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#### PRESENTATION OF DATA FROM THE GAMBELL, ALASKA WELL PROJECT

by

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Division of Mining and Water Management

Alaska Hydrologic Survey

in cooperation with
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Village Safe Water Program,
City of Gambell, and
Jim Munter, Bristol Environmental Services

September 1994

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## PRESENTATION OF DATA FROM THE GAMBELL WATER PROJECT. TWO WELLS NEAR SEVUOKUK MOUNTAIN, ST LAWRENCE ISLAND, NEAR GAMBELL, ALASKA





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#### PRESENTATION OF DATA FROM THE GAMBELL, ALASKA WELL PROJECT

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Roy R. Ireland

#### **ABSTRACT**

Planned improvements to the City of Gambell infrastructure included construction of a piped water system and a sewer system, and also an expansion of the water supply if the water resources were available. The main restriction on the expansion of the water supply was ensuring that the aquifer was not degraded by either saltwater intrusion into the body of the aquifer or by advancement of permafrost on the margins of the aquifer. Instances of increased salinity had been noted in the past, but careful placement of new production wells might allow future expansion without any degradation. This report comprises the data gathering stage of the project, with interpretation.

#### INTRODUCTION

This project was initiated by Chuck Eggener Consulting Engineers and the Department of Environmental Conservation (DEC), Village Safe Water Program who contracted with the Alaska Hydrologic Survey (AHS) of the Alaska Department of Natural Resources, Division of Mining and Water Management, to determine the limits of a small aquifer on St Lawrence Island near the village of Gambell (fig. 1) in order to expand the water supply to the city.

The aquifer was already being utilized but it was uncertain as to whether further development could take place without damaging the aquifer, