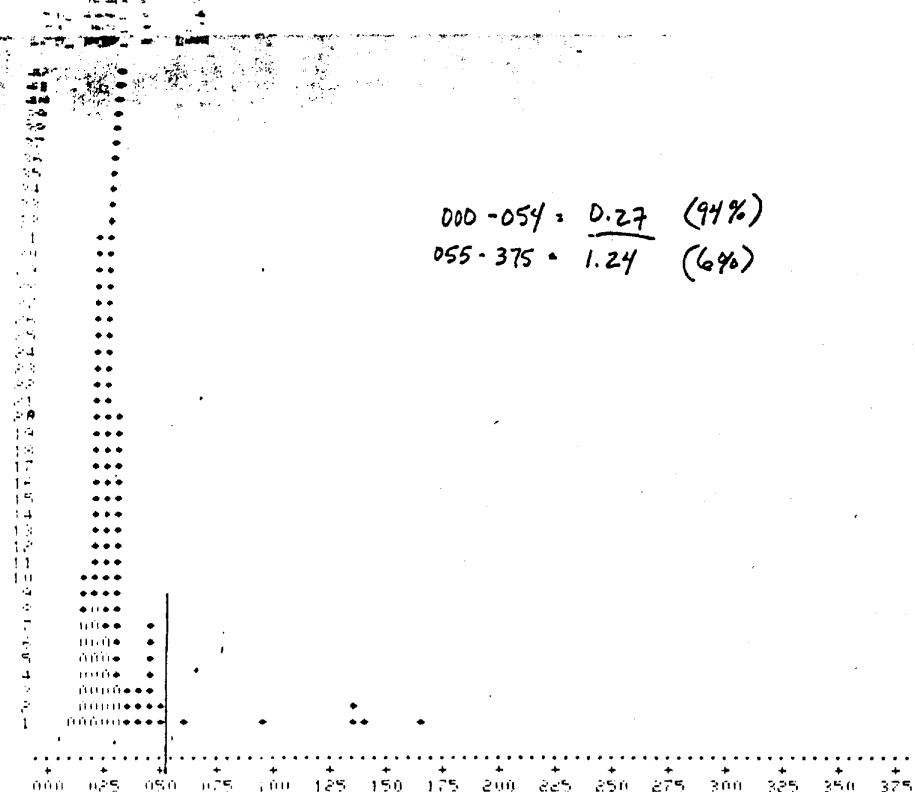
11-12-81 18720 50 19200 4 STANDARD OF CALIF. CAPT. EXPERIMENTAL

N = 125
 MEAN = 35
 STD. ERR. = 7
 STD. DEVI. = 41
 PCT. POP. = 100

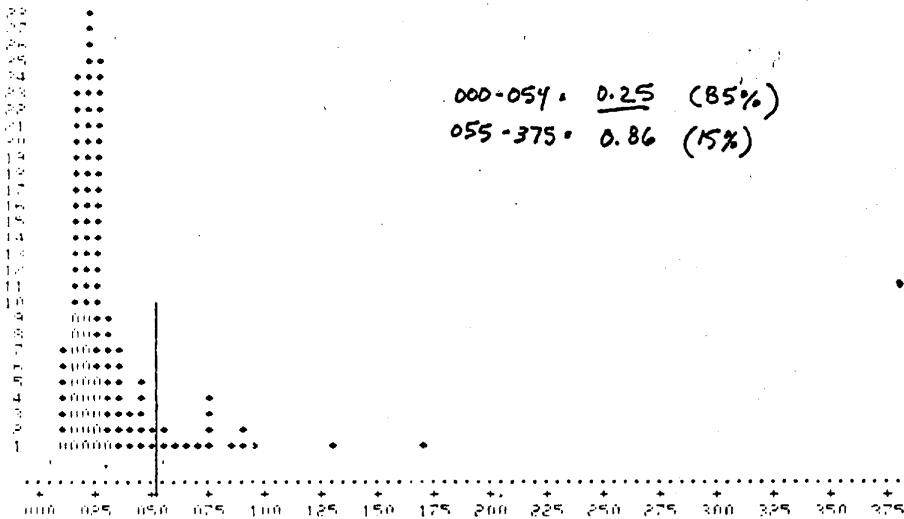
$$\begin{aligned} 000-049 &= 0.27 \text{ (89\%)} \\ 050-375 &= 1.28 \text{ (11\%)} \end{aligned}$$

11-12-81 18721 50 23200 4 STANDARD OF CALIF. CAPT. EXPERIMENTAL

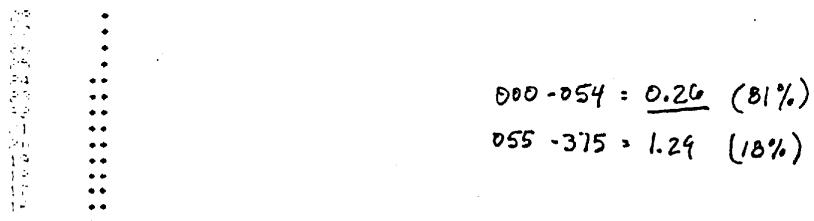
N = 125
 MEAN = 34
 STD. ERR. = 7
 STD. DEVI. = 40
 PCT. POP. = 100

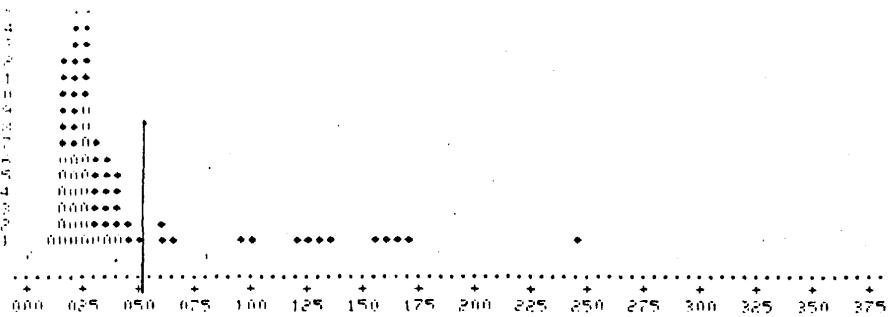


$n = 125$
 $N_{PDR} = 32$
 $STD. PDR_1 = .4$
 $STD. PDR_2 = .23$
 $ACT. PDR_1 = 1.60$



$n = 100$
 $N_{PDR} = 41$
 $STD. PDR_1 = .7$
 $STD. PDR_2 = .46$
 $ACT. PDR_1 = 1.00$



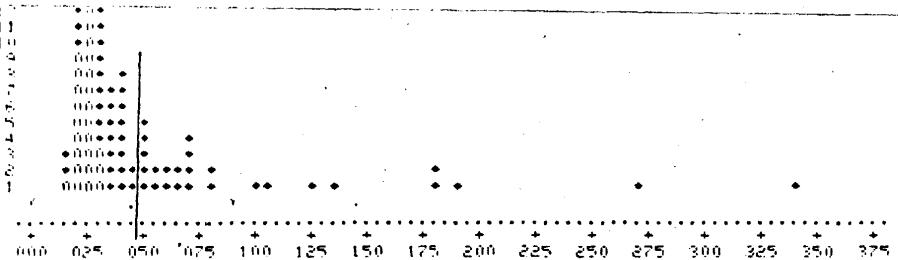


11-13-81 18724 50 348.07 4 STANDARD OF CALIF.CAPE ESPENBERG#1.AK

$N = 124$
MEAN = 45
STD. ERR. = 9
STD. DEV. = 45
C.V. PROP. = 22

$$000-050 = \underline{0.29} \quad (73\%)$$

$$050-375 = 1.05 \quad (26\%)$$

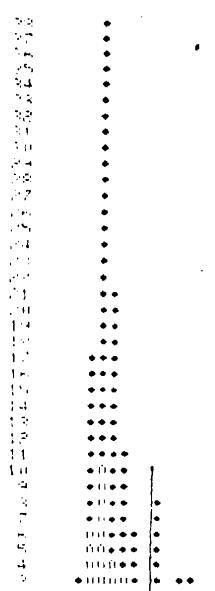


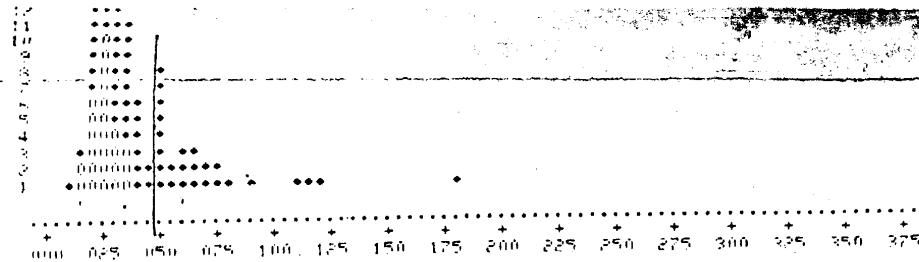
11-13-81 18725 50 382.01 4 STANDARD OF CALIF.CAPE ESPENBERG#1.AK

$N = 125$
MEAN = 45
STD. ERR. = 4
STD. DEV. = 23
C.V. PROP. = 100

$$000-049 = \underline{0.29} \quad (74\%)$$

$$050-375 = 0.74 \quad (26\%)$$

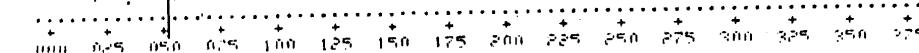




11-13-81 1872A 50 41800 4 STANDARD OF CALIF. CAPE ENTERPRISE INC.

N = 125
MEAN = 39
STD. ERR. = 3
STD. DEVI. = 18
PCT. POP. = 100

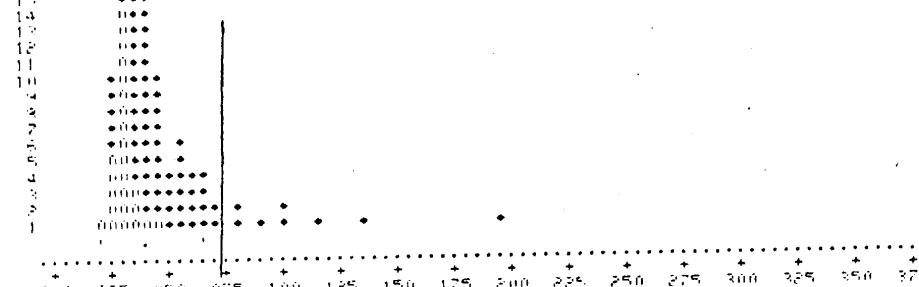
$$000 - 054 = \underline{0.34} \text{ (84\%)} \\ 055 - 375 = \underline{0.76} \text{ (16\%)}$$



11-13-81 1872T 50 49400 4 STANDARD OF CALIF. CAPE ENTERPRISE INC.

N = 125
MEAN = 44
STD. ERR. = 3
STD. DEVI. = 22
PCT. POP. = 100

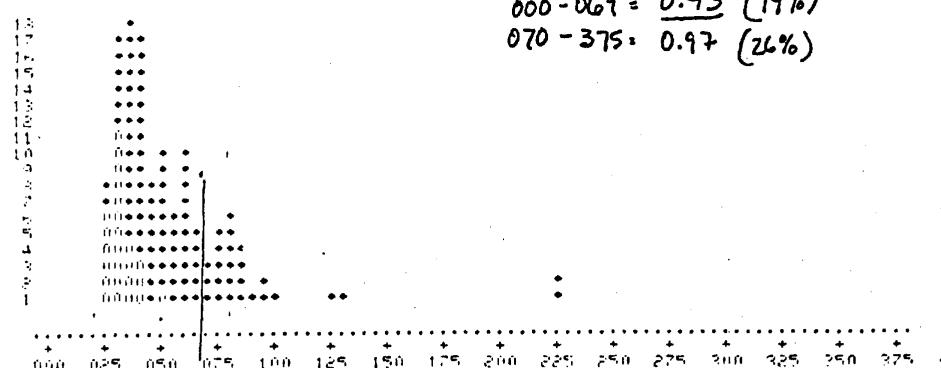
$$000 - 074 = \underline{0.40} \text{ (92\%)} \\ 075 - 375 = \underline{1.13} \text{ (8\%)}$$



11-13-81 18728 50 4900' 4 STANDARD OF CALIF.CAPE ESPENBERG+AK

N = 125
MEAN = 54
STD. ERR. = 5
STD. DEV. = 30
PCT. RDP. = 100

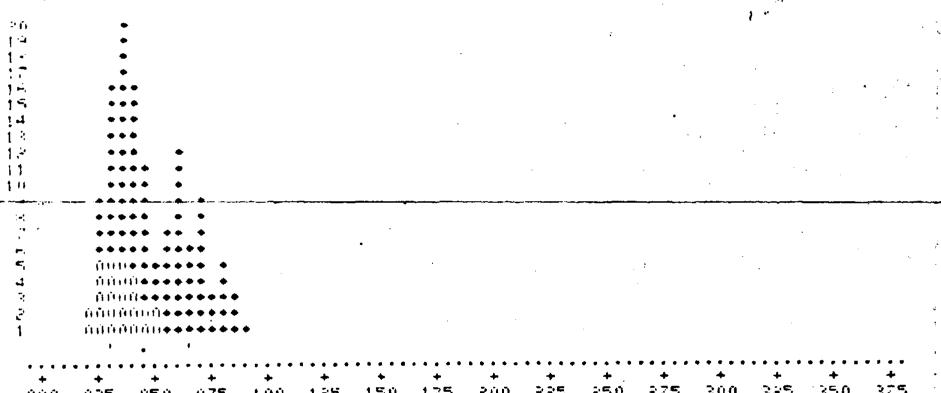
000 - 069 = 0.43 (74%)
070 - 375 = 0.97 (26%)



BASALT AT 5000' - 5650'

11-13-81 18729 50 5620' 4 STANDARD OF CALIF.CAPE ESPENBERG+AK

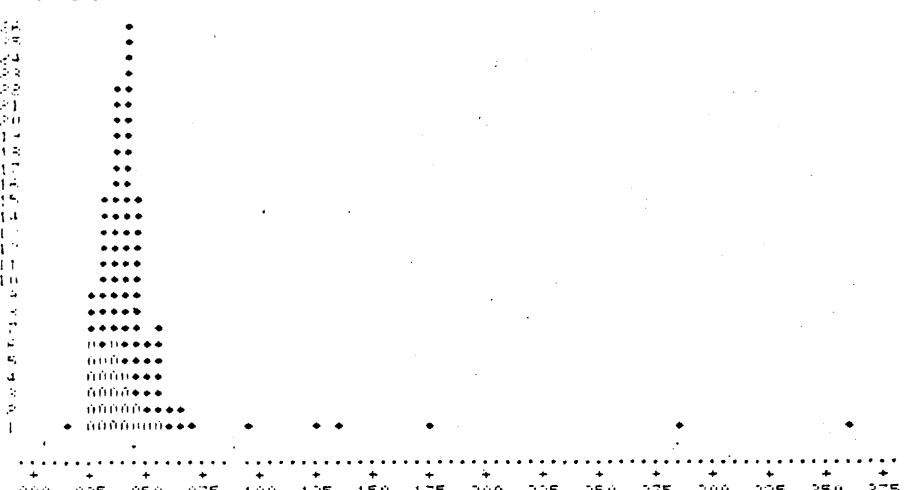
N = 125
MEAN = 49
STD. ERR. = 3
STD. DEV. = 17
PCT. RDP. = 100



VOLCANIC WELDED TUFF FROM 5800' - 7400'

11-13-81 18731 50 5480' 4 STANDARD OF CALIF.CAPE ESPENBERG+AK

N = 112
MEAN = 44
STD. ERR. = 7
STD. DEV. = 42
PCT. RDP. = 100



11-13-81 18732 50 4940' 4 STANDARD OF CALIF.CAPE ESPENBERG+AK

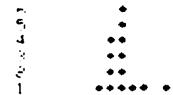
N = 14
MEAN = 37
STD. ERR. = 5

INSUFFICIENT DATA

11-13-81 18732 50 A3401 4 STANDARD OF CALIF,CAFE ESPENBERG&AK

INSUFFICIENT DATA

N = 14
MEAN = 32
STD. ERR. = 2
STD. DEV. = 2
PCT. POP. = 100



11-13-81 18733 50 A3701 4 STANDARD OF CALIF,CAFE ESPENBERG&AK

INSUFFICIENT DATA

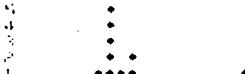
N = 9
MEAN = 44
STD. ERR. = 12
STD. DEV. = 12
PCT. POP. = 100



11-13-81 18734 50 Z0601 4 STANDARD OF CALIF,CAFE ESPENBERG&AK

INSUFFICIENT DATA

N = 10
MEAN = 44
STD. ERR. = 11
STD. DEV. = 17
PCT. POP. = 100

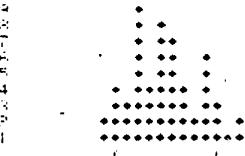


VOLCANIC AGGLOMERATE FROM ~7400' - 7900'

11-13-81 18735 50 74201 4 STANDARD OF CALIF,CAFE ESPENBERG&AK

0.66

N = 52
MEAN = 66
STD. ERR. = 5
STD. DEV. = 22
PCT. POP. = 100

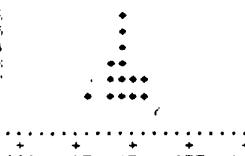


11-13-81 18736 50 77801 4 STANDARD OF CALIF,CAFE ESPENBERG&AK

000-124 = 0.46 (35%)

125-375 = 1.70 (64%)

N = 39
MEAN = 125
STD. ERR. = 20
STD. DEV. = 64
PCT. POP. = 100



META SEDIMENTS FROM 8000' TO T.D.

11-13-81 18737 50 91401 4 STANDARD OF CALIF,CAFE ESPENBERG&AK

000-134 = 0.44 (23%)

135-375 = 2.13 (77%)

N = 125
MEAN = 143
STD. ERR. = 15
STD. DEV. = 15
PCT. POP. = 100

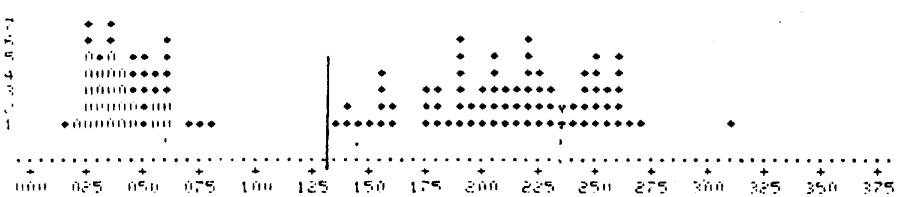
META SEDIMENTOLOGY FROM 18000' TO 0'

18140254 STANDARD OF CALIF. CAPE ESPERENGB1+AK

N = 125
MEAN = 143
STD. DEVI. = 15
STD. DEVP. = 18.7
PCT. POP. = 100

000 - 134 = 0.44 (23%)

135 - 375 = 2.13 (77%)

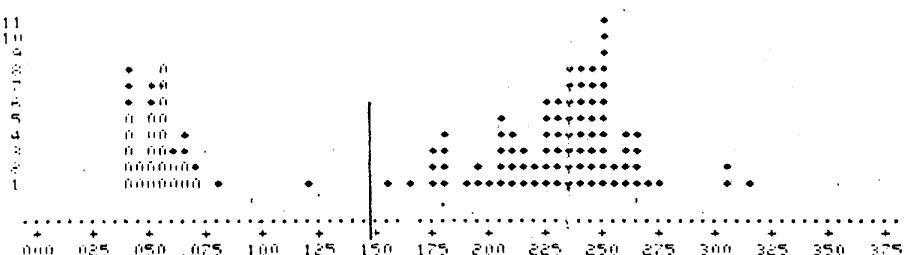


11-13-81 18738 50 50207 4 STANDARD OF CALIF. CAPE ESPERENGB1+AK

N = 125
MEAN = 122
STD. DEVI. = 14
STD. DEVP. = 18.4
PCT. POP. = 100

000 - 149 = 0.56 (11%)

150 - 375 = 2.33 (89%)



CORE

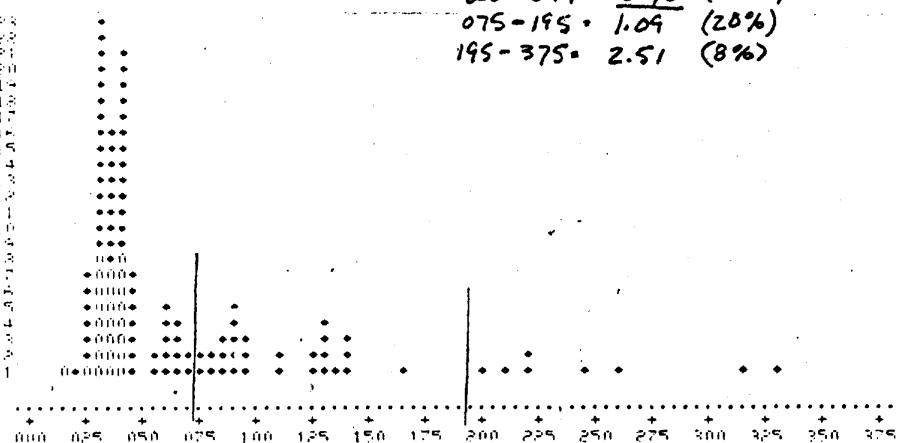
11-13-81 18739 50 50007 2 STANDARD OF CALIF. CAPE ESPERENGB1+AK

N = 125
MEAN = 64
STD. DEVI. = 1.0
STD. DEVP. = 1.8
PCT. POP. = 100

000 - 074 = 0.40 (64%)

075 - 195 = 1.09 (20%)

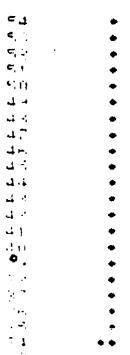
195 - 375 = 2.51 (8%)



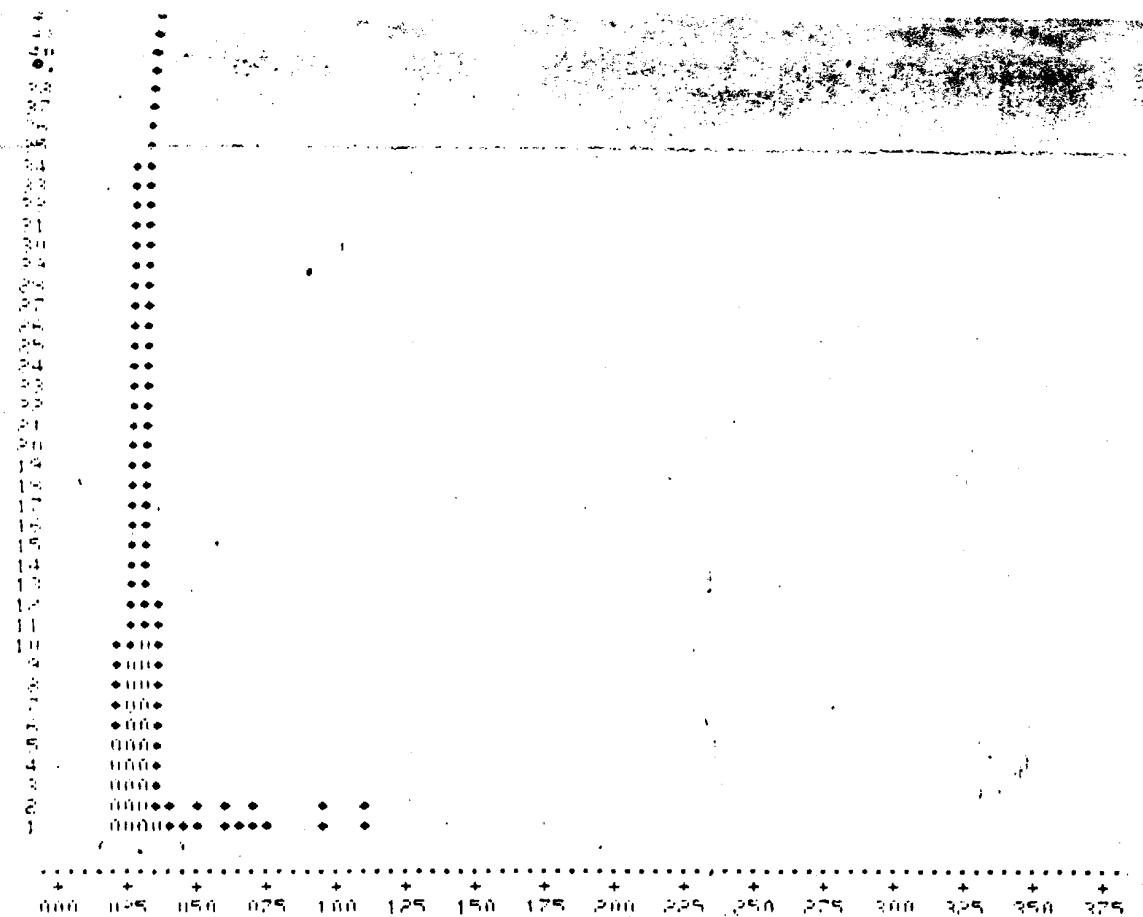
CORE

11-13-81 18740 50 50261 2 STANDARD OF CALIF. CAPE ESPERENGB1+AK

N = 125
MEAN = 34
STD. DEVI. = 2
STD. DEVP. = 1.5
PCT. POP. = 100



0.34

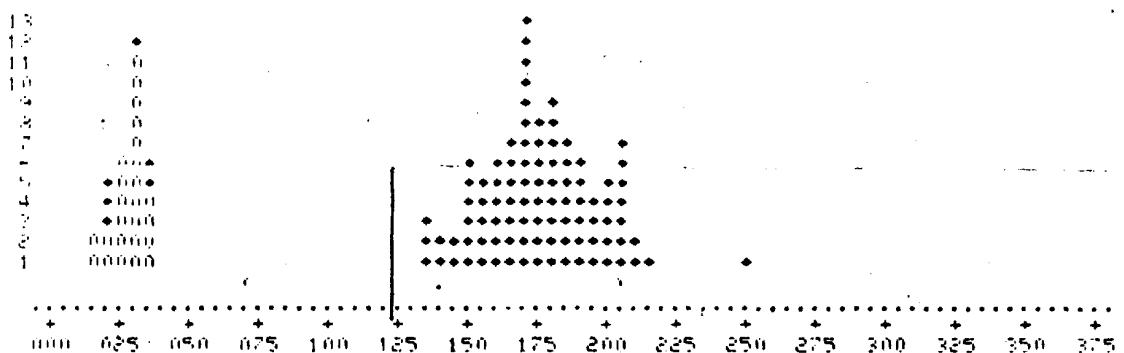


VOLCANIC AGGLOMERATE

11-13-81 18741 50 77051 2 STANDARD OF CALIF,CAPE ESCHENBERG#1,AK

N = 126
MEAN = 140
STD. ERR. = 11
STD. DEV. = 56
PCT. POP. = 100

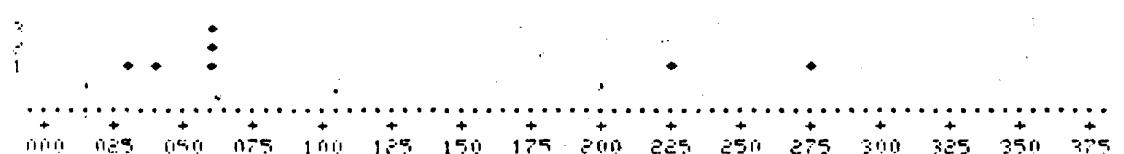
$$000-124 = 0.29 \text{ (6\%)} \\ 125-375 = \underline{1.77} \text{ (94\%)}$$



11-13-81 18742 50 83612 2 STANDARD OF CALIF,CAPE ESCHENBERG#1,AK

INSUFFICIENT DATA.

N = ?
MEAN = 104
STD. ERR. = 54
STD. DEV. = 92
PCT. POP. = 100



**COMMAND =

original

Mobil Exploration and Producing Services Inc.

P.O. BOX 900
DALLAS, TEXAS 75221

November 23, 1981

3

Mr. William Van Aken
State of Alaska
Alaska Oil & Gas Conservation Commission
3001 Porcupine Drive
Anchorage, Alaska 99501

ESC REQUEST NO. 311A78
VISUAL KERGEN, THERMAL MATURATION,
TOC AND ROCK-EVAL ANALYSES,
SOCAL CAPE ESPENBERG #1.
KOTZEBUE, ALASKA

Dear Mr. Aken:

This report describes the visual kerogen, thermal maturation, TOC and Rock-Eval results from the SOCAL Cape Espenberg #1 well, Kotzebue, Alaska. Visual kerogen and vitrinite reflectance analyses are based on 24 ditch samples taken at 300' intervals between 130' and 8320' (TD). Four core samples are also included in these studies. TOC and Rock-Eval analyses are based on 24 ditch samples taken at 90' intervals between 190' and 3970', and 510' intervals between 3970' and 7750'. A plot of the low-gray Ro means (figure 1), a kerogen analysis sheet (table 1), a summary of the thermal maturity and hydrocarbon potential (table 2), histogram plots, and a copy of the TOC and Rock-Eval report are included.

Results from TAI analysis of the SOCAL Cape Espenberg #1 indicate that the section penetrated from 130' to 1570' is transitionally mature, and the interval between 2380' and 4540' is slightly mature. The TAI results and vitrinite reflectance results are in conflict. The vitrinite data indicate the 130' to 4540' interval is thermally immature. The TAI values were taken from spores which tend to be thicker walled, therefore, darker than the preferred bissacates. It is possible that the dark color of the spores was caused by oxidation. In either event, the sparseness of palynomorphs inhibits any further breakdown of maturity by TAI analysis.

- Results from visual kerogen analysis of the SOCAL Cape Espenberg #1 samples are listed on the attached kerogen analysis sheet (table 1). It should be noted that all of the samples analyzed from this well are dominated by cellulosic (gas type) kerogens. Fluorescence analysis of these samples supports this interpretation.

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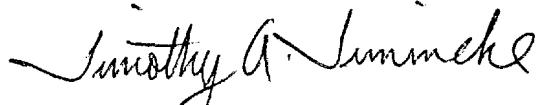
November 23, 1981

Results from vitrinite reflectance studies on the SOCAL Cape Espenberg #1 well indicate that the interval between 130' and 5000' is thermally immature. The interval between 5000' and 7420' contains no in situ vitrinite. The interval from 7705' to 8320' is overmature. Lithologies indicate a section of volcanic rocks from 5000' to approximately 7400' with pyroclastic rocks and metamorphic sediments from about 7400' to 8373' (TD). A plot of the low-gray Ro means from the Cape Espenberg #1 samples is attached (figure 1). A summary of the thermal maturity and hydrocarbon potential of the Cape Espenberg #1 samples is also included with the report (table 2). Histogram plots of the Ro readings from each sample are attached. The reflectance measurements used in this study were made by R. R. Taylor.

Results from TOC analysis range from "poor" below 5860' to "very good" for samples between 1030' and 1450'. Pyrolysis indicates "poor" to "marginal" hydrocarbon potential for the samples that have TOC's over 1% and gas as the most likely hydrocarbon they would generate.

Time requirements for this job were charged to ESC Request No. 311A78. If you have any questions concerning the results or interpretations, please do not hesitate to contact me.

Very truly yours,



T. A. Timmcke
Exploration Services Center
Applied Stratigraphy

TAT/jg
Attachments



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TABLE I
ORGANIC RESIDUE (KEROGEN) ANALYSIS

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[Rev. 01-80]

FIGURE 1
Plot of Low-Gray Ro Means
SOCAL Cape Espenberg #1, Kotzebue, Alaska

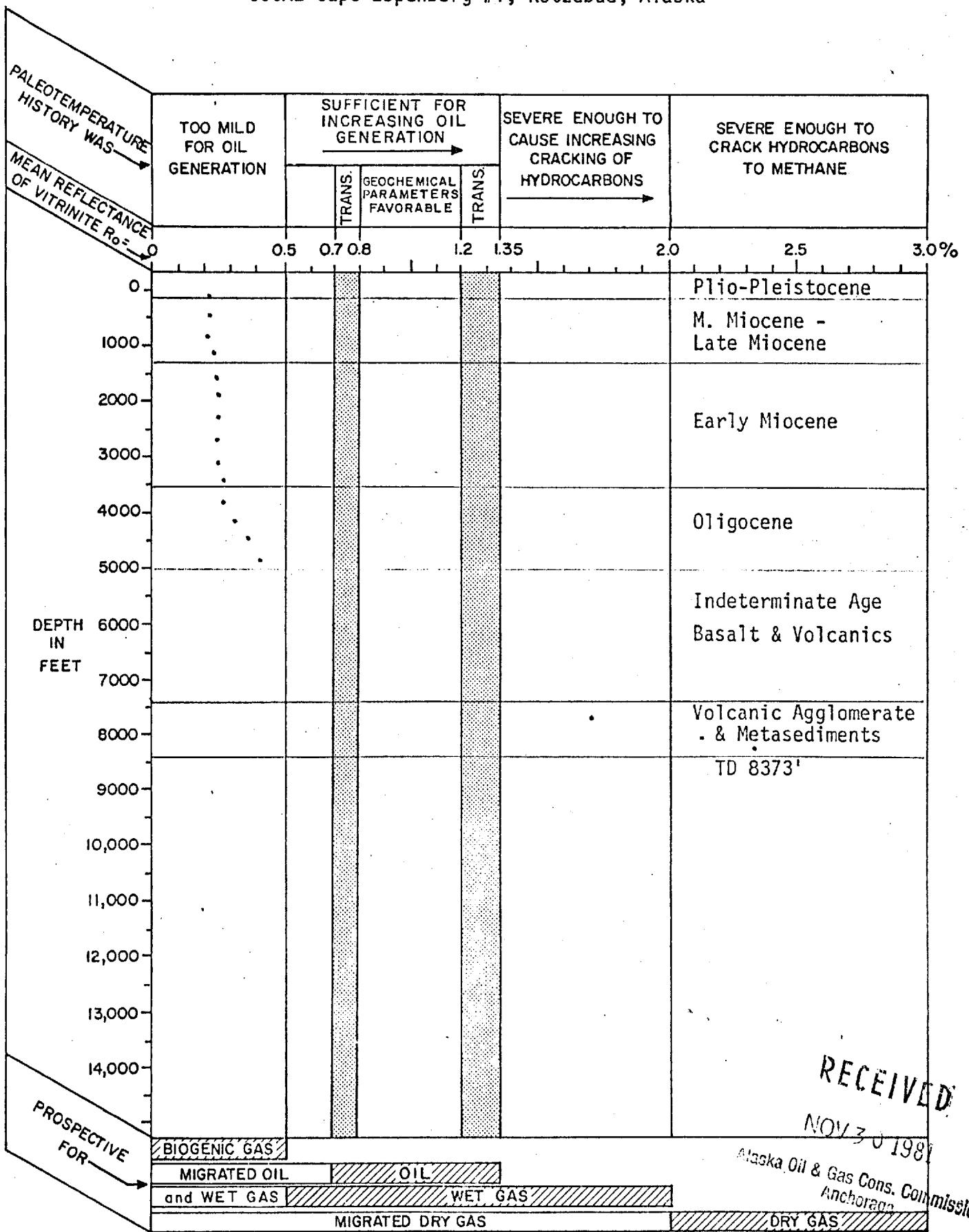


TABLE 2
Thermal Maturation and Visual Kerogen Analyses
Socal Cape Espenberg No. 1, Kotzebue, Alaska

<u>DEPTH OR SPL. NO.</u>	<u>LOW-GRAY Ro MEAN</u>	<u>% POP.</u>	<u>FIRST HIGH-GRAY Ro MEAN</u>	<u>% POP.</u>	<u>TAI</u>	<u>THERMAL MATURITY</u>	<u>KEROGEN TYPE</u>	<u>HYDROCARBON POTENTIAL/REMARKS</u>
130'	0.22	28	0.81	48	2	Immature	Cellulosic	Gas type kerogen
490'	0.23	65	0.87	35	2	Immature	Cellulosic	Gas type kerogen
850'	0.22	73	0.93	26		Immature	Cellulosic	Gas type kerogen
1210'	0.25	92	0.76	8		Immature	Cellulosic	Gas type kerogen
1570'	0.26	75	1.13	24		Immature	Cellulosic	Gas type kerogen
1930'	0.27	89	1.28	11	2+	Immature	Cellulosic	Gas type kerogen
2380'	0.27	94	1.24	6		Immature	Cellulosic	Gas type kerogen
2740'	0.25	85	0.86	15		Immature	Cellulosic	Gas type kerogen
3110'	0.26	81	1.29	18		Immature	Cellulosic	Gas type kerogen
3460'	0.29	73	1.05	26		Immature	Cellulosic	Gas type kerogen
3820'	0.29	74	0.74	26		Immature	Cellulosic	Gas type kerogen
4180'	0.34	84	0.76	16	2+	Immature	Cellulosic	Gas type kerogen
4540'	0.40	92	1.13	8		Immature	Cellulosic	Gas type kerogen
4900'	0.43	74	0.97	26		Immature	Cellulosic	Gas type kerogen
5260'	-	-	-	-		-	-	Sample lost
5620'	0.49	100				Immature	Cellulosic	Basalt-caved vitrinite
5980'	0.49	100				Immature	Cellulosic	Welded tuff-caved vit.

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TABLE 2
Thermal Maturation and Visual Kerogen Analyses
Socal Cape Espenberg No. 1, Kotzebue, Alaska

<u>DEPTH OR SPL. NO.</u>	<u>LOW-GRAY Ro MEAN</u>	<u>% POP.</u>	<u>FIRST HIGH-GRAY Ro MEAN</u>	<u>% POP.</u>	<u>TAI</u>	<u>THERMAL MATURITY</u>	<u>KEROGEN TYPE</u>	<u>HYDROCARBON POTENTIAL/REMARKS</u>
6340'	-	-	-	-	-	-	-	Insufficient data
6670'	-	-	-	-	-	-	-	Insufficient data
7060'	-	-	-	-	-	-	-	Insufficient data
7420'	0.66	100				Immature	Cellulosic	Volcanic Agglomerate- Probable caved vit.
7780'	1.70	64				Overmature	Cellulosic	Volcanic Agglomerate
8140'	2.13	77				Overmature	Cellulosic	Gas-metasediments
8320'	2.33	89				Overmature	Cellulosic	Gas-metasediments
<u>Cores</u>								
5000'	0.40	65	1.09	28		Immature	Cellulosic	Gas type kerogen
5026'	0.34	100				Immature	Cellulosic	Basalt-caved vitrinite
7705'	1.77	94				Overmature	Cellulosic	Volcanic Agglomerate
AB361'	-	-	-	-		-	-	Insufficient data

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REPORT NO. 489

GEOCHEMICAL EVALUATION OF
TWENTY-FOUR SAMPLES FROM
THE SOCAL CAPE ESPENBERG
#1 WELL

by
Mary Michael Page

Project No. RRUS/812/II/T/51

Prepared by:
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September 25, 1981

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INTRODUCTION

Twenty-four samples were forwarded for Total Organic Carbon (TOC) analysis and Rock-Eval pyrolysis. The Rock-Eval pyrolysis was to be run regardless of the TOC value. Two of the samples exhibited high amounts of bitumen, as evidenced by the coalescence of the pyrolysis S1 and S2 into a single peak. The suggestion was made to, and accepted by, the client to extract these samples and evaluate both the extracted sample and the recovered extract.

SUMMARY

The source richness based on TOC range from "non-source" below 5,860 feet to "very good" for samples between 1030 and 1450 ft. Pyrolysis generally indicates "nonsource" to "marginal" amounts of hydrogen-poor kerogen. The T-max values indicate immature material but are probably not representative for the samples with the single S1 + S2 peak. For samples 1450 and 2290, the S1 and S2 peaks merge, suggesting the presence of significant amounts of bitumen. A portion of the sample was extracted and rerun; however the general shape of the pyrogram did not change. The extract consists of moderate amounts of immature bitumen, and gives no indication of the type of material responsible for the anomalous Rock-Eval response.

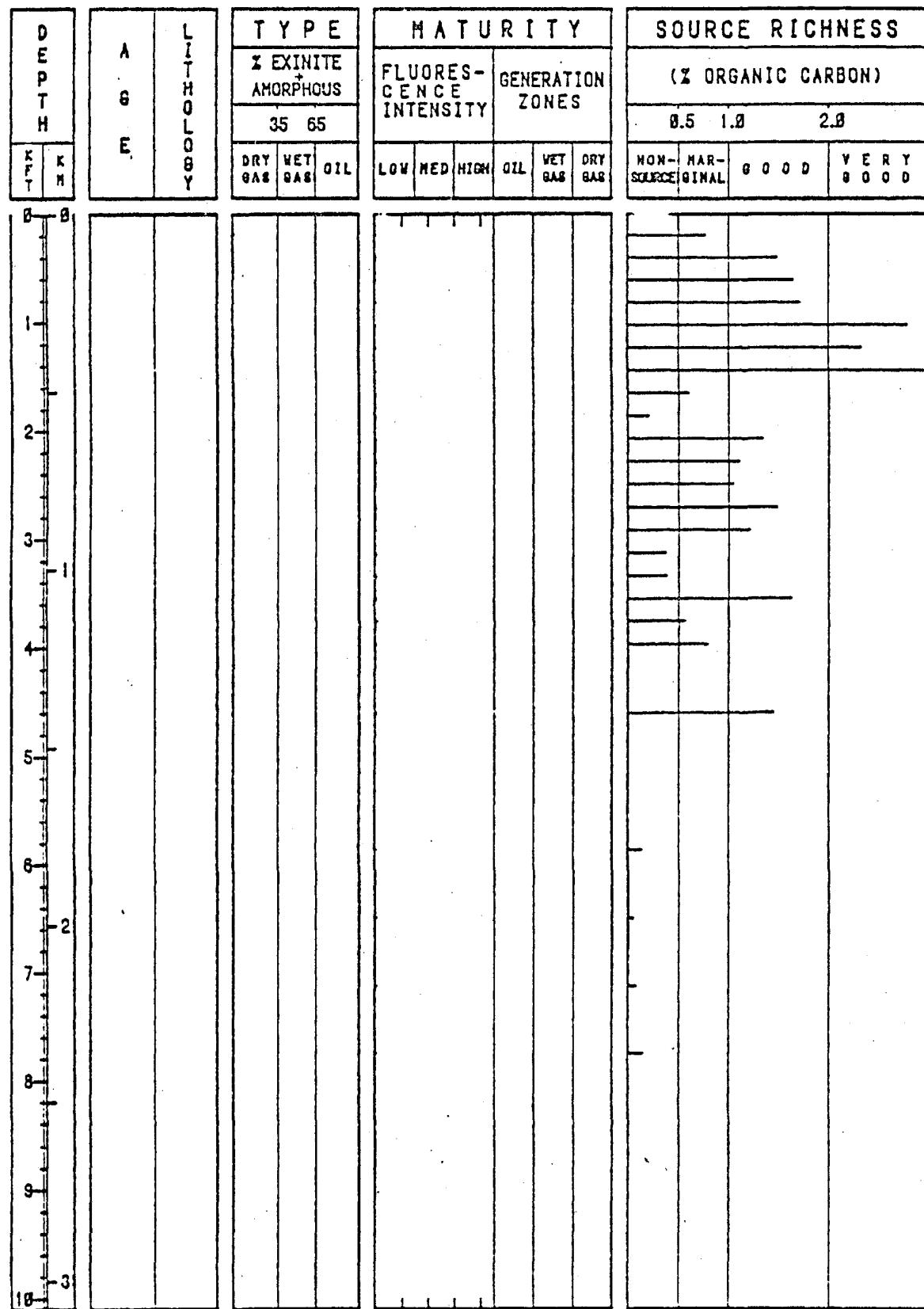
The increase in TOC for sample 1450 is reproducible and probably due to the removal of sulfur together with the bitumen during extraction. The high per cent carbon and character of the chromatogram are consistent with a coaly type material, which accumulates in an environment conducive to high sulfur concentrations.

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SOCAL CAPE ESPENBERG #1



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FIGURE 1: SUMMARY PLOTS SHOWING KEROGEN TYPES, MATURITY,
NOV 30 1981 AND SOURCE RICHNESS (SEE APPENDICES IV AND II)Alaska Oil & Gas Cons. Commission
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SOCAL CAPE ESPENBERG #1

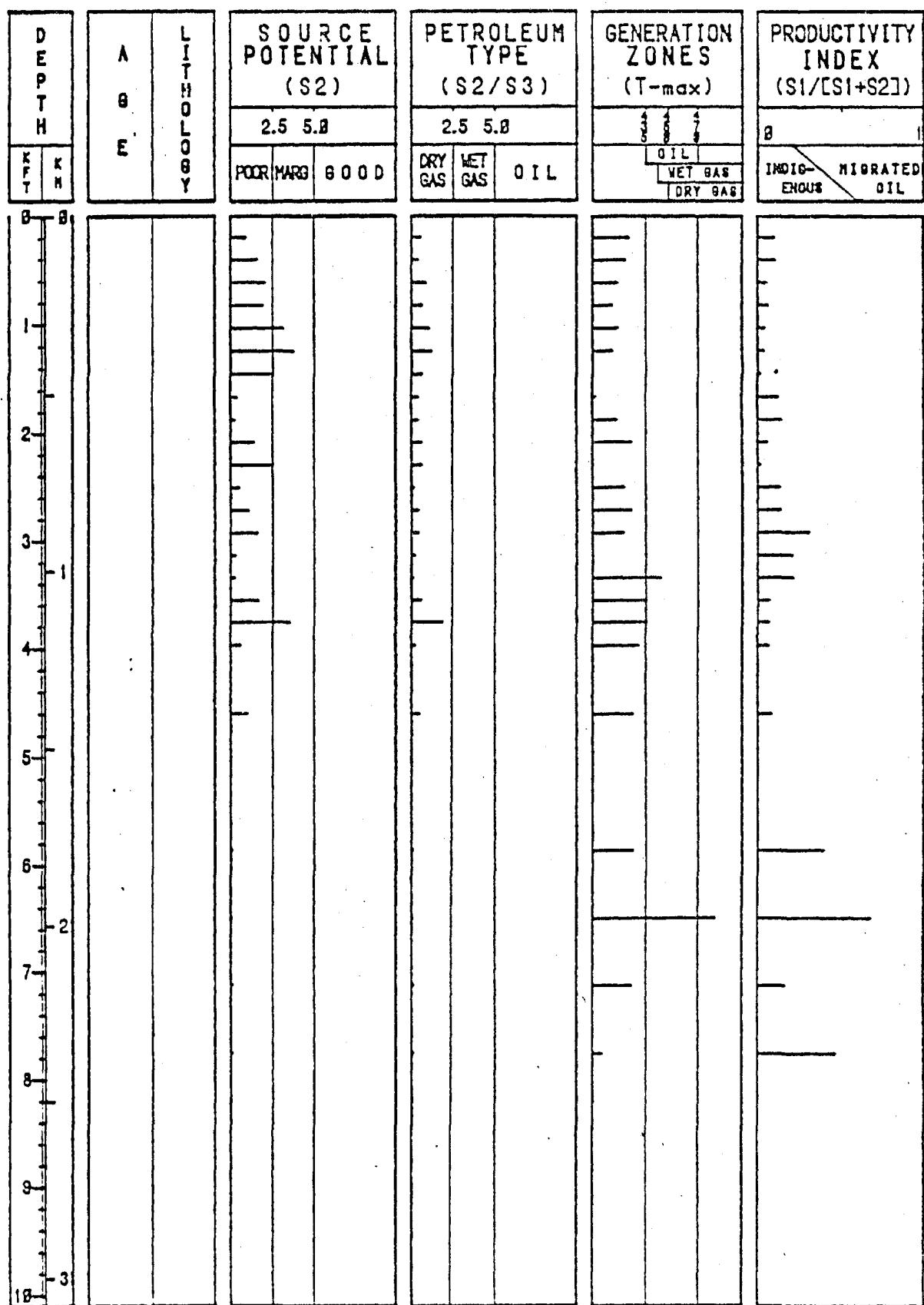


FIGURE 2: SUMMARY PLOTS OF ROCK-EVAL PYROLYSIS DATA (APPENDIX II)

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APPENDIX I

TOTAL ORGANIC CARBON DATA

Total organic carbon is determined by pulverizing the sample, treating a carefully weighed portion with warm hydrochloric acid to remove carbonate minerals, and analysing the residue for carbon content with a Leco carbon analyser. It is generally accepted that samples with less than about 0.5 percent TOC cannot yield sufficient petroleum to form commercial deposits and are therefore considered nonsources; samples with between 0.5 and 1.0 TOC are rated as marginal in source quality; and samples with more than 1.0 TOC are considered to be good in source quality.

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TOTAL ORGANIC CARBON DATA
SOCAL CAPE ESPENBERG #1

Sample Interval	DEPTH (FEET)	TOC (%)	Sample Interval	DEPTH (FEET)	TOC (%)
130- 250	190	0.76	2650-2770	2710	1.48
340- 460	400	1.48	2860-2980	2920	1.20
550- 670	610	1.64	3070-3190	3130	0.36
760- 880	820	1.70	3280-3400	3340	0.37
970-1090	1030	2.78	3490-3610	3550	1.62
1180-1300	1240	2.32	3700-3820	3755	0.55
1390-1510	1450	17.17	3910-4030	3970	0.78
1600-1720	1660	0.59	4540-4660	4600	1.44
1810-1930	1870	0.19	5800-5920	5860	0.12
2020-2140	2080	1.33	6430-6550	6490	0.24
2230-2350	2290	1.10	7060-7180	7120	0.26
2440-2560	2500	1.04	7690-7810	7750	0.13

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APPENDIX II

ROCK-EVAL PYROLYSIS DATA

Rock-Eval data are expressed as mg/g of rock and include four basic parameters: 1) S_1 represents the quantity of free hydrocarbons present in the rock and is roughly analogous to the solvent extractable portion of the organic matter; 2) S_2 represents the quantity of hydrocarbons released by the kerogen in the sample during pyrolysis; 3) S_3 is related to the amount of oxygen present in the kerogen; and 4) T -max, in °C, is the temperature at which the maximum rate of generation (of the S_2 peak) occurs and can be used as an estimate of thermal maturity.

In addition, the ratio S_2/S_3 provides a general indication of kerogen quality (type) and reveals whether oil or gas are likely to be generated. The ratio $S_1/(S_1+S_2)$, or the productivity index, is an indication of the relative amount of free hydrocarbons (in place or migrated) present in the sample. Hydrogen and oxygen index values are in mg of hydrocarbons (S_2 peak) or carbon dioxide (S_3 peak) per gram of organic carbon. When plotted against each other on a van Krevelen-type diagram, information on kerogen type and maturity can be obtained.

Data are interpreted in the following manner:

Source Potential - values of S_2	<2.5	: poor
	2.5-5.0	: marginal
	>5.0	: good

Petroleum Type - value of S_2/S_3	<2.5	: dry gas
	2.5-5.0	: wet gas
	>5.0	: oil

Generation Zones - values of T -max	<435	: immature
	435-470	: oil
	450 +	: gas

Productivity Index - high values of $S_1/(S_1+S_2)$ indicate migrated hydrocarbons.

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ROCK-EVAL PYROLYSIS RAW DATA

SOCAL CAPE ESPENBERG #1

DEPTH (FEET)	S1	S2	S3	S2/S3	S1/(S1+S2)	T-MAX
190	0.081	0.820	1.768	0.464	0.090	423
400	0.157	1.514	4.284	0.354	0.094	421
610	0.082	1.982	2.487	0.797	0.040	415
820	0.110	1.855	3.106	0.597	0.056	412
1030	0.102	3.105	3.113	0.997	0.032	416
1240	0.114	3.747	3.266	1.147	0.030	412
1450	---	---	---	---	---	---
1660	0.043	0.328	0.927	0.354	0.115	401
1870	0.025	0.163	0.498	0.328	0.131	415
2080	0.069	1.349	2.493	0.541	0.048	425
2290	---	---	---	---	---	---
2500	0.057	0.416	3.818	0.109	0.121	420
2710	0.148	1.004	2.835	0.354	0.129	425
2920	0.664	1.551	4.397	0.353	0.300	420
3130	0.050	0.204	1.478	0.138	0.198	362
3340	0.041	0.162	3.893	0.042	0.203	445
3550	0.096	1.598	3.457	0.462	0.257	434
3755	0.210	3.466	1.949	1.779	0.057	435
3970	0.033	0.510	3.245	0.157	0.061	430
4600	0.070	0.886	2.267	0.391	0.073	426
5860	0.018	0.029	1.151	0.025	0.387	426
6490	0.017	0.008	0.550	0.015	0.674	481
7120	0.015	0.083	1.069	0.077	0.155	425
7750	0.038	0.044	0.641	0.069	0.458	405

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HYDROGEN AND OXYGEN INDICES FROM ROCK-EVAL
PYROLYSIS DATA, WITH TOC DATA

SOCAL CAPE ESPENBERG #1

DEPTH (FEET)	HYDROGEN INDEX (mg HC/g TOC)	OXYGEN INDEX (mg CO ₂ /g TOC)	TOC (%)
190	108	233	0.76
400	102	289	1.48
610	121	152	1.64
820	109	183	1.70
1030	112	112	2.78
1240	162	141	2.32
1450	13	24	17.17
1660	56	157	0.59
1870	86	262	0.19
2080	101	187	1.33
2290	211	377	1.10
2500	40	367	1.04
2710	68	192	1.48
2920	129	366	1.20
3130	57	411	0.36
3340	44	1052	0.37
3550	99	213	1.62
3755	630	354	0.55
3970	65	416	0.78
4600	62	157	1.44
5860	24	959	0.12
6490	20	1374	0.04
7120	138	1781	0.06
7750	34	493	0.13

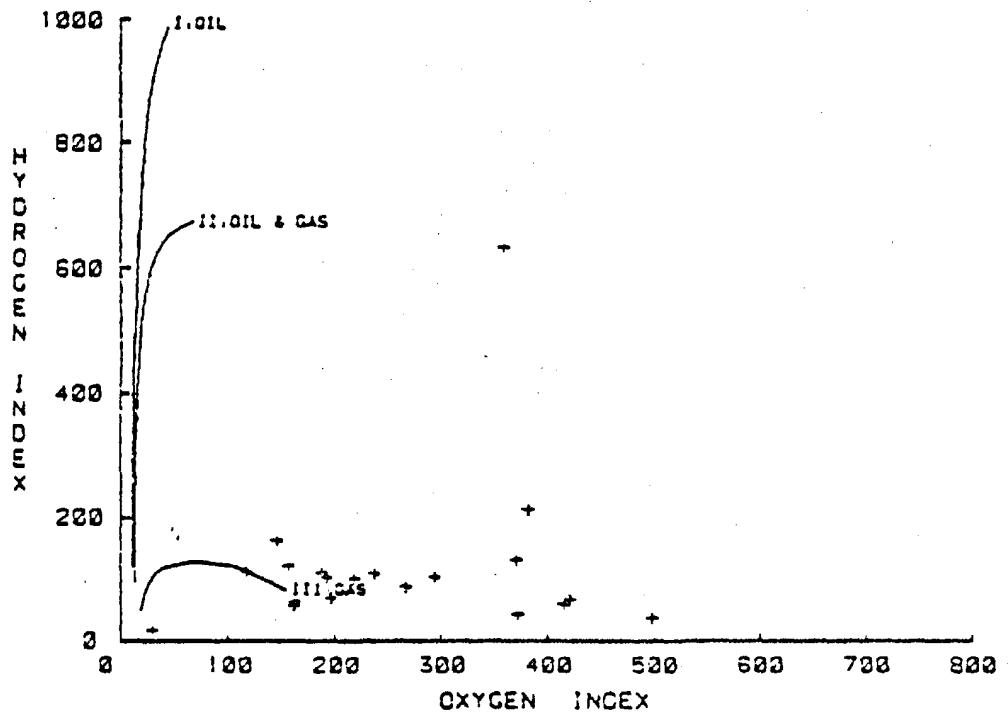
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SOCAL CAPE ESPENBERG #1



KEROGEN TYPE DETERMINATION FROM ROCK-EVAL.
PYROLYSIS DATA (APPENDIX III).

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ROCK-EVAL PYROLYSIS RAW DATA

SOCAL CAPE ESPENBERG #1

DEPTH (FEET)	S1+S2	S3	S2/S3	S1/(S1+S2)	T-MAX
1450	23.548	13.384	1.759	0.000	362
2290	3.610	2.765	0.000	1.000	---

HYDROGEN AND OXYGEN INDICES FROM ROCK-EVAL
PYROLYSIS DATA, WITH TOC DATA

SOCAL CAPE ESPENBERG #1

DEPTH (FEET)	HYDROGEN INDEX (mg HC/g TOC)	OXYGEN INDEX (mg CO ₂ /g TOC)	TOC (%)
1450	137	78	17.17
2290	0	251	1.10

SOCAL CAPE ESPENBERG #1

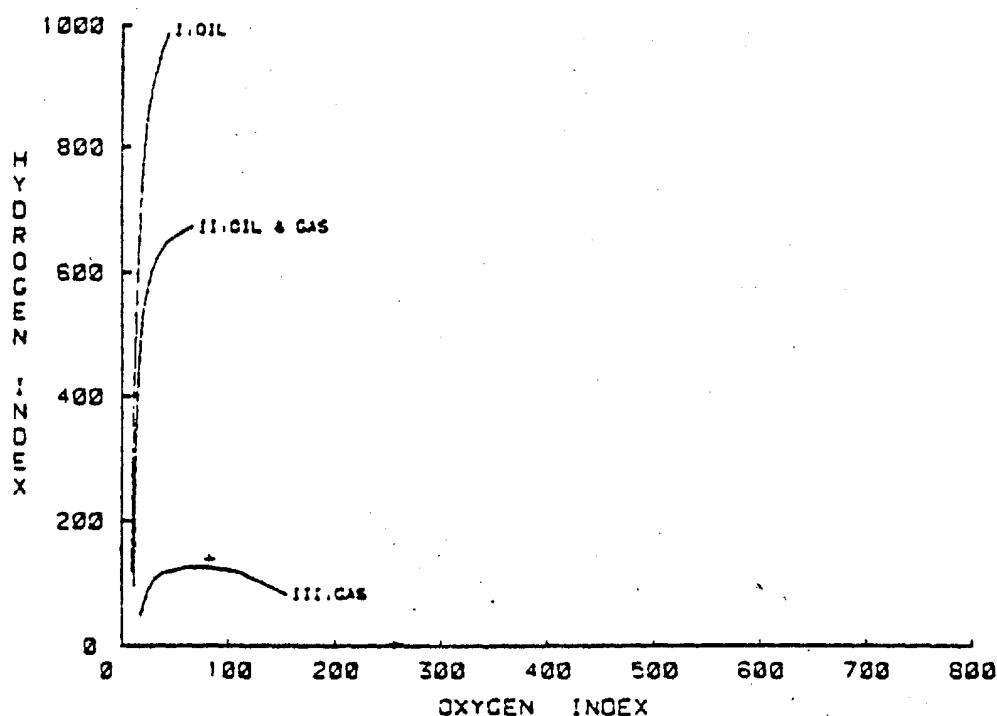


FIGURE 3: KEROGEN TYPE DETERMINATION FROM ROCK-EVAL PYROLYSIS DATA (APPENDIX III).

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ROCK-EVAL PYROLYSIS RAW DATA

SOCAL CAPE ESPENBERG #1 - EXTRACTED

DEPTH (FEET)	S1+S2	S3	S2/S3	S1/(S1+S2)	T-MAX
1450	16.745	15.649	1.056	0.013	393
2290	0.516	3.693	0.132	0.058	410

HYDROGEN AND OXYGEN INDICES FROM ROCK-EVAL
PYROLYSIS DATA, WITH TOC DATA

SOCAL CAPE ESPENBERG #1 - EXTRACTED

DEPTH (FEET)	HYDROGEN INDEX (mg HC/g TOC)	OXYGEN INDEX (mg CO ₂ /g TOC)	TOC (%)
1450	92	88	18.12
2290	62	471	0.83

SOCAL CAPE ESPENBERG #1 - EXTRACTED

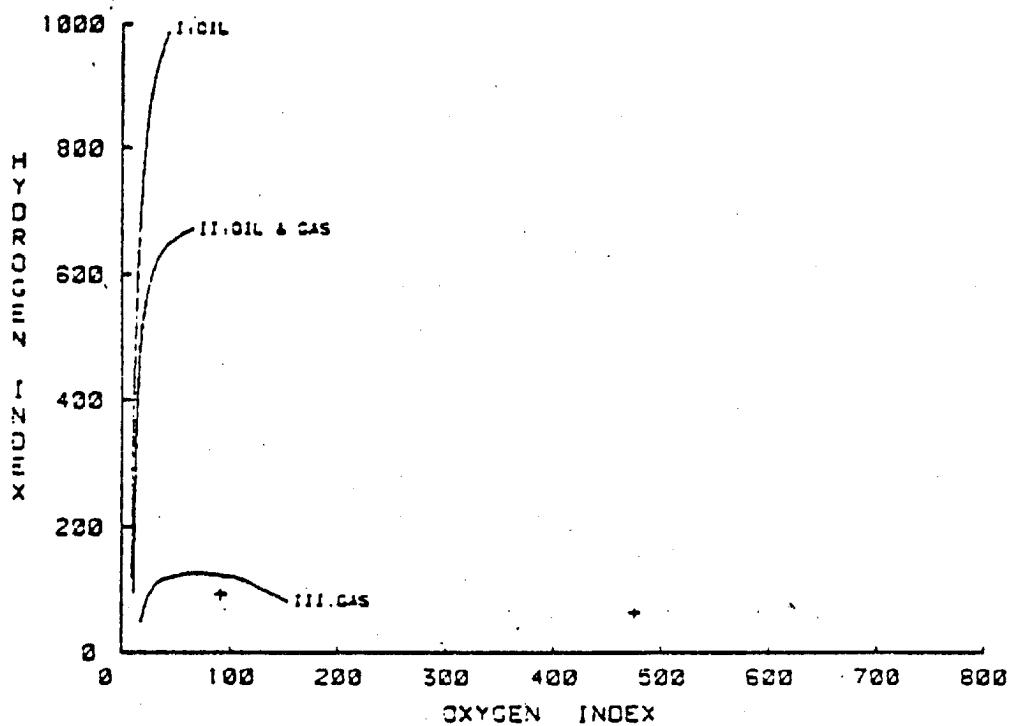


FIGURE 3: KEROGEN TYPE DETERMINATION FROM ROCK-EVAL PYROLYSIS DATA (APPENDIX II).

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APPENDIX III

ORGANIC EXTRACT DATA

Fifty grams of each sample is pulverized and soxhlet extracted for 18 hours with dichloromethane to obtain the total amount of extractable material. The extract is first deasphaltened by precipitation with hexane. The soluble fraction is then separated into saturates, aromatics, and NSO compounds on a silica-alumina chromatographic column by successive elutions with hexane, benzene, and benzene-methanol solvents respectively. The total extract is expressed in parts per million of total sample extracted and the functional groups are expressed as weight percent of total extract.

Gas chromatograms of the C₁₅+ saturate fraction were produced with a Perkin-Elmer, Sigma 3 gas chromatograph fitted with a 12 foot, NaNO₃/LiNO₃/KNO₃ eutectic column. The chromatograph was programmed from 40°C to 360°C at 12°C/min. using helium carrier gas at the rate of 25 ml/min.

Straight chain paraffins (n-alkanes) are normalized between C₁₅ and C₄₀ to a sum of 100% and the percent of individual components plotted on bar graphs. Several ratios involving pristane (Pr) and phytane (Ph) are also calculated and plotted. Carbon preference index (CPI) values are calculated with the original Bray and Evans formula.

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COMPOSITION OF SOURCE ROCK EXTRACT

SOCAL CAPE ESPENBERG #1

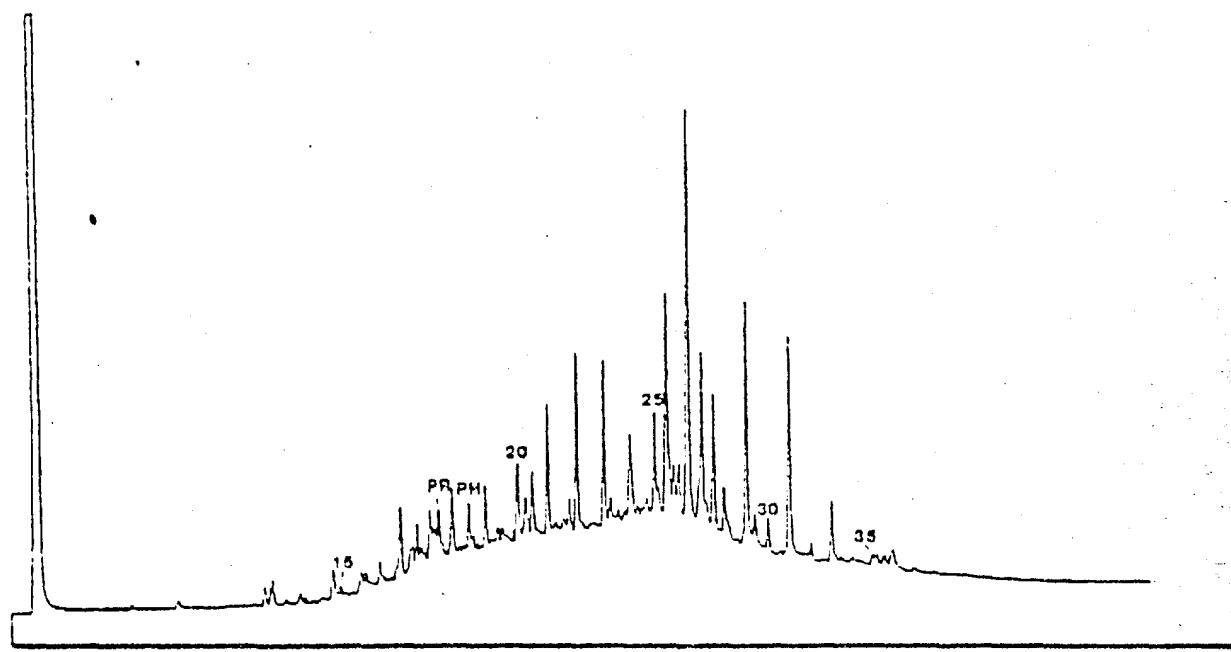
DEPTH(FEET)	EXTRACT PPM	% SAT	% AROM	% NSO	% ASPH
1450	480	19.50	18.30	8.50	53.70
2270	3536	10.70	33.50	31.40	24.40

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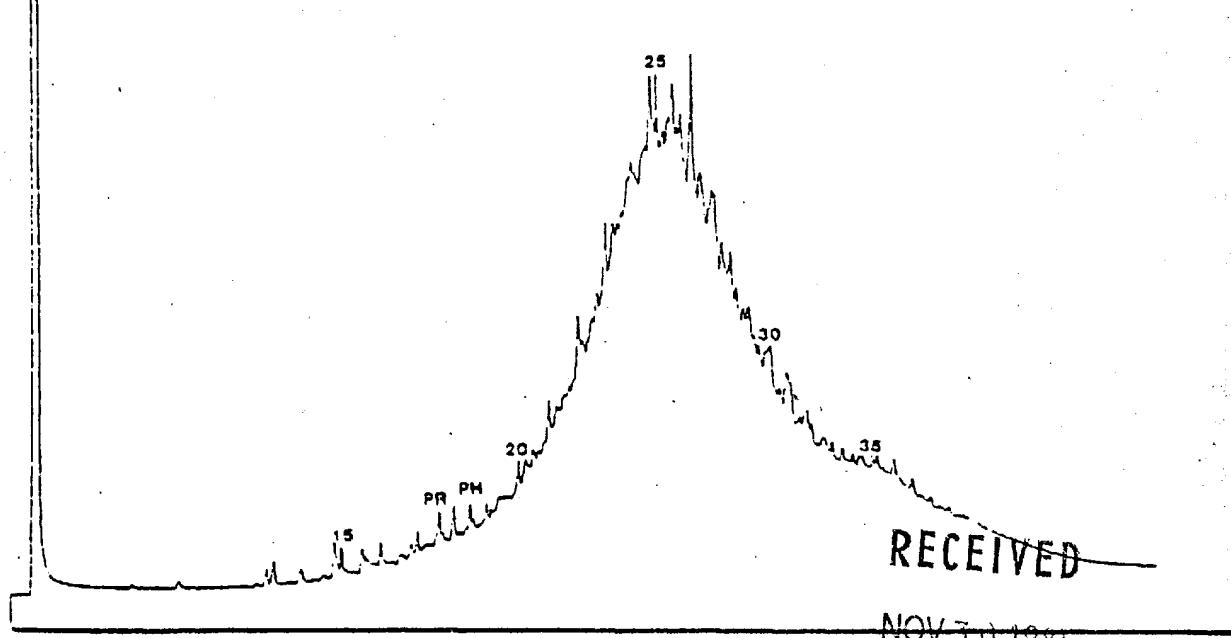
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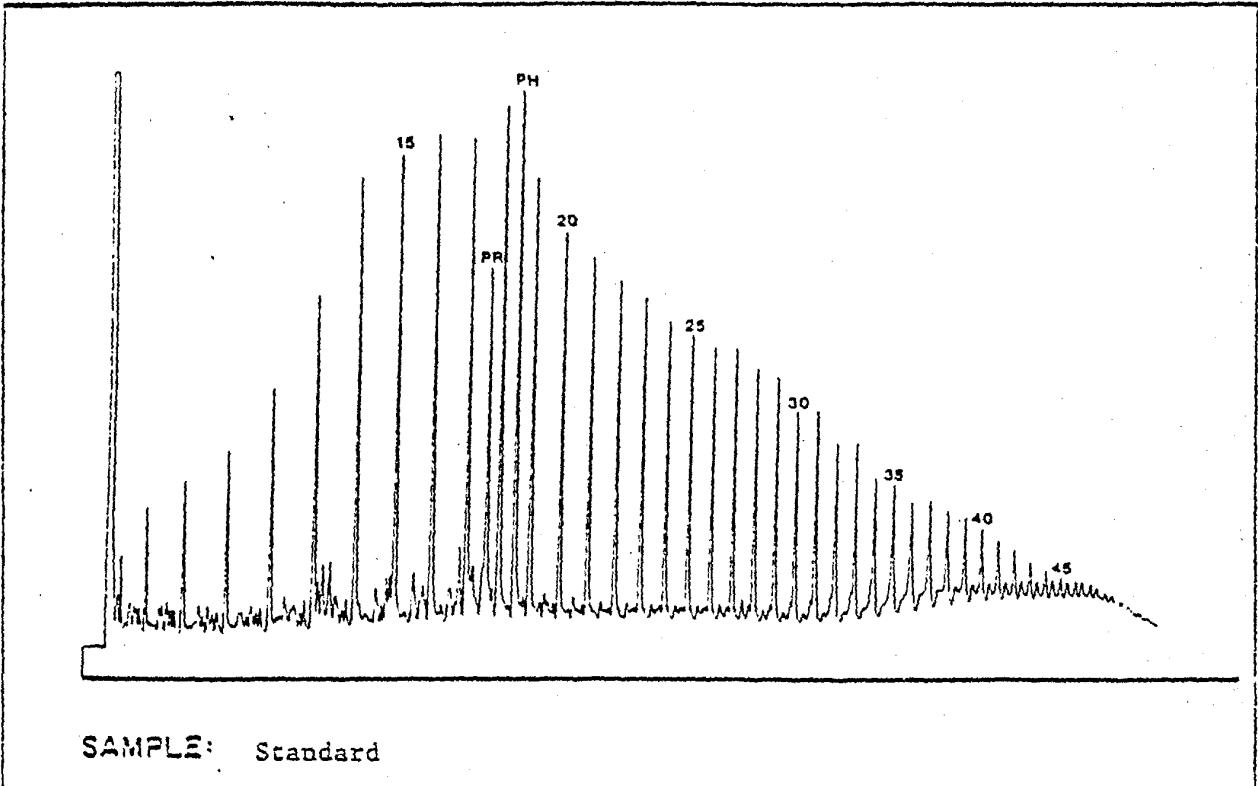
SAMPLE: 1450 feet.



SAMPLE: 2290 feet.

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GAS CHROMATOGRAMS OF CIS- SATURATE



GAS CHROMATOGRAMS OF C15+ SATURATE HYDROCARBONS

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ROCK-EVAL PYROLYSIS RAW DATA

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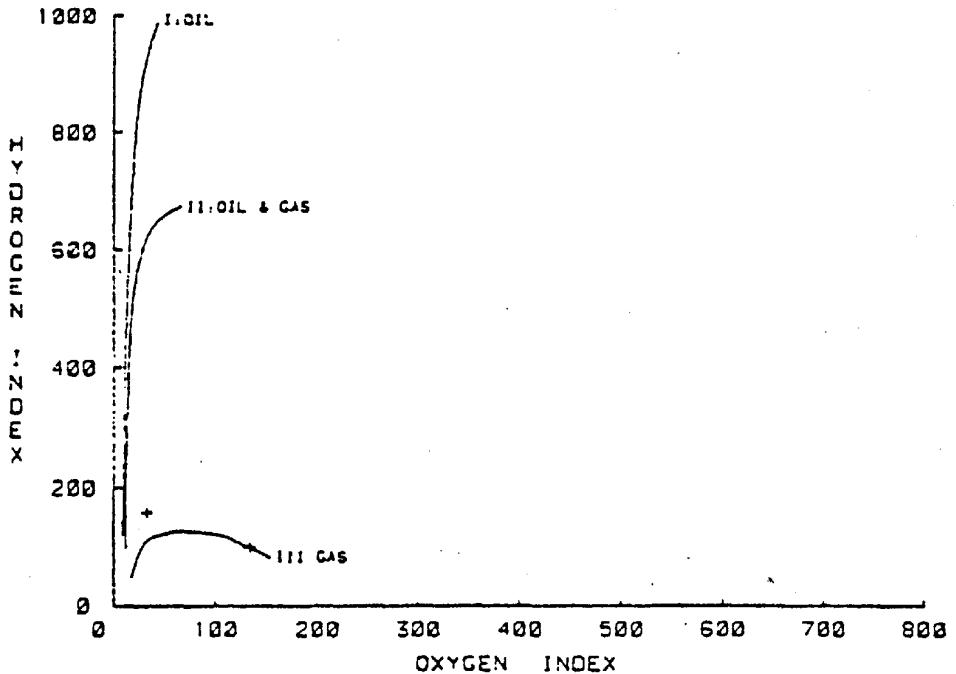
DEPTH (FEET)	S1+S2	S3	S2/S3	S1/(S1+S2)	T-MAX
790	1.535	2.023	0.758	0.000	332
1420	14.542	2.589	5.617	0.000	331

HYDROGEN AND OXYGEN INDICES FROM ROCK-EVAL
PYROLYSIS DATA, WITH TOC DATA

SOCAL MIMIUK PT. #1 - EXTRACTED

DEPTH (FEET)	HYDROGEN INDEX (mg HC/g TOC)	OXYGEN INDEX (mg CO ₂ /g TOC)	TOC (%)
790	98	130	1.56
1420	156	28	9.32

SOCAL MIMIUK PT. #1 - EXTRACTED

FIGURE 3. KEROGEN TYPE DETERMINATION FROM ROCK-EVAL.
PYROLYSIS DATA (APPENDIX III).

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APPENDIX III

ORGANIC EXTRACT DATA

Fifty grams of each sample is pulverized and soxhlet extracted for 18 hours with dichloromethane to obtain the total amount of extractable material. The extract is first deasphaltened by precipitation with hexane. The soluble fraction is then separated into saturates, aromatics, and NSO compounds on a silica-alumina chromatographic column by successive elutions with hexane, benzene, and benzene-methanol solvents respectively. The total extract is expressed in parts per million of total sample extracted and the functional groups are expressed as weight percent of total extract.

Gas chromatograms of the C₁₅+ saturate fraction were produced with a Perkin-Elmer, Sigma 3 gas chromatograph fitted with a 12 foot, NaNO₃/LiNO₃/KNO₃ eutectic column. The chromatograph was programmed from 40°C to 360°C at 12°C/min. using helium carrier gas at the rate of 25 ml/min.

Straight chain paraffins (n-alkanes) are normalized between C₁₅ and C₄₀ to a sum of 100% and the percent of individual components plotted on bar graphs. Several ratios involving pristane (Pr) and phytane (Ph) are also calculated and plotted. Carbon preference index (CPI) values are calculated with the original Bray and Evans formula.

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COMPOSITION OF SOURCE ROCK EXTRACT

SOCAL MIMIUK PT. #1

DEPTH(FEET)	EXTRACT PPM	% SAT	% AROM	% NSO	% ASPH
790	181	6.50	19.60	58.70	15.20
1420	200	20.60	12.70	50.80	15.90

DEPTH (Feet)	EXT/TOC	RELATIVE COMPOSITION			PR/PH	CPI
		%SAT	%AROM	%NSO+ASPH		
790	0.011	6.5	19.6	73.9	0.42	2.42
1420	0.002	20.6	12.7	66.7	0.94	3.13

HEAVY HYDROCARBONS NORMALIZED TO 100%

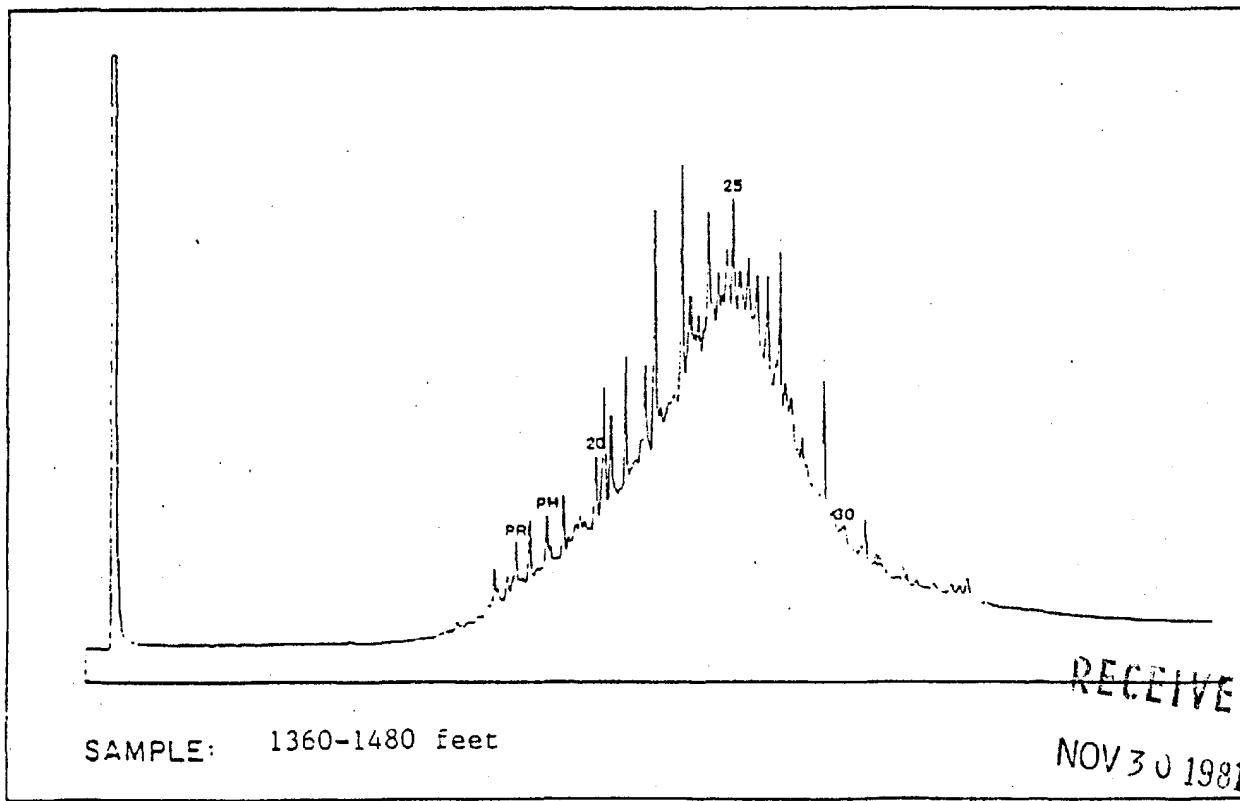
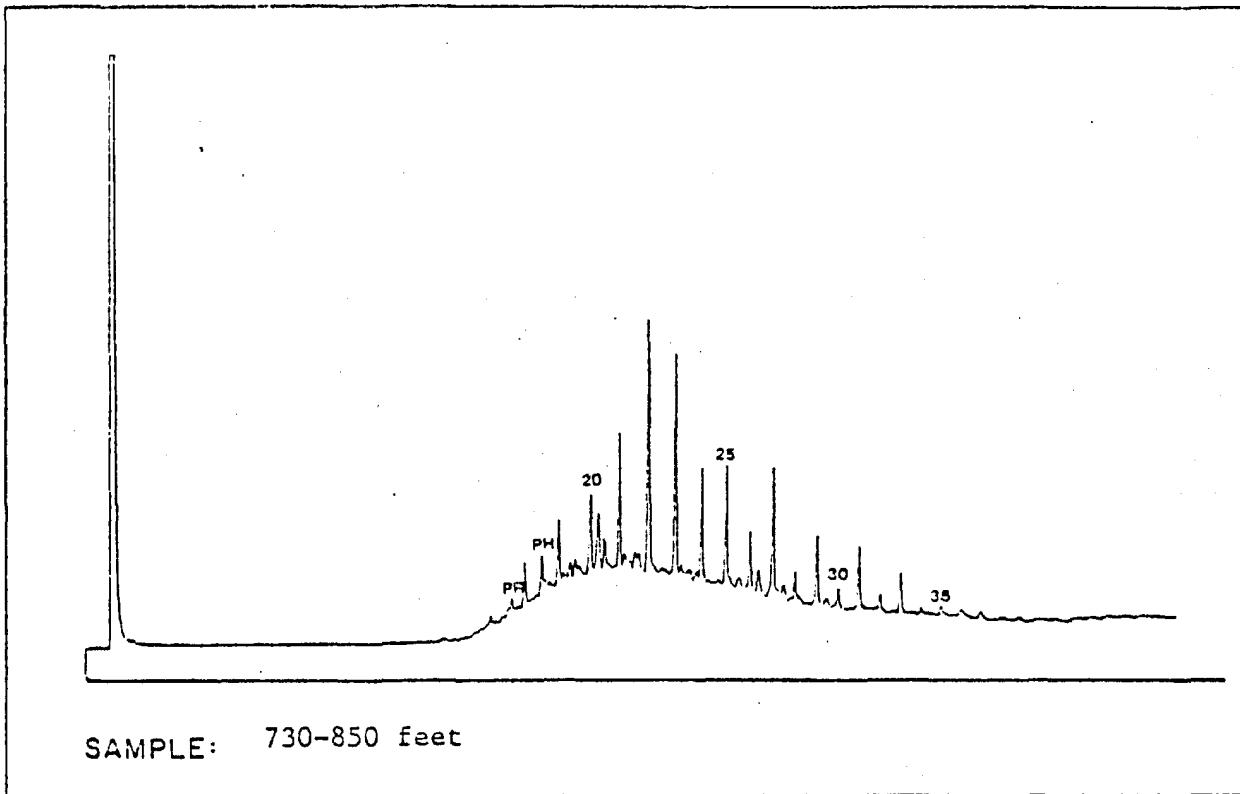
SOCAL MIMIUK PT. #1

ID	C-10	C-11	C-12	C-13	C-14	C-15	C-16	C-17	C-18	C-19	C-20
790	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.60	2.80	4.30	5.11
1420	0.00	0.00	0.00	0.00	0.00	0.10	0.50	2.50	3.89	3.79	4.39
ID	C-21	C-22	C-23	C-24	C-25	C-26	C-27	C-28	C-29	C-30	
790	8.91	16.72	14.71	7.71	8.11	3.80	8.71	2.20	4.60	1.40	
1420	8.18	14.77	14.87	9.98	9.08	3.99	9.88	1.80	8.08	1.00	
ID	C-31	C-32	C-33	C-34	C-35	C-36	C-37	C-38	C-39	C-40	
790	4.10	1.20	2.80	0.50	0.70	0.50	0.50	0.20	0.00	0.00	
1420	2.50	0.00	0.70	0.20	0.00	0.00	0.00	0.20	0.00	0.00	
ID	C-41	C-42	C-43	C-44	C-45	C-46	C-47	C-48	C-49	C-50	
790	0.00	0.00	0.00	0.30	0.00	0.00	0.00	0.00	0.00	0.00	
1420	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ID	PR/T X100	PH/T X100		PR/17		PH/18		PR/PH		CPI	C-MAX
790	1.10	2.60		1.83		0.93		0.42		2.42	C-22
1420	3.09	3.29		1.24		0.85		0.94		3.13	C-23

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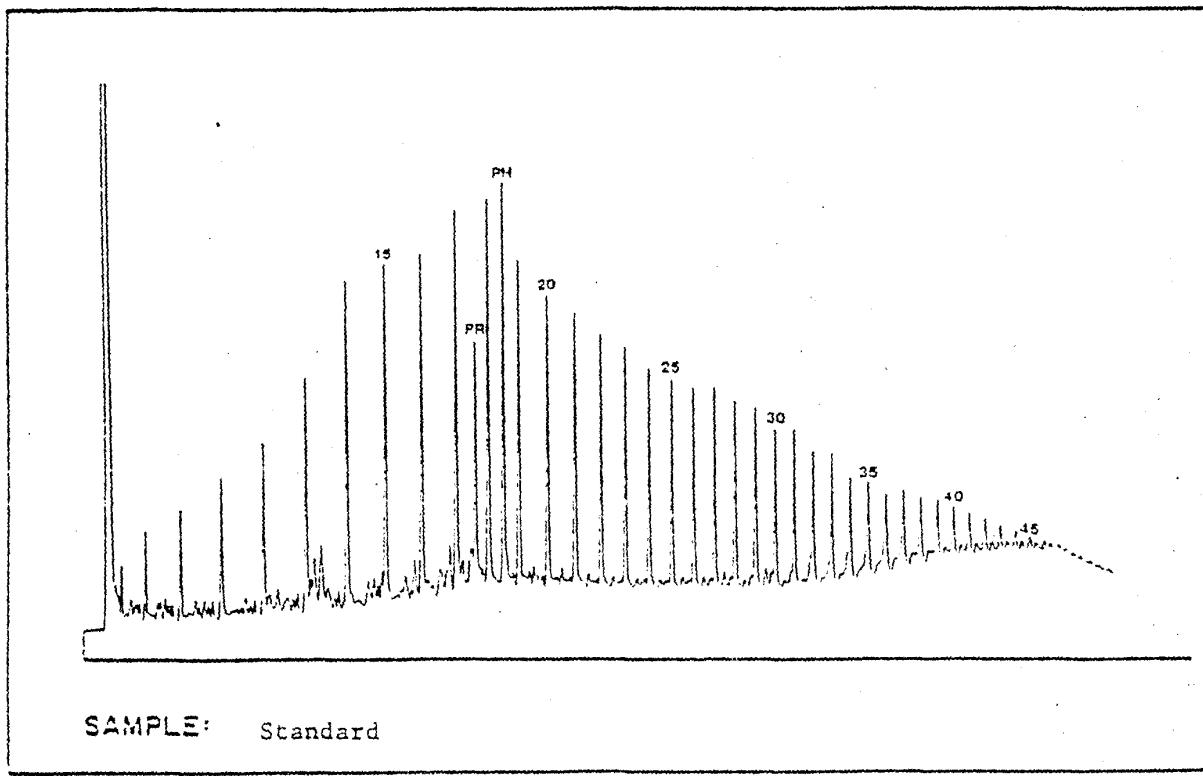
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GAS CHROMATOGRAMS OF C15+ SATURATE HYDROCARBONS Alaska Oil & Gas Cons. Commission
Anchorage

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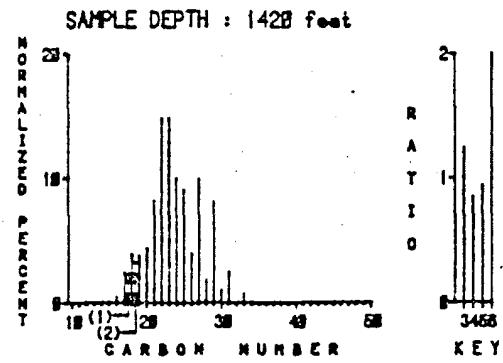
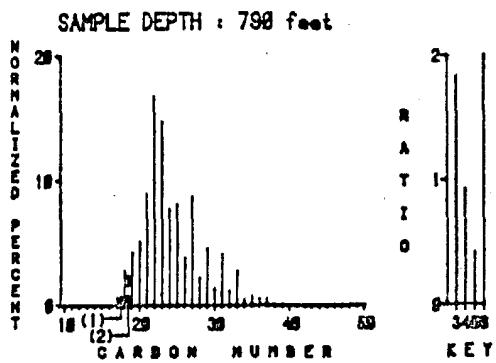
GAS CHROMATOGRAMS OF C15+ SATURATE HYDROCARBONS

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SOCAL MIMIUK PT. #1

1=18C ₁₈ Pristane/Total	3=Pristane/n-C ₁₇	5=Pristane/Phytane
2=18C ₁₈ Phytane/Total	4=Phytane/n-C ₁₈	6=Carbon Pref. Index

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TOTAL ORGANIC CARBON DATA

SOCAL MIMIUK PT. #1

Sample Interval	DEPTH (Feet)	TOC (%)	Sample Interval	DEPTH (Feet)	TOC (%)
100- 220	160	0.18	3880-4000	3940	0.14
730- 850	790	1.61	4510- 630	4570	0.12
1360- 480	1420	8.34	5140- 260	5200	0.06
1990-2110	2050	0.31	5770- 890	5830	0.12
2620- 740	2680	1.11	6211- 310	6261	0.18
3250- 370	3310	0.57			

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Mobil Exploration and Producing Services Inc.

(P)

P.O. BOX 900
DALLAS, TEXAS 75221

November 23, 1981

Mr. William Van Alen
State of Alaska
Alaska Oil & Gas Conservation Commission
3001 Porcupine Drive
Anchorage, Alaska 99501

ESC REQUEST NO. 311A78
VISUAL KEROGEN, THERMAL MATURATION,
TOC AND ROCK-EVAL ANALYSES,
SOCAL NIMIUK PT. #1,
KOTZEBUE, ALASKA

Dear Mr. Van Alen:

This report describes the visual kerogen, thermal maturation, TOC and Rock-Eval results from the SOCAL Nimiuk Pt. #1, Kotzebue, Alaska. Visual kerogen and vitrinite reflectance analyses are based on 19 ditch samples taken at 300' intervals between 100' and 6310' (TD). TOC and Rock-Eval analyses are based on 11 ditch samples taken at 510' intervals between 100' and 6310' (TD). A plot of the low-gray Ro means (figure 1), a summary of the thermal maturity and hydrocarbon potential (table 1), a kerogen analysis sheet (table 2), edited Ro histogram plots, and a copy of the TOC and Rock-Eval reports are included.

Results from TAI analysis of the SOCAL Nimiuk Pt. #1 indicate that the section penetrated from 100' to 5770' is transitionally mature. The vitrinite data indicate that the 100' to 5770' interval is thermally immature. It is possible the dark color of the spores was caused by oxidation or by the fact that spores tend to be thicker walled than the preferred bissacates.

Results from visual kerogen analysis of the SOCAL Nimiuk Pt. #1 samples are listed on the attached kerogen analysis sheet (table 2). It should be noted that all of the samples analyzed are dominated by cellulosic (gas type) kerogens. Fluorescence analysis indicates traces of lipid rich kerogens are present down to about 2600'.

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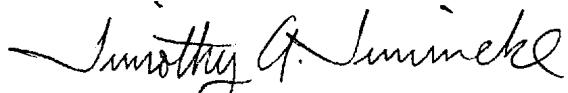
November 23, 1981

Results from vitrinite reflectance studies on the SOCAL Nimiuk Pt. #1 well indicate that the sediments penetrated down to 5830' are all thermally immature. Igneous and metamorphic rock fragments are found below 5900'. A summary of the thermal maturity and hydrocarbon potential of the SOCAL Nimiuk Pt. #1 samples are listed in Table 1. Edited histogram plots of the Ro readings from each sample are enclosed. The vitrinite reflectance measurements were made by R. R. Taylor.

Results from TOC analysis range from "poor" below 3940' to "very good" for the 1420' sample. Pyrolysis indicates little hydrocarbon potential for any of the samples, and gas as the most likely hydrocarbon they could generate during maturation.

Time requirements for this job were charged to ESC Request No. 311A78. If you have any questions concerning the results or interpretations, please do not hesitate to contact me.

Very truly yours,



T. A. Timmcke
Exploration Services Center
Applied Stratigraphy

TAT/jg
Attachments

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TABLE 1
Thermal Maturation and Visual Kerogen Analyses
Soal Nimiuk Pt. No. 1, Kotzebue, Alaska

<u>DEPTH OR SPL. NO.</u>	<u>LOW-GRAY Ro MEAN</u>	<u>% POP.</u>	<u>FIRST HIGH-GRAY Ro MEAN</u>	<u>% POP.</u>	<u>TAI</u>	<u>THERMAL MATURITY</u>	<u>KEROGEN TYPE</u>	<u>HYDROCARBON POTENTIAL/REMARKS</u>
100'	0.19	18	0.36	37		Immature	Cellulosic	Gas type kerogen
460'	0.23	65	0.69	33		Immature	Cellulosic	Gas type kerogen
820'	0.25	85	1.64	15		Immature	Cellulosic	Gas type kerogen
1180'	0.28	36	0.58	37	2	Immature	Cellulosic	Gas type kerogen
1540'	0.25	69	0.99	31	2	Immature	Cellulosic	Gas type kerogen
1900'	0.25	74	1.10	26	1+	Immature	Cellulosic	Gas type kerogen
2260'	0.34	85	1.75	15		Immature	Cellulosic	Gas type kerogen
2530'	0.35	80	0.91	20		Immature	Cellulosic	Gas type kerogen
2890'	0.31	74	2.29	17		Immature	Cellulosic	Gas type kerogen
3250'	0.37	66	0.72	34		Immature	Cellulosic	Gas type kerogen
3650'	0.35	100	-	-		Immature	Cellulosic	Gas type kerogen
3970'	0.39	45	0.59	32		Immature	Cellulosic	Gas type kerogen
4330'	0.36	100	-	-		Immature	Cellulosic	Gas type kerogen
4690'	0.37	72	1.36	25		Immature	Cellulosic	Gas type kerogen
5050'	0.41	47	0.74	38		Immature	Cellulosic	Gas type kerogen
5410'	0.44	85	0.87	15	2	Immature RECEIVED	Cellulosic	Gas type kerogen

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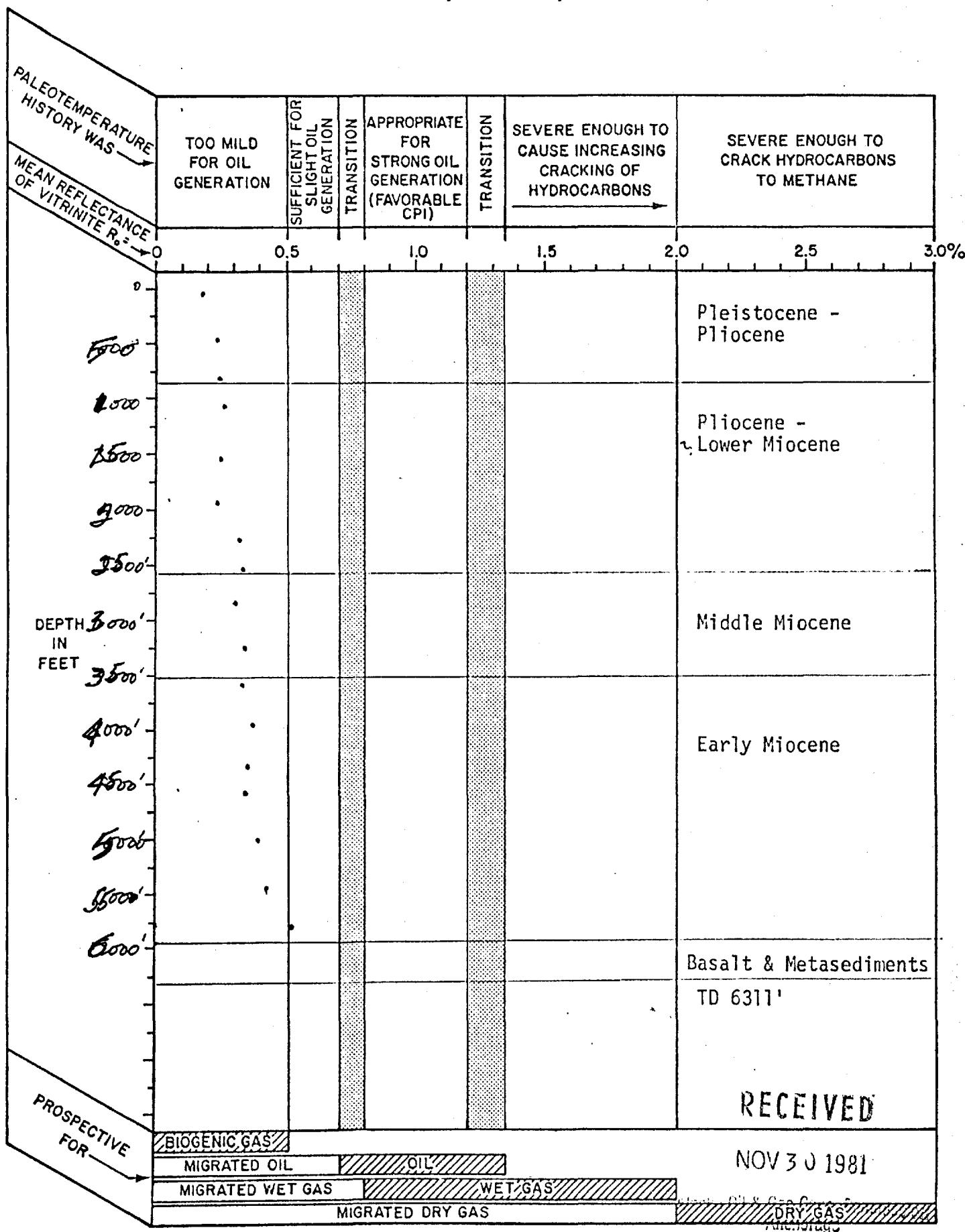
TABLE 1
Thermal Maturation and Visual Kerogen Analyses
SoCal Nimiuk Pt. No. 1, Kotzebue, Alaska

<u>DEPTH OR SPL. NO.</u>	<u>LOW-GRAY Ro MEAN</u>	<u>% POP.</u>	<u>FIRST HIGH-GRAY Ro MEAN</u>	<u>% POP.</u>	<u>TAI</u>	<u>THERMAL MATURITY</u>	<u>KEROGEN TYPE</u>	<u>HYDROCARBON POTENTIAL/REMARKS</u>
5770'	0.51	68	1.03	32	2,2+	Immature	Cellulosic	Gas type kerogen
6130'	-	-	-	-	-	-	-	Metamorphic rocks
6250'	-	-	-	-	-	-	-	Metamorphic rocks

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FIGURE 1
Plot of Low-Gray Ro Means
SOCAL Nimiuk Pt. #1, Kotzebue, Alaska



ESC No. 311A78

TABLE 2
ORGANIC RESIDUE (KEROGEN) ANALYSIS

M-005
(Rev. 01-80)

ROBERTSON RESEARCH (U.S.) INC.

REPORT NO. 488

GEOCHEMICAL EVALUATION OF
ELEVEN SAMPLES FROM THE
SOCAL NIMIUK POINT #1 WELL

by
Mary Michael Page

Project No. RRUS/812/II/T/50

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Alaska Oil & Gas Cons. Commission
Anchorage

Prepared by:

Robertson Research (U.S.) Inc.
16730 Hedgecroft, Suite 306
Houston, Texas 77060

Prepared for:

Mobil Exp. & Pro. Serv. Inc
P. O. Box 900
Dallas, Texas 75221

September 25, 1981

ROBERTSON
RESEARCH (U.S.) INC.

INTRODUCTION

Eleven samples were forwarded for Total Organic Carbon (TOC) analysis and Rock-Eval pyrolysis. The Rock-Eval pyrolysis was to be run regardless of the TOC value. Two of the samples exhibited high amounts of bitumen, as evidenced by the coalescence of the pyrolysis S1 and S2 into a single peak. The suggestion was made to, and accepted by, the client to extract these samples and evaluate both the extracted sample and the recovered extract.

SUMMARY

The source richness based on TOC ranges from "non-source" below 3,940 feet to "very good" for sample 1420. Pyrolysis generally indicates "nonsource" amounts of hydrogen-poor kerogen. The T-max values indicate very immature material but may not be representative for the samples with the very low S2 values or with the single S1 + S2 peak. For samples 790 and 1420, the S1 and S2 peaks merge, suggesting the presence of significant amounts of bitumen. A portion of the sample was extracted and rerun; however the general shape of the pyrogram did not change. The extract consists of moderate amounts of immature bitumen, and gives no indication of the type of material responsible for the anomalous Rock-Eval response.

The increase in TOC for sample 1420 is reproducible and probably due to the removal of sulfur together with the bitumen during extraction. The high per cent carbon and character of the chromatogram are consistent with a coaly type material, which accumulates in an environment conducive to high sulfur concentrations.

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SOCAL MIMIUK PT. #1

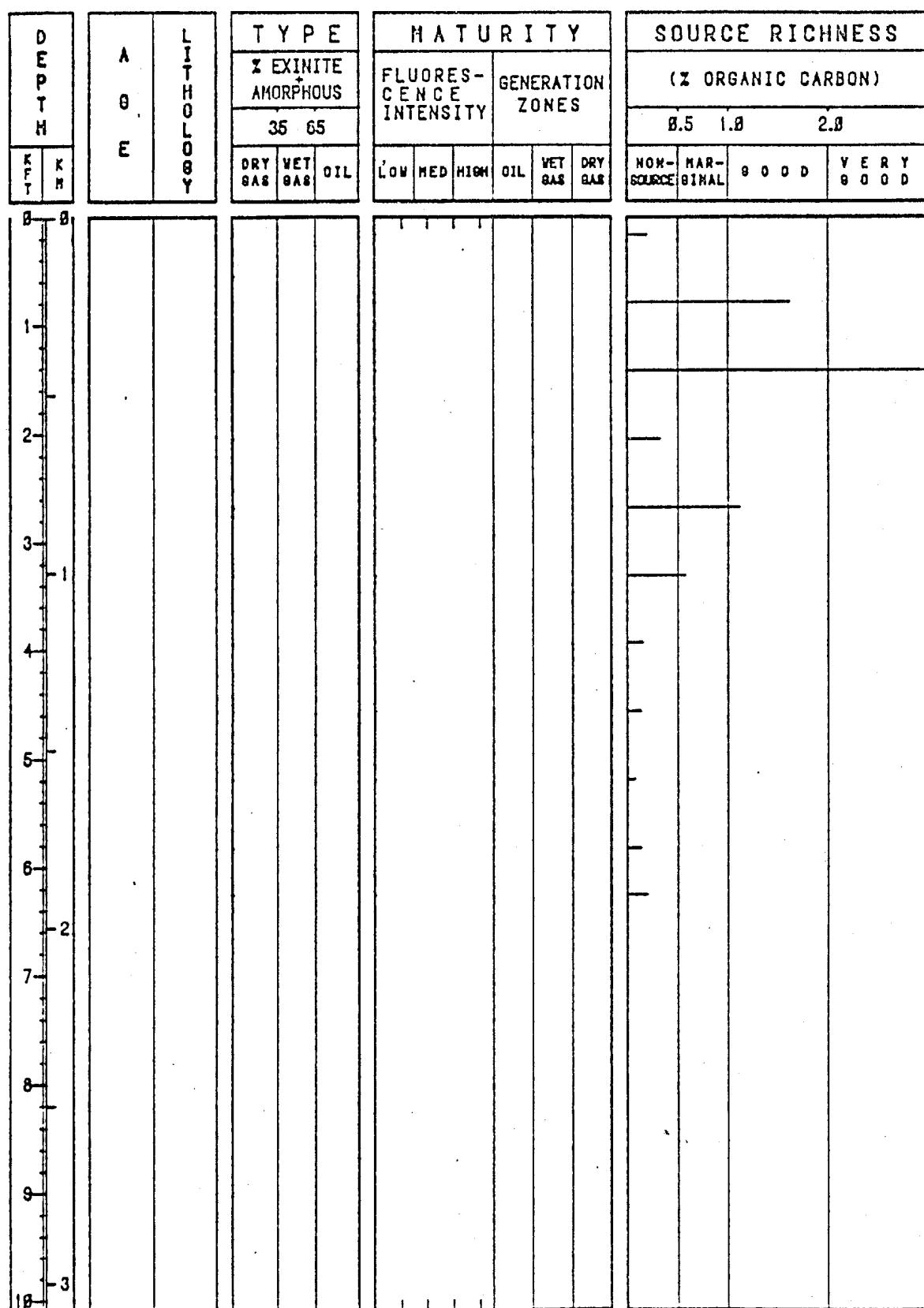


FIGURE 1: SUMMARY PLOTS SHOWING KEROGEN TYPES, MATURITY,
AND SOURCE RICHNESS (SEE APPENDICES I AND II)

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SOCAL MIMIUK PT. #1

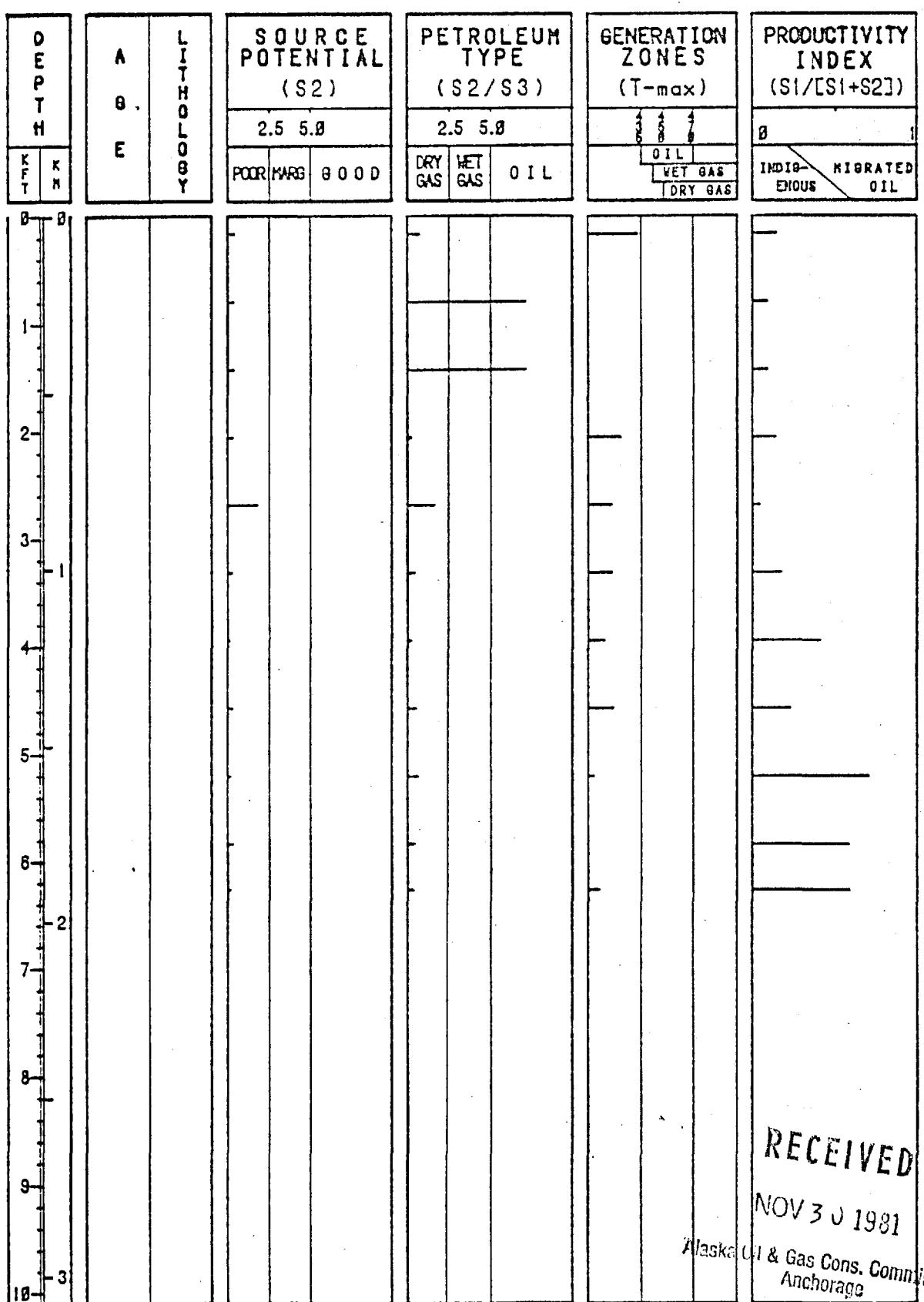


FIGURE 2: SUMMARY PLOTS OF ROCK-EVAL PYROLYSIS DATA (APPENDIX II)

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APPENDIX I

TOTAL ORGANIC CARBON DATA

Total organic carbon is determined by pulverizing the sample, treating a carefully weighed portion with warm hydrochloric acid to remove carbonate minerals, and analysing the residue for carbon content with a Leco carbon analyser. It is generally accepted that samples with less than about 0.5 percent TOC cannot yield sufficient petroleum to form commercial deposits and are therefore considered nonsources; samples with between 0.5 and 1.0 TOC are rated as marginal in source quality; and samples with more than 1.0 TOC are considered to be good in source quality.

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APPENDIX II

ROCK-EVAL PYROLYSIS DATA

Rock-Eval data are expressed as mg/g of rock and include four basic parameters: 1) S_1 represents the quantity of free hydrocarbons present in the rock and is roughly analogous to the solvent extractable portion of the organic matter; 2) S_2 represents the quantity of hydrocarbons released by the kerogen in the sample during pyrolysis; 3) S_3 is related to the amount of oxygen present in the kerogen; and 4) T-max, in °C, is the temperature at which the maximum rate of generation (of the S_2 peak) occurs and can be used as an estimate of thermal maturity.

In addition, the ratio S_2/S_3 provides a general indication of kerogen quality (type) and reveals whether oil or gas are likely to be generated. The ratio $S_1/(S_1+S_2)$, or the productivity index, is an indication of the relative amount of free hydrocarbons (in place or migrated) present in the sample. Hydrogen and oxygen index values are in mg of hydrocarbons (S_2 peak) or carbon dioxide (S_3 peak) per gram of organic carbon. When plotted against each other on a van Krevelen-type diagram, information on kerogen type and maturity can be obtained.

Data are interpreted in the following manner:

Source Potential - values of S_2	<2.5	: poor
	2.5-5.0	: marginal
	>5.0	: good

Petroleum Type - value of S_2/S_3	<2.5	: dry gas
	2.5-5.0	: wet gas
	>5.0	: oil

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Generation Zones - values of T-max	<435	: immature	NOV 30 1981
	435-470	: oil	
	450 +	: gas	Alaska Oil & Gas Cons. Commission Anchorage

Productivity Index - high values of $S_1/(S_1+S_2)$ indicate migrated hydrocarbons.

ROCK-EVAL PYROLYSIS RAW DATA

SOCAL MIMIUK PT. #1

DEPTH (FEET)	S1	S2	S3	S2/S3	S1/(S1+S2)	T-MAX
160	0.051	0.326	0.519	0.629	0.135	432
790	---	---	---	---	---	---
1420	---	---	---	---	---	---
2050	0.040	0.261	1.746	0.150	0.132	421
2680	0.062	1.719	1.121	1.533	0.035	415
3310	0.236	0.181	0.589	0.307	0.164	415
3940	0.025	0.238	0.378	0.100	0.402	410
4570	0.263	0.218	0.533	0.409	0.223	416
5200	0.297	0.129	0.242	0.532	0.598	403
5830	0.363	0.259	0.877	0.295	0.577	392
6260	0.111	0.080	0.361	0.227	0.582	406

HYDROGEN AND OXYGEN INDICES FROM ROCK-EVAL
PYROLYSIS DATA, WITH TOC DATA

SOCAL MIMIUK PT. #1

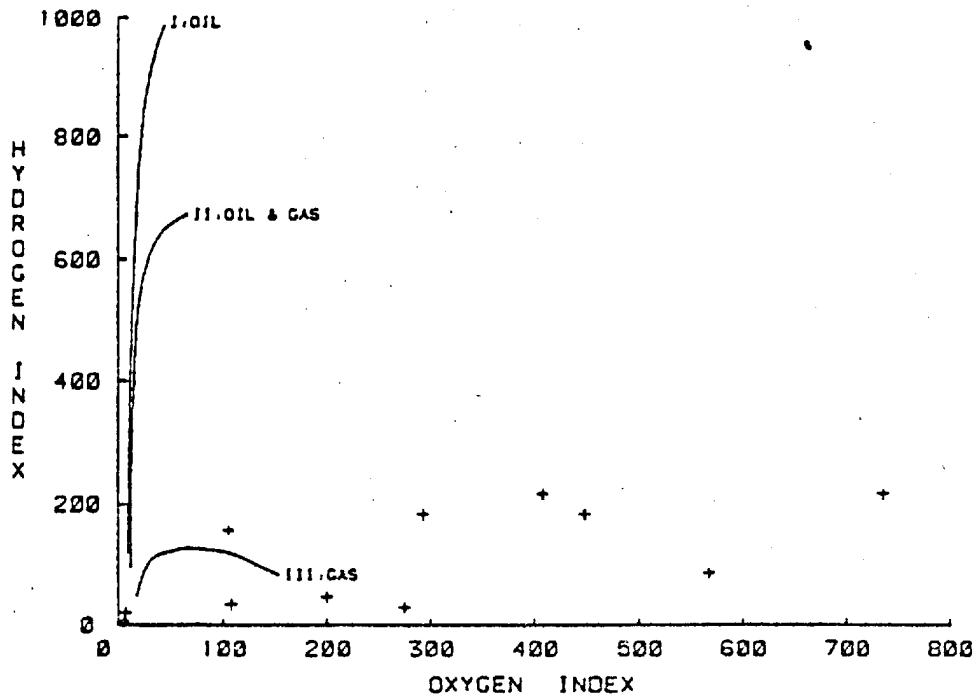
DEPTH (FEET)	HYDROGEN INDEX (mg HC/g TOC)	OXYGEN INDEX (mg CO ₂ /g TOC)	TOC (%)
160	181	288	0.18
790	---	---	1.61
1420	---	---	8.34
2050	84	563	0.31
2680	155	101	1.11
3310	32	123	0.57
3940	27	270	0.14
4570	182	444	0.12
5200	215	403	0.06
5830	216	731	0.12
6260	44	195	0.18

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KEROGEN TYPE DETERMINATION FROM ROCK-EVAL.
PYROLYSIS DATA (APPENDIX II).

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ROCK-EVAL PYROLYSIS RAW DATA

SOCAL MIMIUK PT. #1

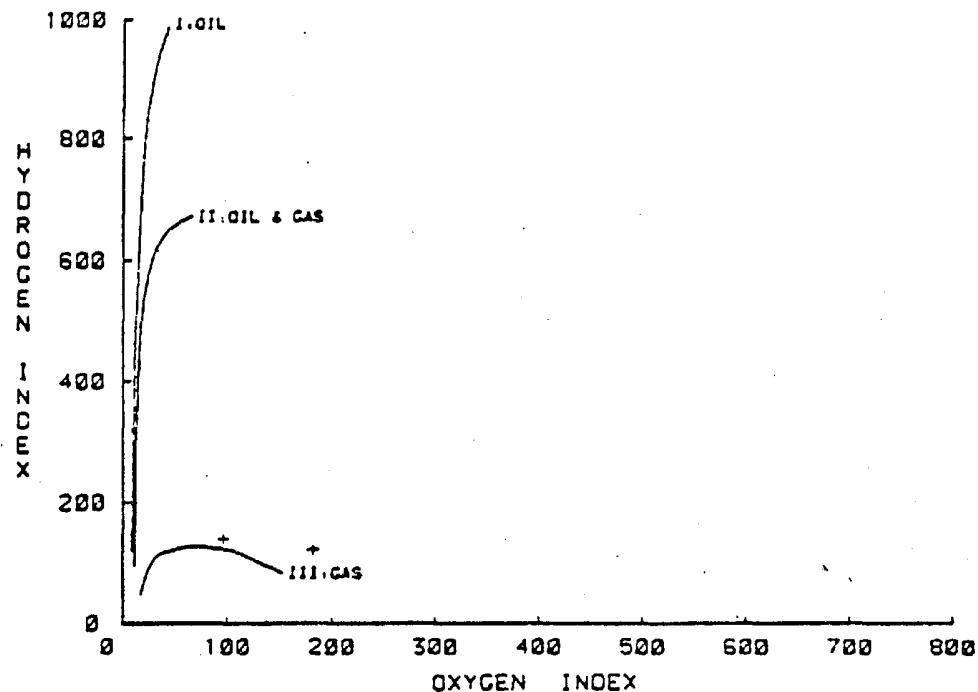
DEPTH (FEET)	S1+S2	S3	S2/S3	S1/(S1+S2)	T-MAX
790	1.949	2.874	0.678	0.000	393
1420	11.512	7.731	1.489	0.000	392

HYDROGEN AND OXYGEN INDICES FROM ROCK-EVAL
PYROLYSIS DATA, WITH TOC DATA

SOCAL MIMIUK PT. #1

DEPTH (FEET)	HYDROGEN INDEX (mg HC/g TOC)	OXYGEN INDEX (mg CO ₂ /g TOC)	TOC (%)
790	121	179	1.61
1420	138	93	8.34

SOCAL MIMIUK PT. #1



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FIGURE 3: KEROGEN TYPE DETERMINATION FROM ROCK-EVAL. NOV 30 1981
PYROLYSIS DATA (APPENDIX II).

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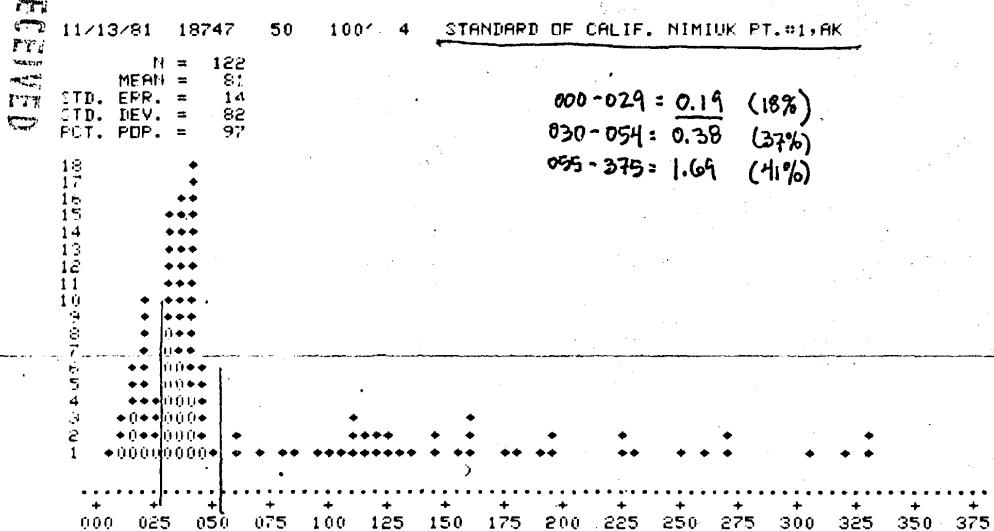
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3	18749	50	820'	4	STANDARD OF CALIF. NIMIUK PT.#1,AK	11/11/81RT
4	18750	50	1180'	4	STANDARD OF CALIF. NIMIUK PT.#1,AK	11/11/81PT
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6	18752	50	1900'	4	STANDARD OF CALIF. NIMIUK PT.#1,AK	11/11/81PT
7	18753	50	2260'	4	STANDARD OF CALIF. NIMIUK PT.#1,AK	11/11/81PT
8	18754	50	2530'	4	STANDARD OF CALIF. NIMIUK PT.#1,AK	11/11/81PT
9	18755	50	2890'	4	STANDARD OF CALIF. NIMIUK PT.#1,AK	11/12/81PT
10	18756	50	3250'	4	STANDARD OF CALIF. NIMIUK PT.#1,AK	11/12/81PT
11	18757	50	3650'	4	STANDARD OF CALIF. NIMIUK PT.#1,AK	11/12/81PT
12	18758	50	3970'	4	STANDARD OF CALIF. NIMIUK PT.#1,AK	11/12/81PT
13	18759	50	4330'	4	STANDARD OF CALIF. NIMIUK PT.#1,AK	11/12/81PT
14	18760	50	4690'	4	STANDARD OF CALIF. NIMIUK PT.#1,AK	11/12/81PT
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17	18763	50	5770'	4	STANDARD OF CALIF. NIMIUK PT.#1,AK	11/12/81PT
18	18764	50	6130'	4	STANDARD OF CALIF. NIMIUK PT.#1,AK	11/12/81PT
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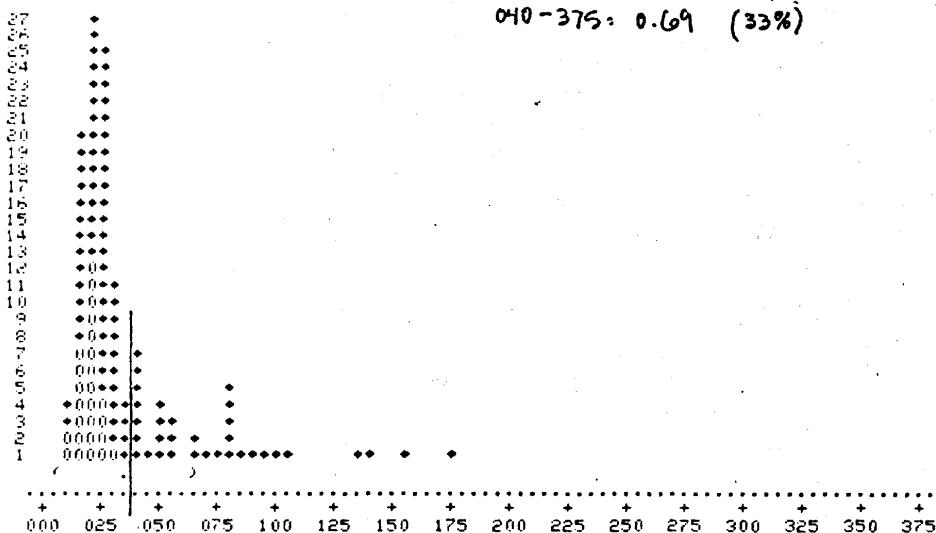
NOV 30 1981



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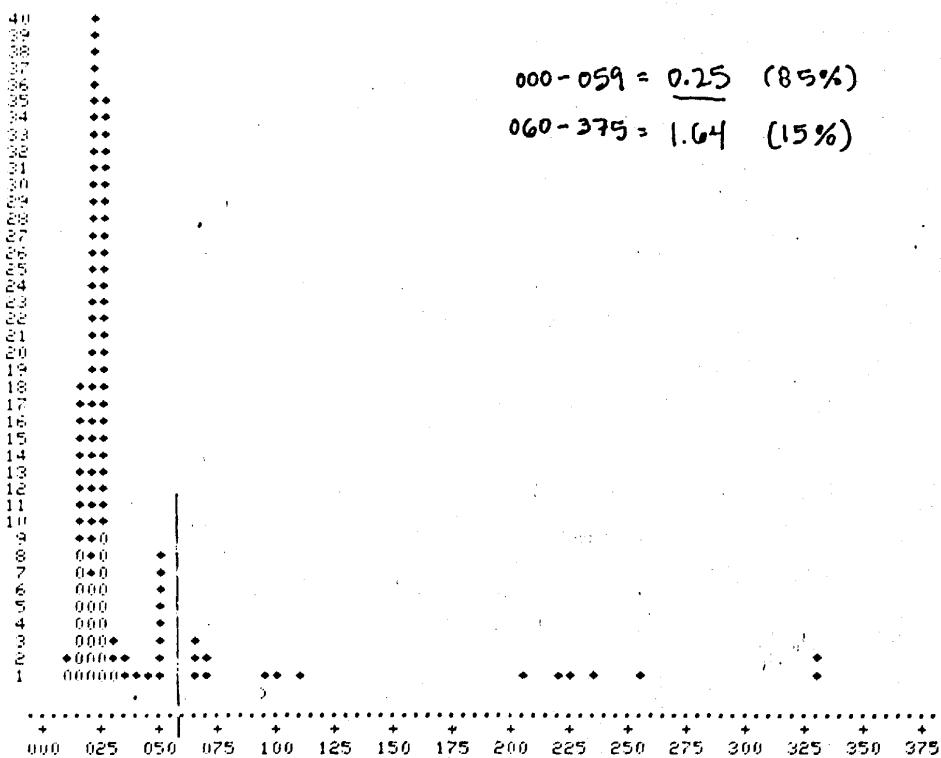
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040-375 = 0.69 (33%)



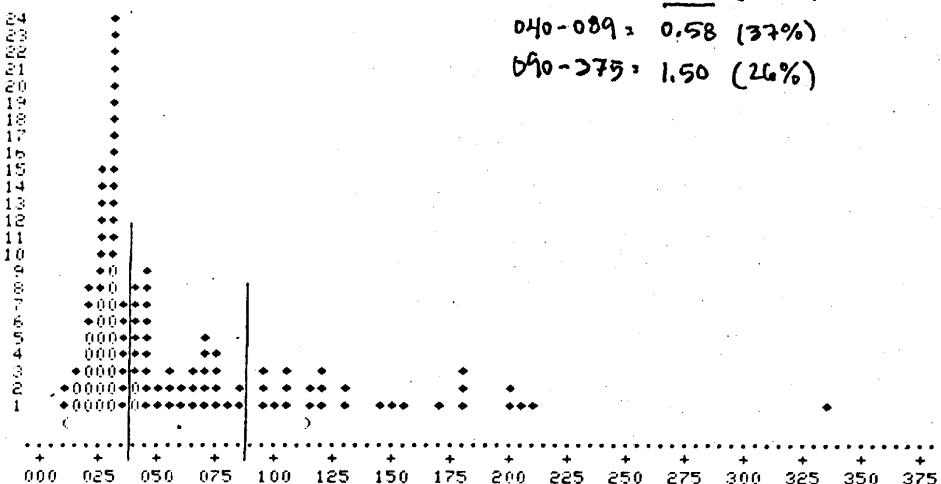
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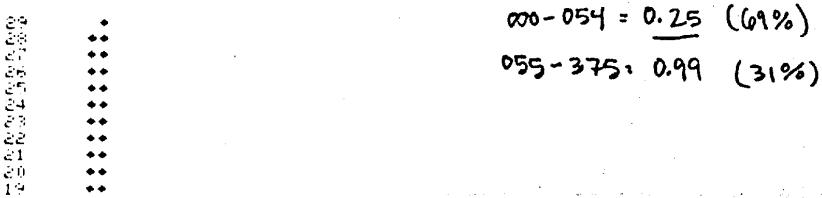
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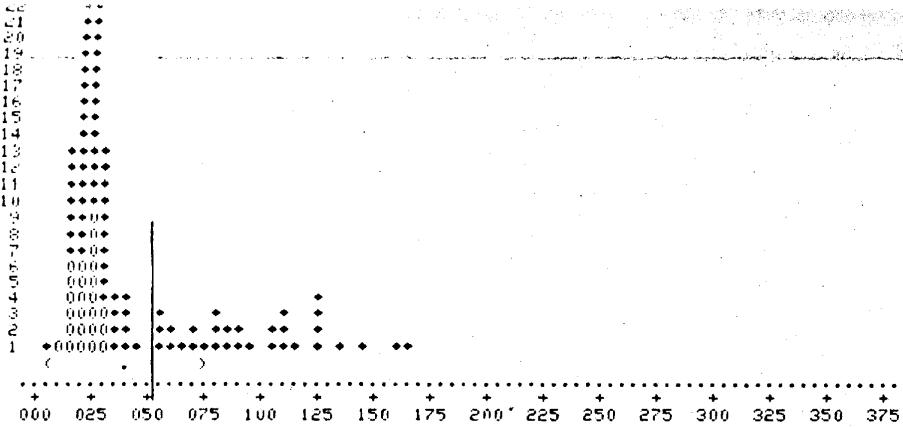
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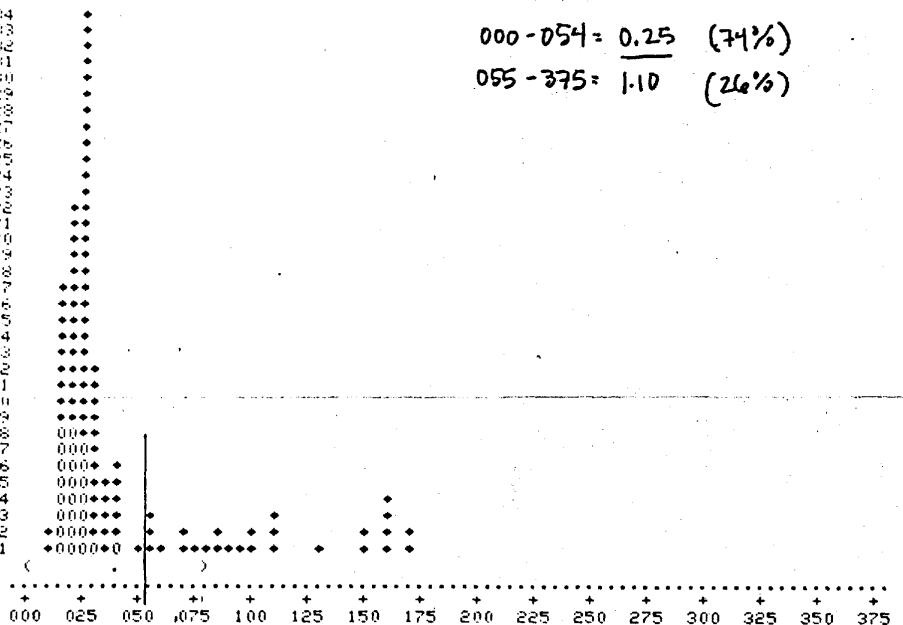


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$$000 - 054 = \underline{0.25} \quad (74\%)$$

$$055 - 375 = 1.10 \quad (26\%)$$

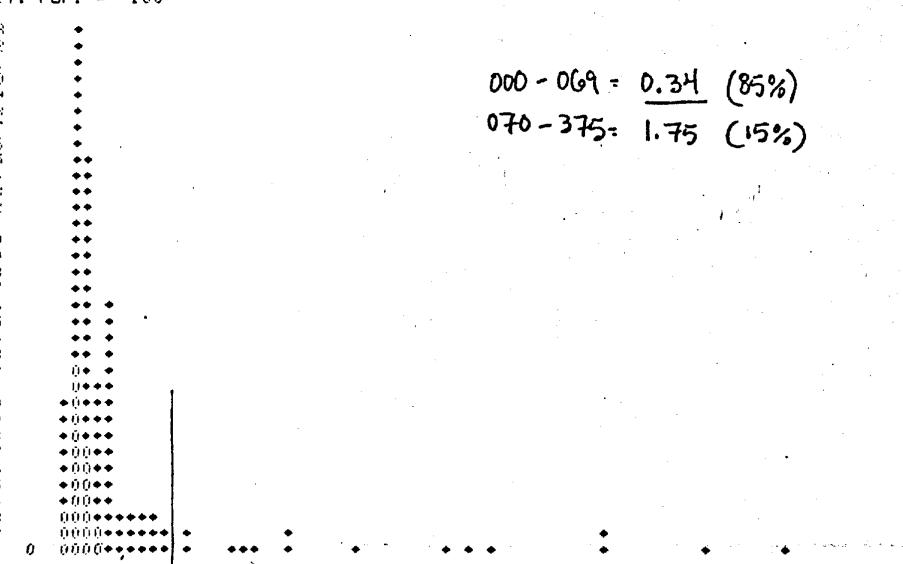


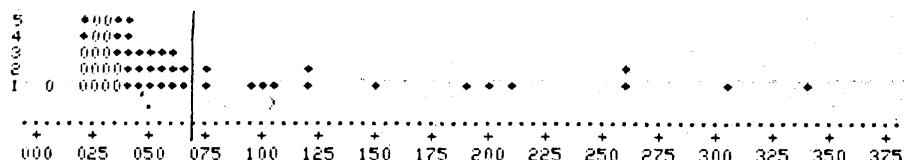
11/13/81 18753 50 2260' 4 STANDARD OF CALIF. NIMIUK PT.#1,AK

N = 125
MEAN = 51
STD. ERR. = 9
STD. DEV. = 54
PCT. POP. = 100

$$000 - 069 = \underline{0.34} \quad (85\%)$$

$$070 - 375 = 1.75 \quad (15\%)$$



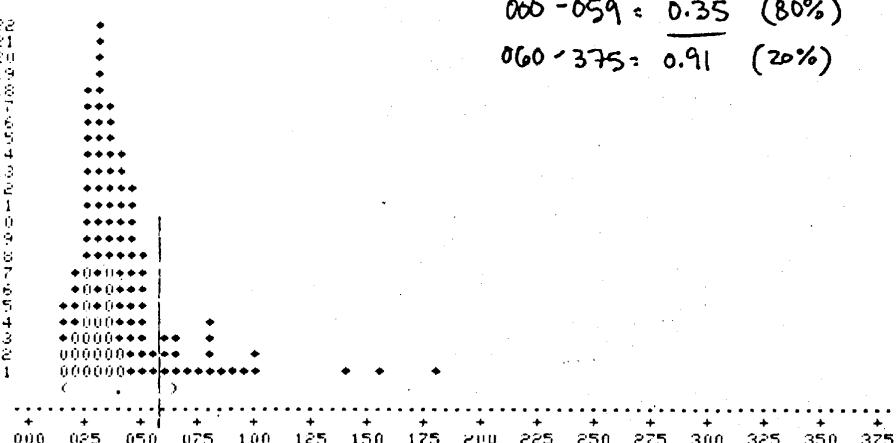


11/13/81 18754 50 2530' 4 STANDARD OF CALIF. NIMIUK PT.#1,AK

N = 125
MEAN = 44
STD. ERR. = 4
STD. DEV. = 25
PCT. POP. = 100

$$000-059 = 0.35 \text{ (80\%)}$$

$$060-375 = 0.91 \text{ (20\%)}$$



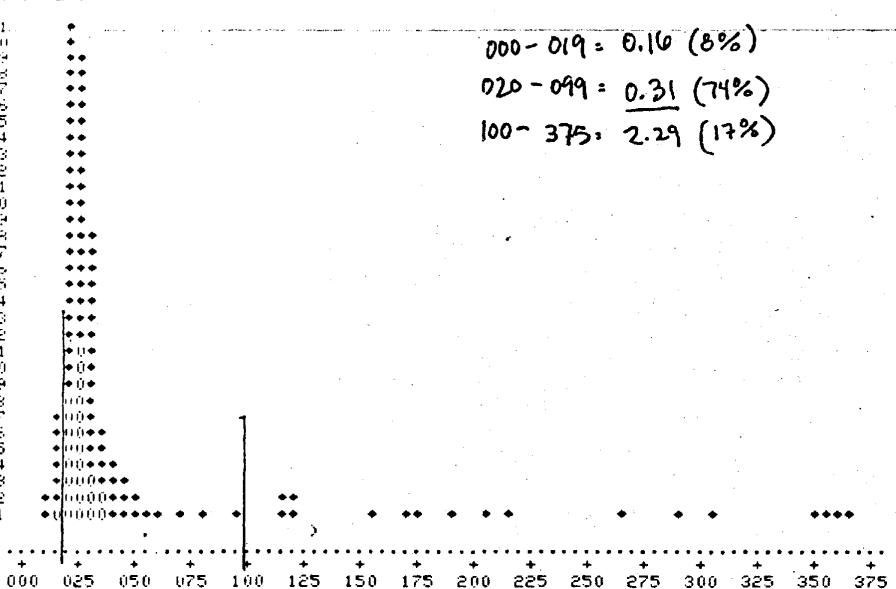
11/13/81 18755 50 2890' 4 STANDARD OF CALIF. NIMIUK PT.#1,AK

N = 124
MEAN = 57
STD. ERR. = 13
STD. DEV. = 27
PCT. POP. = 93

$$000-019 = 0.16 \text{ (8\%)}$$

$$020-099 = 0.31 \text{ (74\%)}$$

$$100-375 = 2.29 \text{ (17\%)}$$

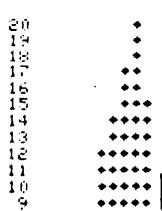


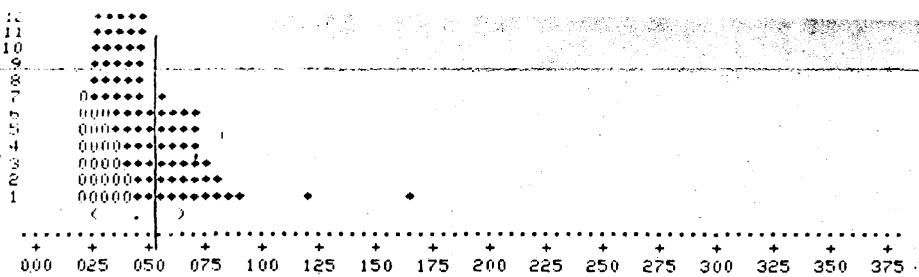
11/13/81 18756 50 3250' 4 STANDARD OF CALIF. NIMIUK PT.#1,AK

N = 125
MEAN = 45
STD. ERR. = 3
STD. DEV. = 20
PCT. POP. = 100

$$000-054 = 0.37 \text{ (66\%)}$$

$$055-375 = 0.72 \text{ (34\%)}$$

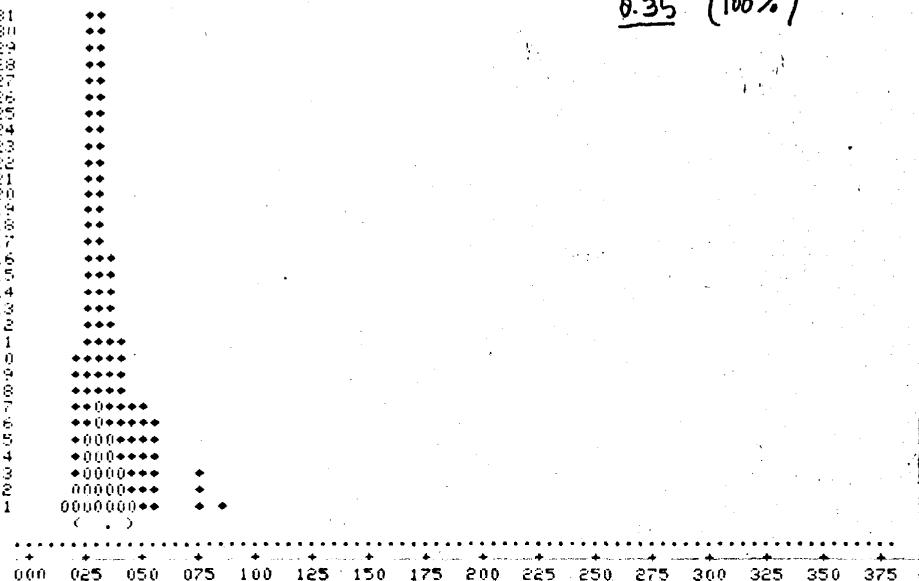




11/13/81 18757 50 36501 4 STANDARD OF CALIF. NIMIUK PT.#1,AK

N = 124
MEAN = 35
STD. EPP. = 12
STD. DEV. = 12
PCT. POP. = 100

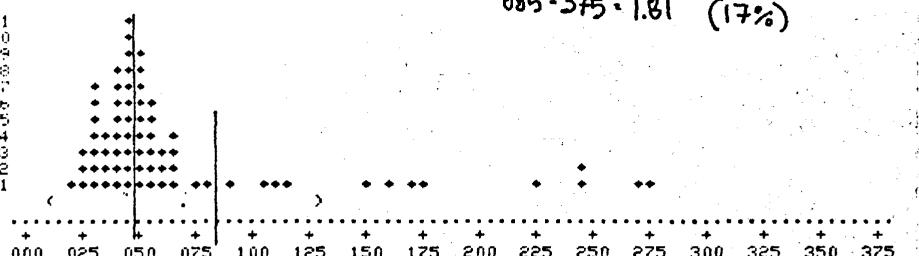
0.35 (100%)



11/13/81 18758 50 39701 4 STANDARD OF CALIF. NIMIUK PT.#1,AK

N = 72
MEAN = 72
STD. EPP. = 13
STD. DEV. = 59
PCT. POP. = 95

000-049 = 0.39 (45%)
050-084 = 0.59 (32%)
085-375 = 1.81 (17%)

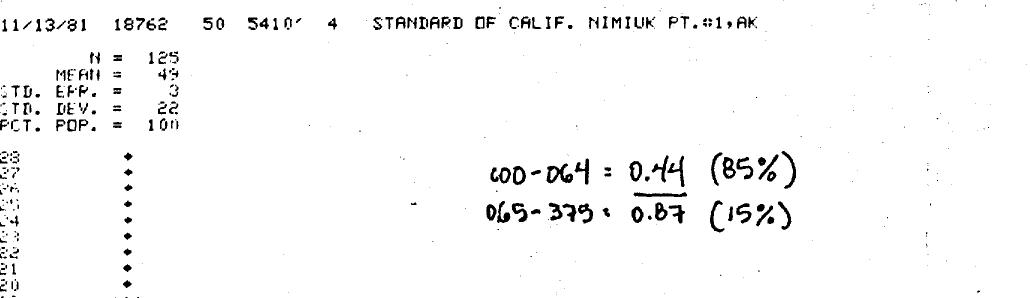
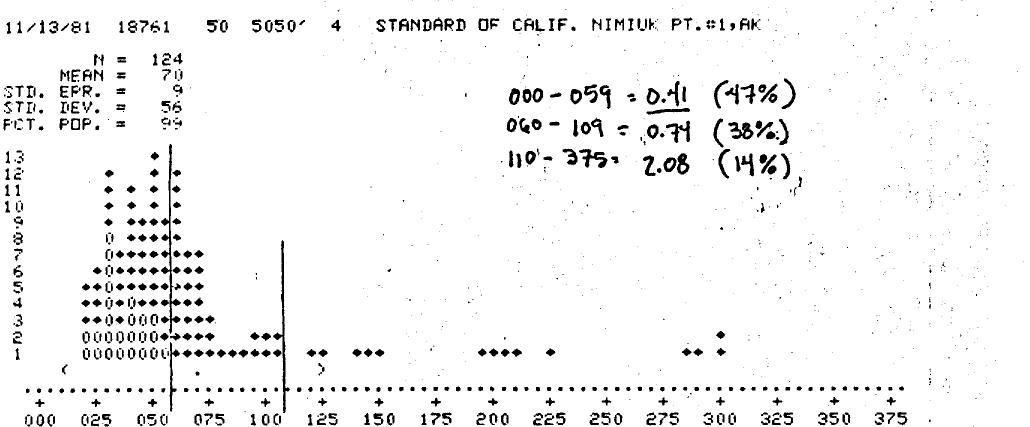
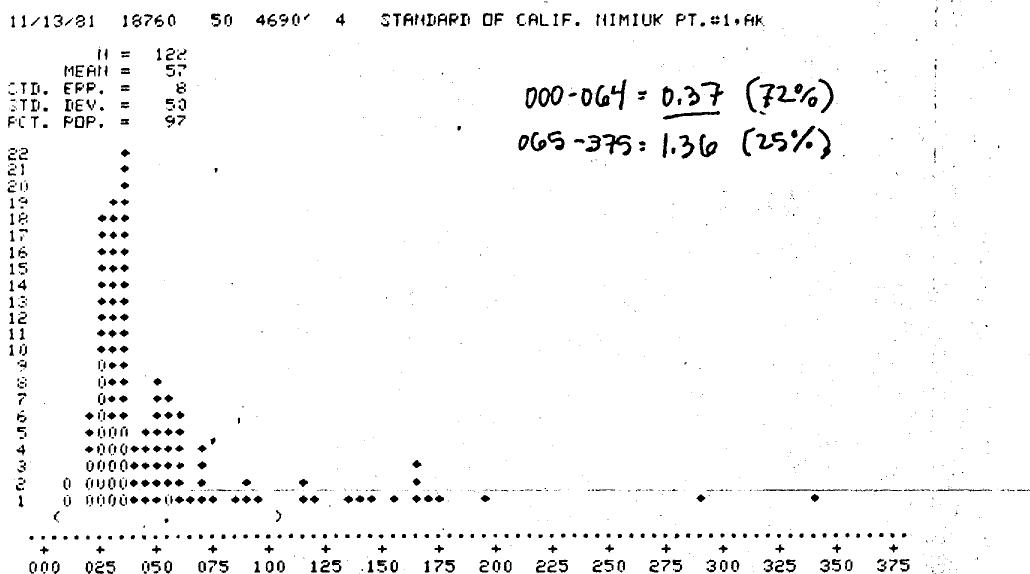
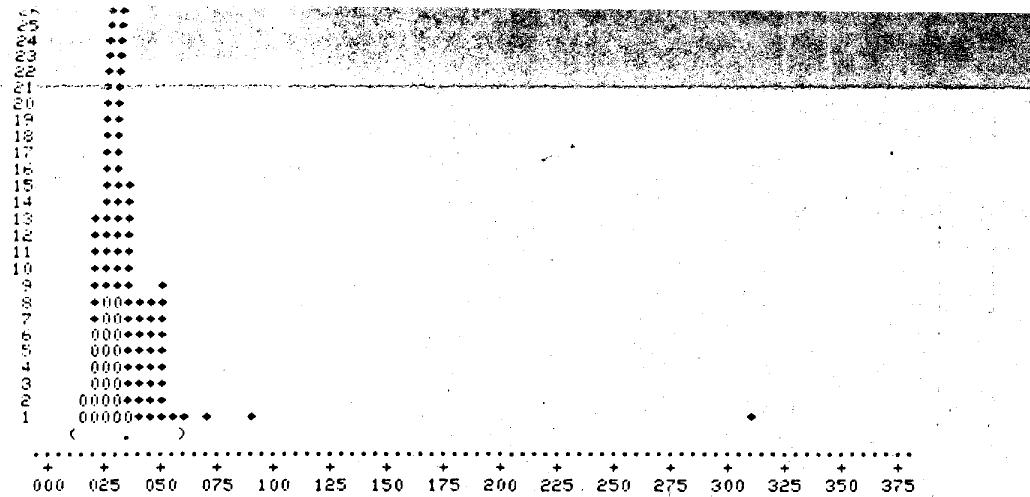


11/13/81 18759 50 43301 4 STANDARD OF CALIF. NIMIUK PT.#1,AK

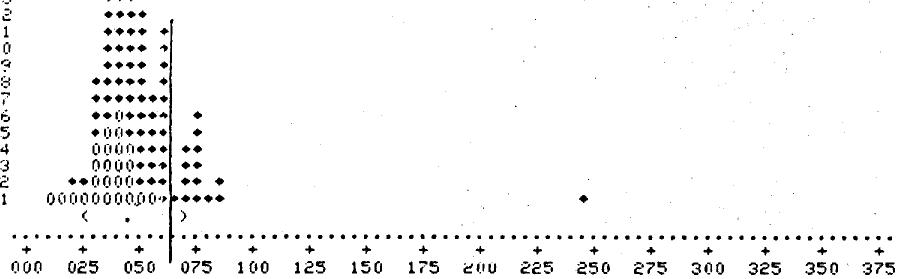
N = 125
MEAN = 36
STD. EPP. = 4
STD. DEV. = 26
PCT. POP. = 100

0.36 (100%)





069-375 = 0.57 (15%)

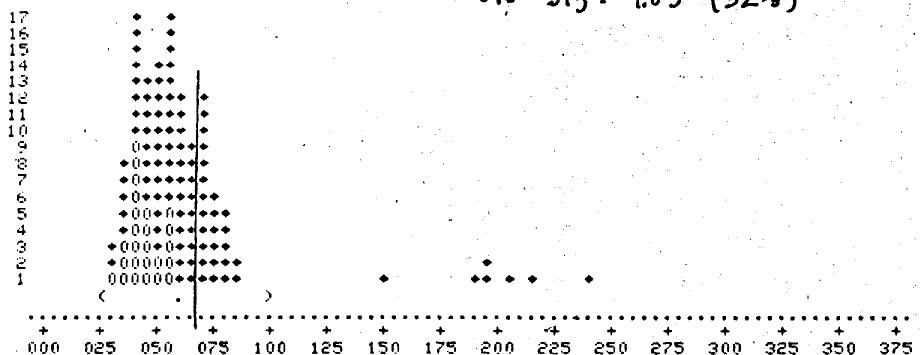


11/13/81 18763 50 5770' 4 STANDARD OF CALIF. NIMIUK PT.#1,AK

N = 125
MEAN = 64
STD. EPR. = 6
STD. DEV. = 36
PCT. POP. = 100

000-069 = 0.51 (68%)

070-375 = 1.03 (32%)

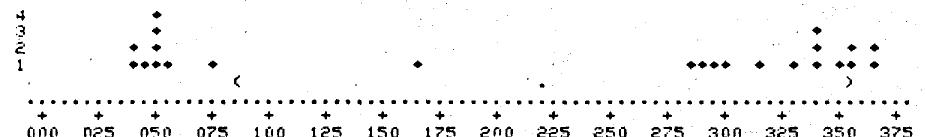


METAMORPHIC ROCKS FROM ~ 5950' to T.D.

11/13/81 18764 50 6130' 4 STANDARD OF CALIF. NIMIUK PT.#1,AK

N = 24
MEAN = 220
STD. EPR. = 55
STD. DEV. = 135
PCT. POP. = 64

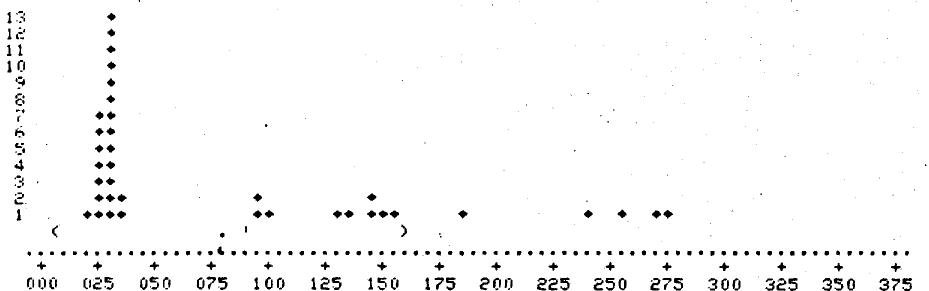
INSUFFICIENT DATA



11/13/81 18765 50 6250' 4 STANDARD OF CALIF. NIMIUK PT.#1,AK

N = 37
MEAN = 83
STD. EPR. = 25
STD. DEV. = 78
PCT. POP. = 97

INSUFFICIENT DATA

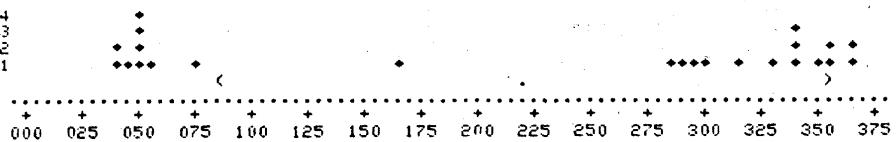


METAMORPHIC ROCKS FROM ~5950' to T.D.

11/13/81 18764 50 6130' 4 STANDARD OF CALIF. NIMIUK PT.#1,AK

N = 24
MEAN = 220
STD. ERR. = 55
STD. DEV. = 135
PCT. PDP. = 64

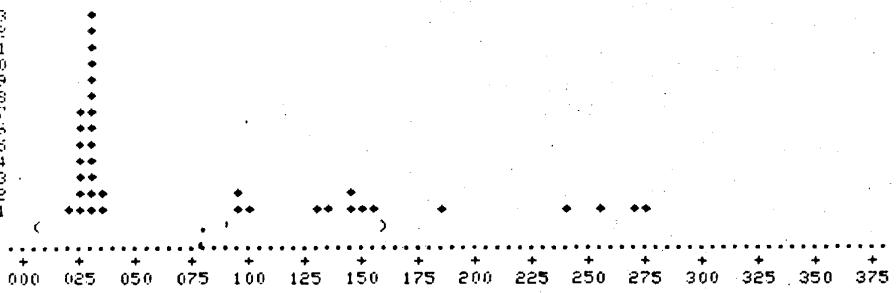
INSUFFICIENT DATA



11/13/81 18765 50 6250' 4 STANDARD OF CALIF. NIMIUK PT.#1,AK

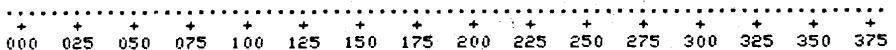
N = 37
MEAN = 83
STD. ERR. = 25
STD. DEV. = 78
PCT. PDP. = 97

INSUFFICIENT DATA



11/13/81 99999 EDT

N = 0
MEAN = 0
STD. ERR. = 0
STD. DEV. = 0
PCT. PDP. = 0



**COMMAND =

original

Mobil Exploration and Producing Services Inc.

P.O. BOX 900
DALLAS, TEXAS 75221

November 24, 1981

Mr. William Van Alen
State of Alaska
Alaska Oil & Gas Conservation Commission
3001 Porcupine Drive
Anchorage, Alaska 99501

ESC REQUEST NO. 311A78
VISUAL KEROGEN AND
THERMAL MATURATION ANALYSES,
BENEDUM NULATO UNIT NO. 1,
NORTON SOUND, ALASKA

Dear Mr. Van Alen:

This report describes the visual kerogen and thermal maturation results from the Benedum Nulato Unit No. 1, Norton Sound, Alaska. Visual kerogen and vitrinite reflectance analyses are based on 31 ditch samples taken at 300' intervals between 0' and 11800' (TD). A summary of the thermal maturity and hydrocarbon potential (table 1), a kerogen analysis sheet (table 2), and histogram plots of the Ro measurements are included.

Results from visual kerogen analysis of the Benedum Nulato Unit No. 1 samples are listed on the attached kerogen analysis sheet (table 2). It should be noted that all of the samples analyzed are dominated by cellulosic (gas type) kerogens. Fluorescence analysis supports this observation. Kerogen slides prepared from these samples were barren of palynomorphs, hence, TAI analysis was not possible.

Results from vitrinite reflectance studies on the Nulato Unit No. 1 well indicate that all the sediments penetrated to a depth of 11800' (TD) are thermally overmature. Only the first sample from 0'-100' contains a low-gray Ro population which can be attributed to surface contamination. A summary of the thermal maturity and hydrocarbon potential of the Nulato Unit No. 1 samples is also included with the report (table 1). Histogram plots of the Ro readings from each sample are attached. No plot was made of the low-gray Ro means because the means are too high and plot off scale. The reflectance measurements used in this study were made by R. R. Taylor.

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Alaska Oil & Gas Conservation Commission
Anchorage, Alaska

ORGANIC RESIDUE (KEROGEN) ANALYSIS

M-005
[Rev. 01-80]

November 24, 1981

Time requirements for this job were charged to ESC Request No. 311A78. If you have any questions concerning our results or interpretations, please do not hesitate to contact us.

Very truly yours,

Timothy A. Timmcke

T. A. Timmcke
Exploration Services Center
Applied Stratigraphy

TAT/jg
Attachments

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Alaska Oil & Gas Cons. Commission
Anchorage

TABLE 1
 Ro Means, TAI, and Kerogen Type
 Benedum Nulato Unit No. 1, Norton Sound, Alaska

<u>DEPTH OR SPL. NO.</u>	<u>LOW-GRAY Ro MEAN</u>	<u>% POP.</u>	<u>FIRST HIGH-GRAY Ro MEAN</u>	<u>% POP.</u>	<u>TAI</u>	<u>THERMAL MATURITY</u>	<u>KEROGEN TYPE</u>	<u>HYDROCARBON POTENTIAL/REMARKS</u>
50'	2.62	62	-	-	-	Overmature	Cellulosic	Gas type kerogen
400'	2.70	92	-	-	-	Overmature	Cellulosic	Gas type kerogen
750'	3.28	91	4.07	8	-	Overmature	Cellulosic	Gas type kerogen
1100'	3.21	82	3.97	13	-	Overmature	Cellulosic	Gas type kerogen
1450'	3.18	94	4.34	1	-	Overmature	Cellulosic	Gas type kerogen
1800'	3.27	72	4.12	16	-	Overmature	Cellulosic	Gas type kerogen
2150'	3.44	80	4.21	16	-	Overmature	Cellulosic	Gas type kerogen
2500'	3.38	84	4.52	7	-	Overmature	Cellulosic	Gas type kerogen
2900'	3.45	92	4.82	5	-	Overmature	Cellulosic	Gas type kerogen
3300'	3.62	76	4.59	20	-	Overmature	Cellulosic	Gas type kerogen
3700'	3.77	72	4.59	22	-	Overmature	Cellulosic	Gas type kerogen
4100'	3.61	92	-	-	-	Overmature	Cellulosic	Gas type kerogen
4500'	3.98	78	4.98	8	-	Overmature	Cellulosic	Gas type kerogen
4900'	4.07	93	5.45	3	-	Overmature	Cellulosic	Gas type kerogen
5300'	3.91	74	5.04	6	-	Overmature	Cellulosic	Gas type kerogen
5700'	3.91	92	5.52	5	-	Overmature	Cellulosic	Gas type kerogen
6100'	4.10	83	5.63	12	-	Overmature	Cellulosic	Gas type kerogen

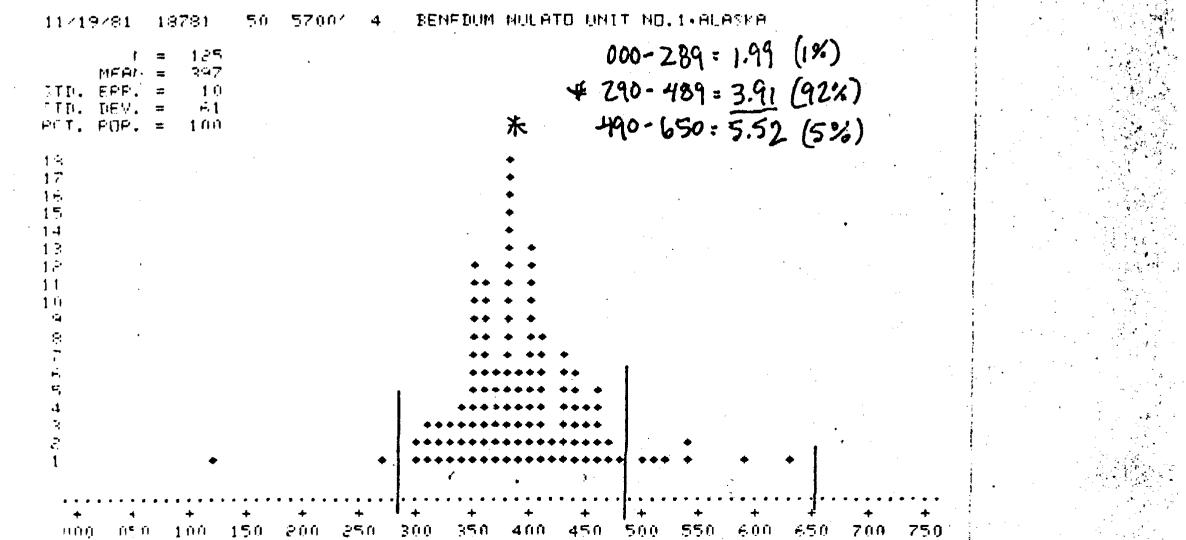
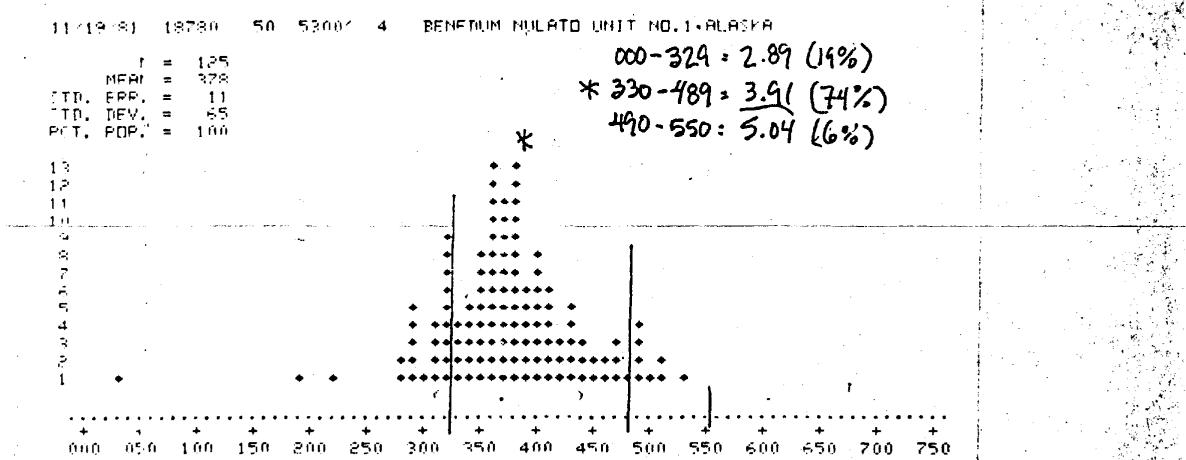
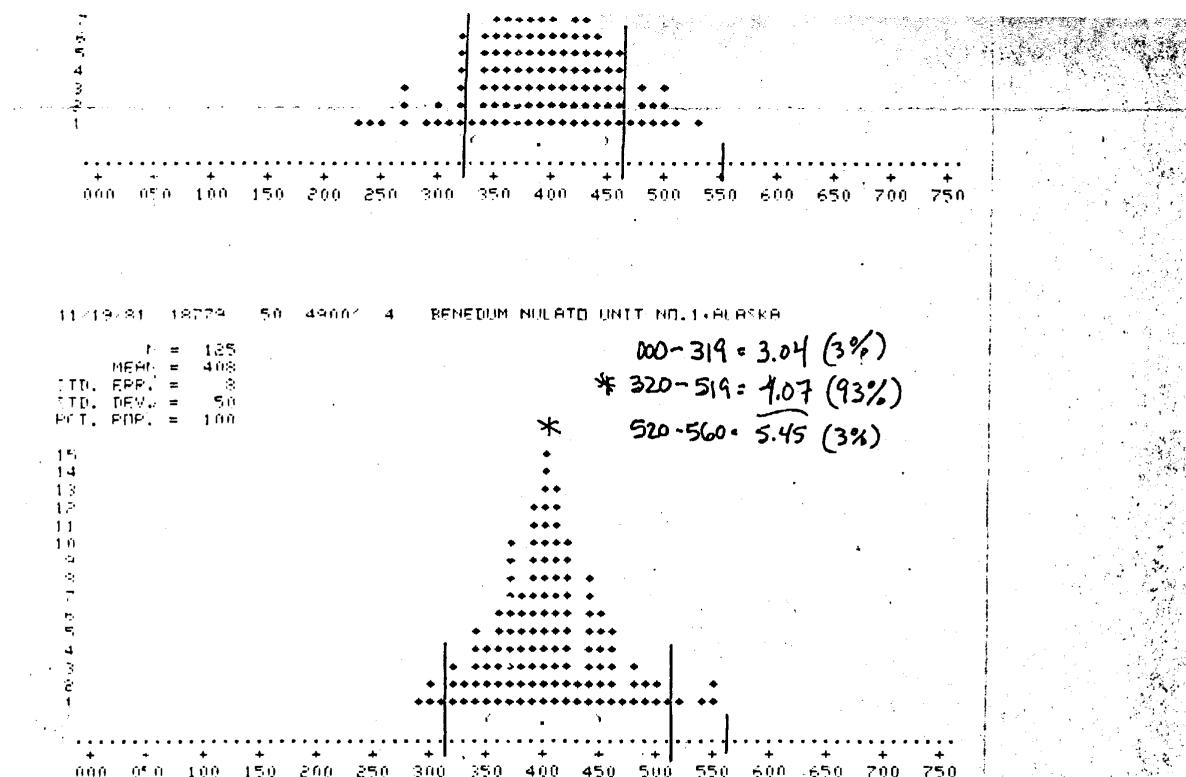
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TABLE 1
Ro Means, TAI, and Kerogen Type
Benedum Nulato Unit No. 1, Norton Sound, Alaska

<u>DEPTH OR SPL. NO.</u>	<u>LOW-GRAY Ro MEAN</u>	<u>% POP.</u>	<u>FIRST HIGH-GRAY Ro MEAN</u>	<u>% POP.</u>	<u>TAI</u>	<u>THERMAL MATURITY</u>	<u>KEROGEN TYPE</u>	<u>HYDROCARBON POTENTIAL/REMARKS</u>
6500'	4.09	88	5.92	1	-	Overmature	Cellulosic	Gas type kerogen
6900'	4.10	71	5.17	13	-	Overmature	Cellulosic	Gas type kerogen
7300'	4.07	65	5.09	9	-	Overmature	Cellulosic	Gas type kerogen
7700'	4.22	70	5.41	14	-	Overmature	Cellulosic	Gas type kerogen
8100'	4.23	79	5.45	12	-	Overmature	Cellulosic	Gas type kerogen
8500'	4.32	76	5.39	21	-	Overmature	Cellulosic	Gas type kerogen
8900'	4.28	86	5.61	7	-	Overmature	Cellulosic	Gas type kerogen
9300'	4.28	85	5.35	12	-	Overmature	Cellulosic	Gas type kerogen
9700'	4.33	77	5.50	17	-	Overmature	Cellulosic	Gas type kerogen
10100'	4.30	80	5.64	5	-	Overmature	Cellulosic	Gas type kerogen
10500'	4.39	80	5.58	5	-	Overmature	Cellulosic	Gas type kerogen
10900'	4.39	63	5.61	17	-	Overmature	Cellulosic	Gas type kerogen
11300'	4.42	.47	5.39	18	-	Overmature	Cellulosic	Gas type kerogen
11700'	4.43	80	5.72	8	-	Overmature	Cellulosic	Gas type kerogen

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Anchorage

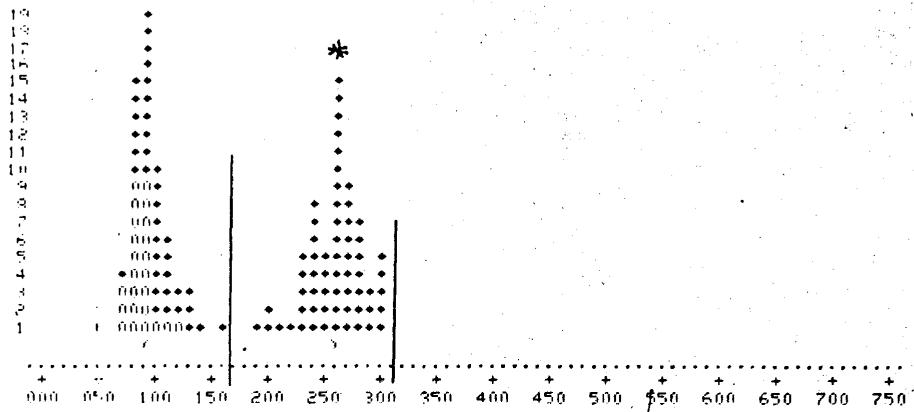
EO

..FIRST SAMPLE NO. = 18766
..LAST SAMPLE NO. = 18796
..OHD COMMNRN = LP

11-19-81 18766 50 500 4 BENEDUM NULATO UNIT NO.1-ALASKA

N = 125
MEAN = 180
STD. ERR. = 14
STD. DEV. = 84
PCT. POP. = 100

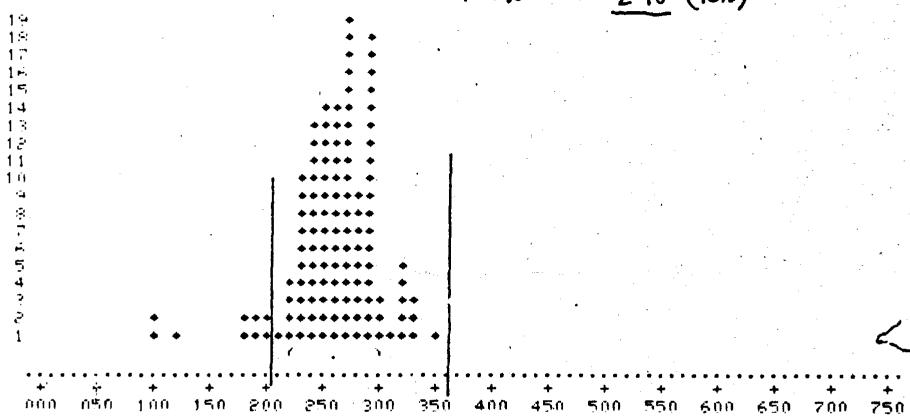
$$000 - 169 = 0.98 \text{ (38\%)} \\ * 170 - 310 = 2.62 \text{ (62\%)}$$



11-19-81 18767 50 1000 4 BENEDUM NULATO UNIT NO.1-ALASKA

N = 124
MEAN = 263
STD. ERR. = 6
STD. DEV. = 89
PCT. POP. = 99

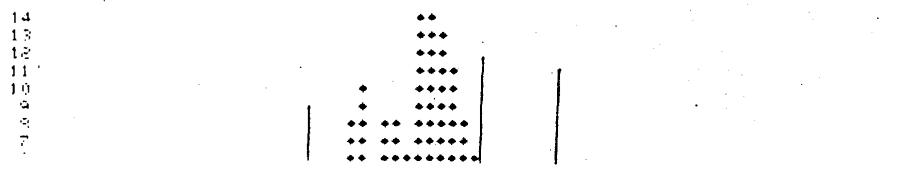
$$000 - 209 = 1.67 \text{ (7\%)} \\ * 210 - 360 = 2.70 \text{ (92\%)}$$

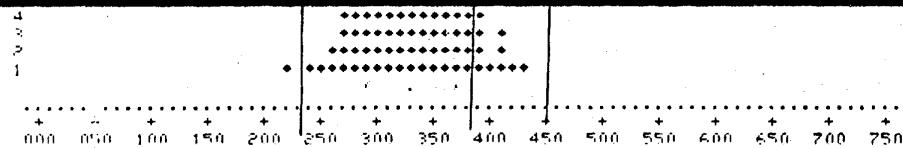


11-19-81 18768 50 750 4 BENEDUM NULATO UNIT NO.1-ALASKA

N = 125
MEAN = 334
STD. ERR. = 7
STD. DEV. = 40
PCT. POP. = 100

$$000 - 234 = 2.20 \text{ (0\%)} \\ * 240 - 389 = 3.28 \text{ (91\%)} \\ 390 - 450 = 4.07 \text{ (8\%)}$$

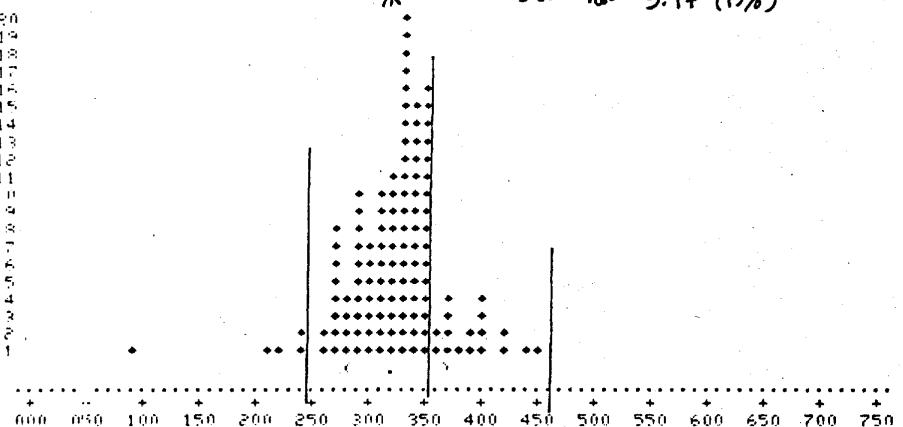




11-19-81 18769 50 11000 4 BENETRUM NULATO UNIT NO. 1+ALASKA

$\bar{x} = 125$
MEAN = 327
STD. ERR. = 7
STD. DEV. = 44
PCT. PDP = 100

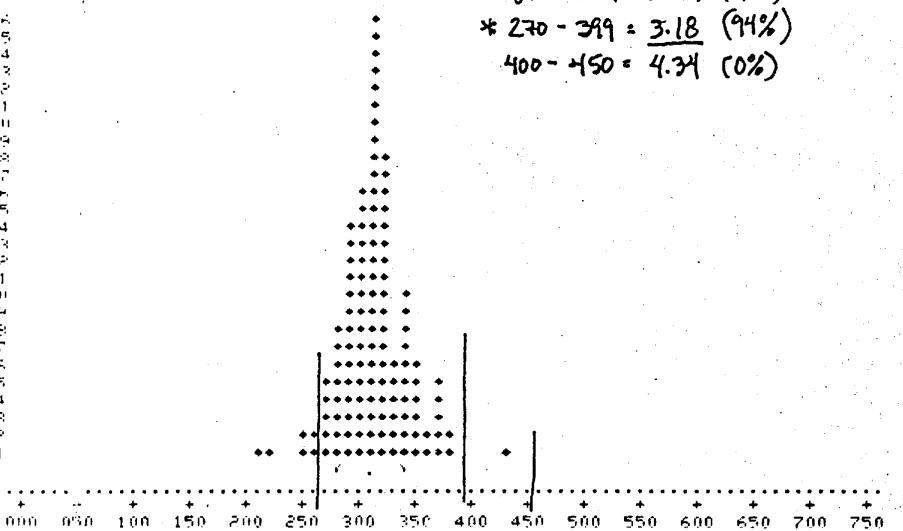
$$\begin{aligned} 000-249 &= 2.06 (4\%) \\ * 250-359 &= 3.21 (82\%) \\ 360-460 &= 3.97 (13\%) \end{aligned}$$



11-19-81 18770 50 14500 4 BENETRUM NULATO UNIT NO. 1+ALASKA

$\bar{x} = 125$
MEAN = 315
STD. ERR. = 9
STD. DEV. = 31
PCT. PDP = 100

$$\begin{aligned} 000-269 &= 2.44 (4\%) \\ * 270-399 &= 3.18 (94\%) \\ 400-450 &= 4.34 (0\%) \end{aligned}$$



11-19-81 18771 50 18000 4 BENETRUM NULATO UNIT NO. 1+ALASKA

$\bar{x} = 125$
MEAN = 328
STD. ERR. = 10
STD. DEV. = 57
PCT. PDP = 100

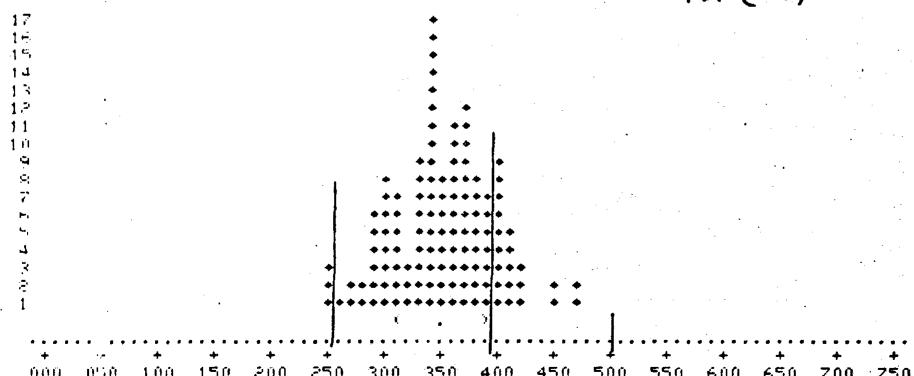
$$\begin{aligned} 000-269 &= 2.26 (12\%) \\ * 270-379 &= 3.27 (72\%) \\ 380-500 &= 4.12 (16\%) \end{aligned}$$



11-19-81 18773 50 21504 4 BENEFUM NULATO UNIT NO.1, ALASKA

N = 125
MEAN = 355
STD. ERR. = 7
STD. DEV. = 44
PCT. POP. = 100

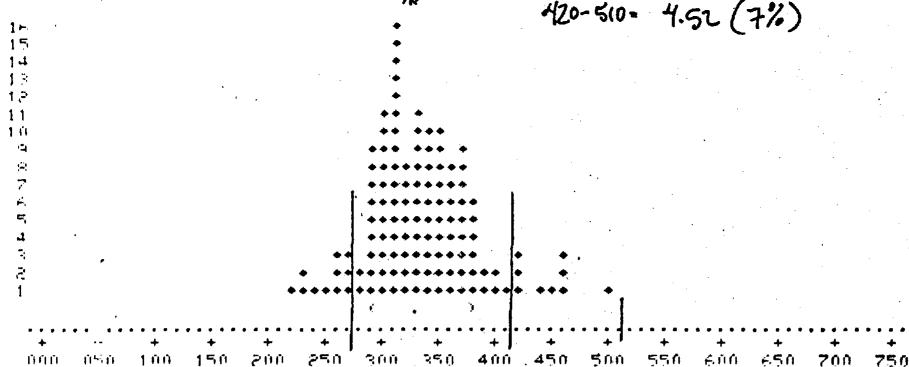
* 000-259 = 2.51 (2%)
* 260-399 = 3.44 (80%)
* 400-500 = 4.21 (16%)



11-19-81 18773 50 25004 4 BENEFUM NULATO UNIT NO.1, ALASKA

N = 125
MEAN = 359
STD. ERR. = 8
STD. DEV. = 42
PCT. POP. = 100

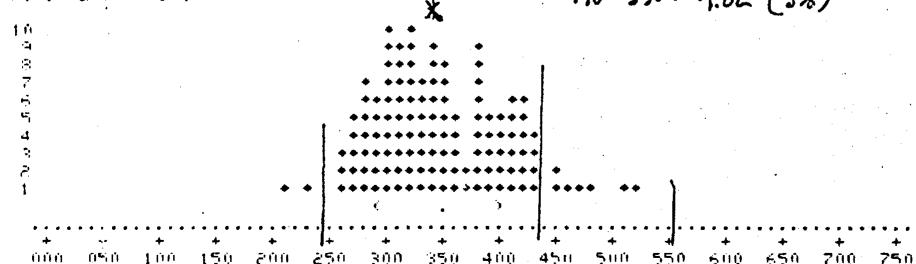
* 000-279 = 2.56 (3%)
* 280-414 = 3.38 (84%)
* 420-510 = 4.52 (7%)



11-19-81 18774 50 29004 4 BENEFUM NULATO UNIT NO.1, ALASKA

N = 125
MEAN = 351
STD. ERR. = 10
STD. DEV. = 58
PCT. POP. = 100

* 000-249 = 2.27 (1%).
* 250-439 = 3.45 (92%).
* 440-550 = 4.82 (5%).



11-19-81 18775 50 33004 4 BENEFUM NULATO UNIT NO.1, ALASKA

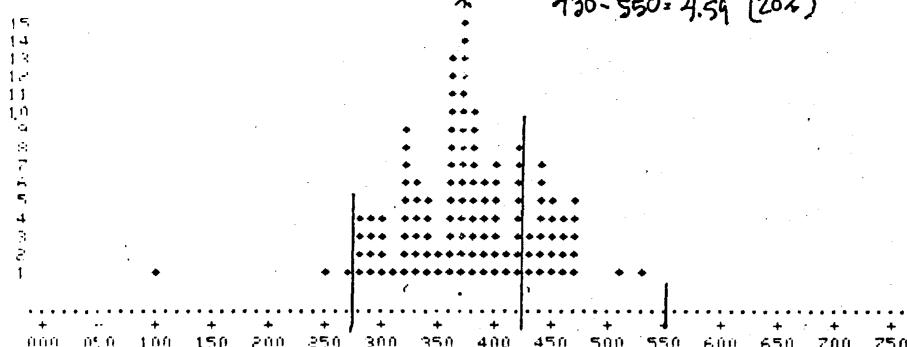
11-19-81 18775 50 33000 4 BENEFIUM NITRATE UNIT NO. 1+ALASKA

\bar{x} = 125
MFR = 329
STD. ERR. = 10
STD. DEV. = 54
PCT. PDP = 100

$$000-279 = 2.11 (2\%)$$

$$* 280-429 = 3.62 (76\%)$$

$$430-550 = \underline{4.59} (20\%)$$



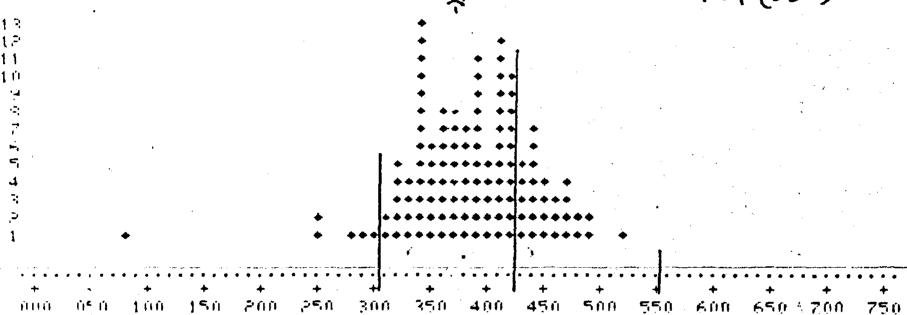
11-19-81 18776 50 37000 4 BENEFIUM NITRATE UNIT NO. 1+ALASKA

\bar{x} = 125
MFR = 329
STD. ERR. = 10
STD. DEV. = 57
PCT. PDP = 100

$$000-309 = 2.48 (4\%)$$

$$* 310-429 = 3.77 (72\%)$$

$$430-550 = \underline{4.59} (22\%)$$

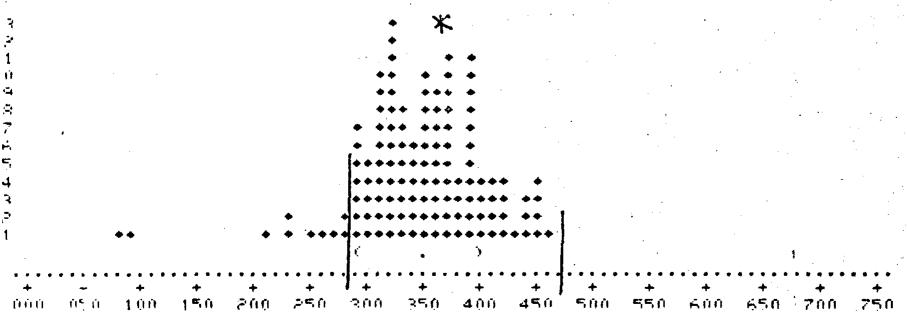


11-19-81 18777 50 41000 4 BENEFIUM NITRATE UNIT NO. 1+ALASKA

\bar{x} = 125
MFR = 350
STD. ERR. = 10
STD. DEV. = 59
PCT. PDP = 100

$$000-289 = 2.23 (8\%)$$

$$* 290-470 = 3.61 (92\%)$$



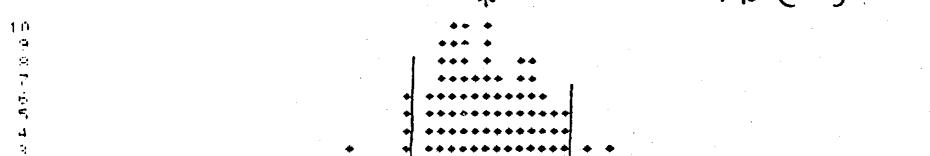
11-19-81 18778 50 45000 4 BENEFIUM NITRATE UNIT NO. 1+ALASKA

\bar{x} = 125
MFR = 394
STD. ERR. = 10
STD. DEV. = 68
PCT. PDP = 100

$$000-329 = 2.95 (12\%)$$

$$* 330-469 = 3.98 (78\%)$$

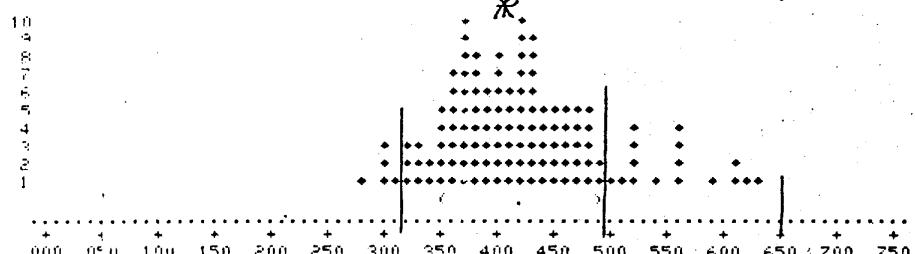
$$470-550 = \underline{4.98} (8\%)$$



11/19/81 18782 50 6100' 4 BENEFUM NULATO UNIT NO.1-ALASKA

$\bar{x} = 125$
MEAN = 425
STD. ERR. = 12
STD. DEV. = 70
PCT. POP. = 100

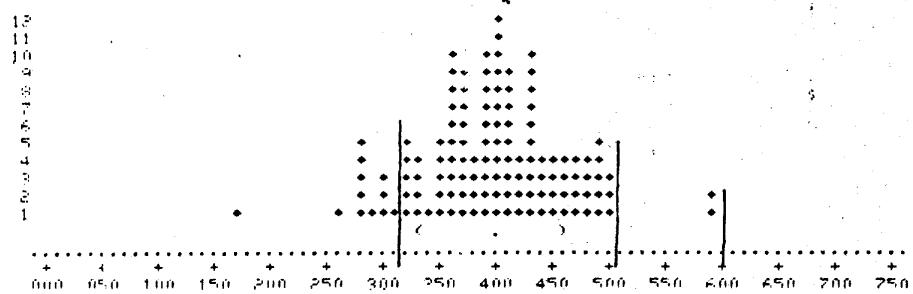
$$\begin{aligned}000-319 &= 3.05 (4\%) \\ *320-499 &= \underline{4.10} (83\%) \\ 500-690 &= 5.63 (12\%)\end{aligned}$$



11/19/81 18783 50 6500' 4 BENEFUM NULATO UNIT NO.1-ALASKA

$\bar{x} = 125$
MEAN = 400
STD. ERR. = 11
STD. DEV. = 64
PCT. POP. = 100

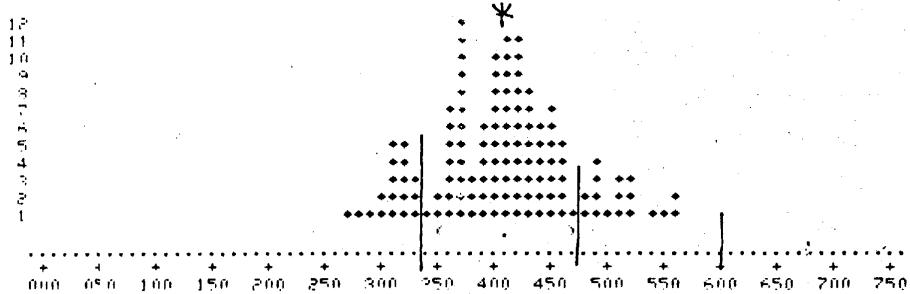
$$\begin{aligned}000-319 &= 2.82 (9\%) \\ *320-509 &= \underline{4.09} (88\%) \\ 510-600 &= 5.92 (1\%)\end{aligned}$$



11/19/81 18784 50 6900' 4 BENEFUM NULATO UNIT NO.1-ALASKA

$\bar{x} = 125$
MEAN = 411
STD. ERR. = 10
STD. DEV. = 60
PCT. POP. = 99

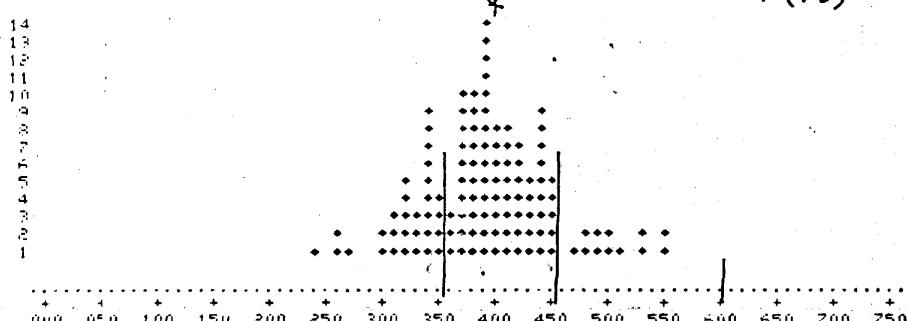
$$\begin{aligned}000-339 &= 3.15 (14\%) \\ *340-479 &= \underline{4.10} (71\%) \\ 480-600 &= 5.17 (13\%)\end{aligned}$$

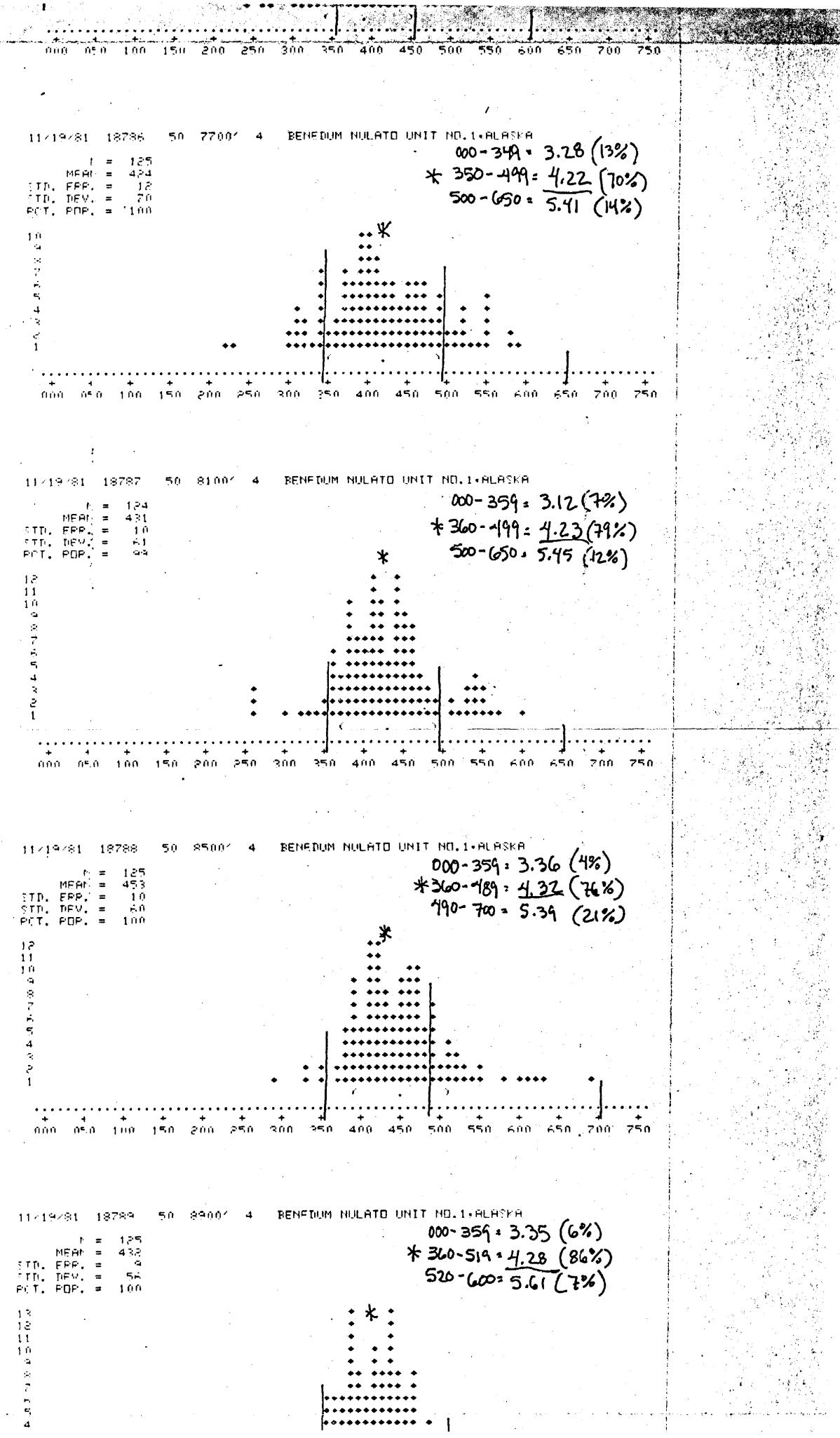


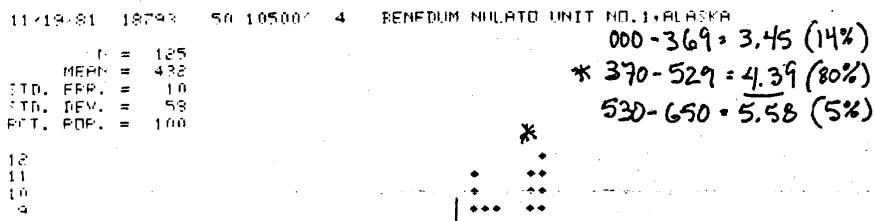
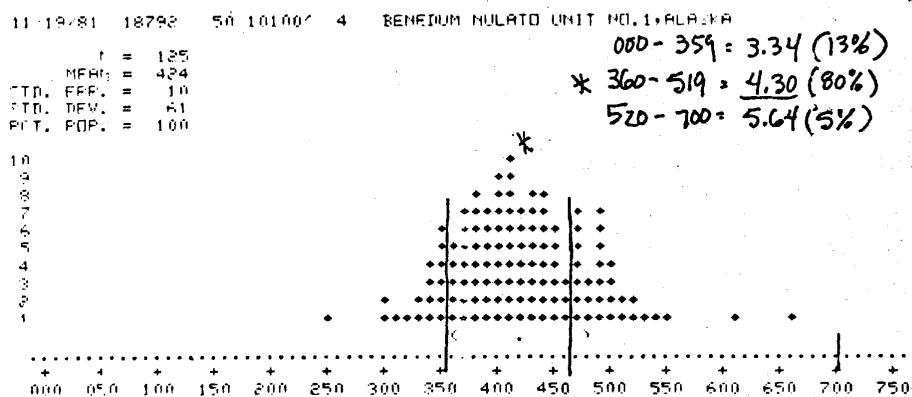
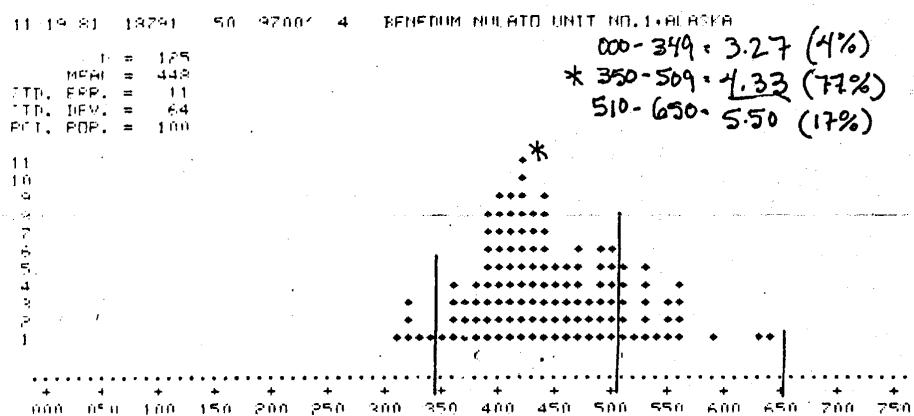
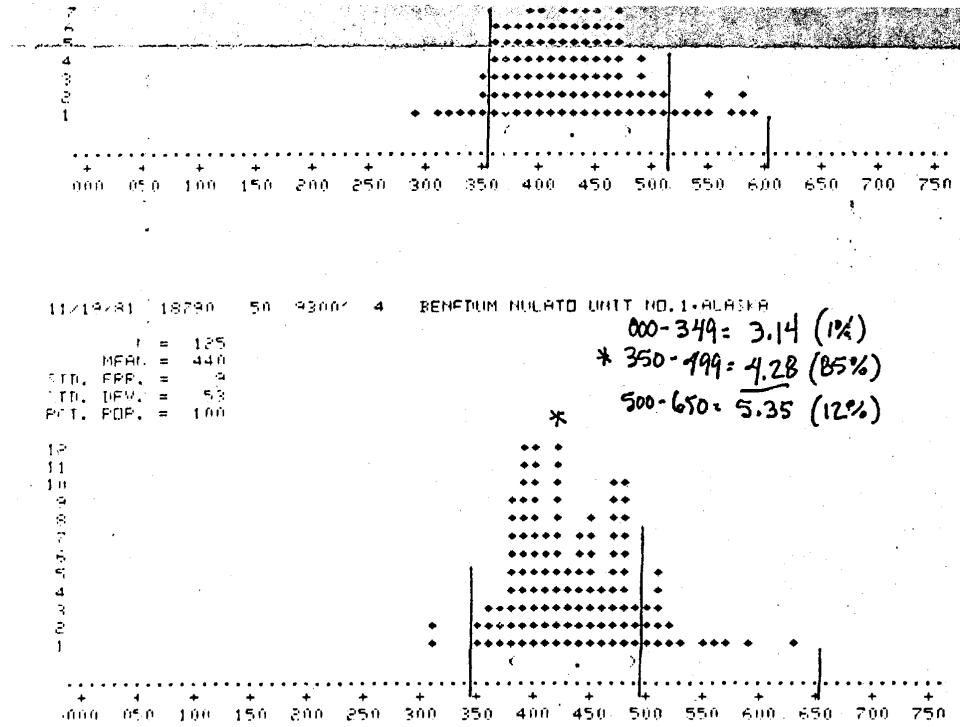
11/19/81 18785 50 7300' 4 BENEFUM NULATO UNIT NO.1-ALASKA

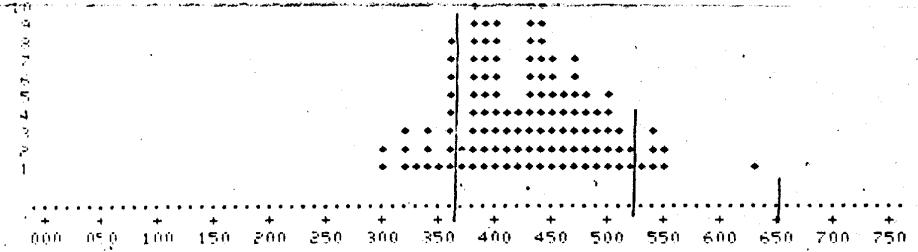
$\bar{x} = 121$
MEAN = 397
STD. ERR. = 10
STD. DEV. = 57
PCT. POP. = 100

$$\begin{aligned}000-359 &= 3.25 (24\%) \\ *360-459 &= \underline{4.07} (65\%) \\ 460-600 &= 5.09 (9\%)\end{aligned}$$







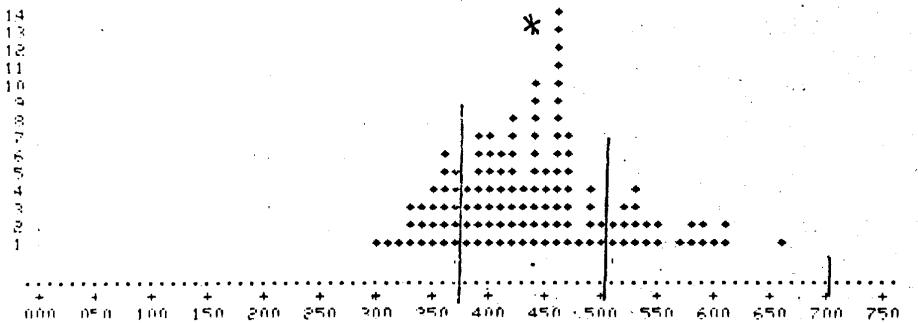


11-19-81 18794 50 109001 4 BENEFUM NULATO UNIT NO. 1-ALASKA
 $n = 125$
 $MFRN = 444$
 $STD. EPP. = 42$
 $STD. DEV. = 71$
 $PCT. POP. = 100$

$$000-379 = 3.51 (19\%)$$

$$*380-509 = 4.39 (63\%)$$

$$510-700 = 5.61 (17\%)$$

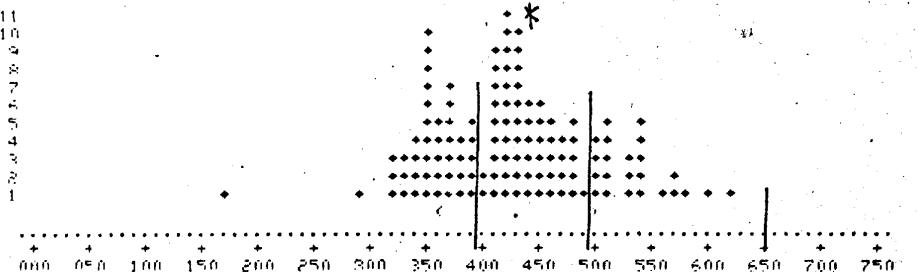


11-19-81 18795 50 113001 4 BENEFUM NULATO UNIT NO. 1-ALASKA
 $n = 125$
 $MFRN = 430$
 $STD. EPP. = 121$
 $STD. DEV. = 70$
 $PCT. POP. = 100$

$$000-399 = 3.56 (34\%)$$

$$*400-499 = 4.42 (47\%)$$

$$500-650 = 5.39 (8\%)$$

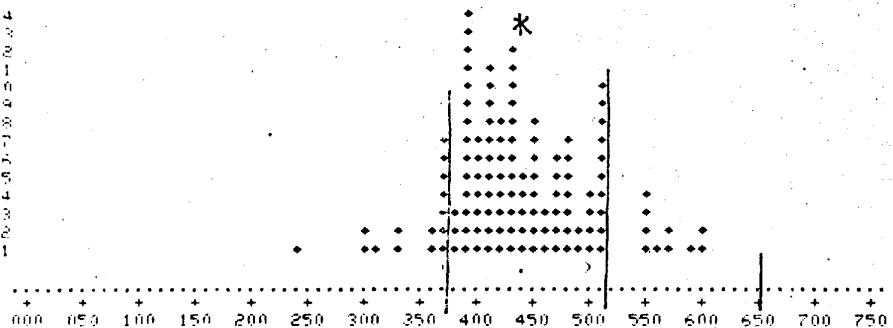


11-19-81 18796 50 117001 4 BENEFUM UNIT NO. 1-ALASKA
 $n = 125$
 $MFRN = 441$
 $STD. EPP. = 11$
 $STD. DEV. = 63$
 $PCT. POP. = 100$

$$000-379 = 3.45 (12\%)$$

$$*380-519 = 4.43 (80\%)$$

$$520-650 = 5.72 (8\%)$$



**COMMAND = ?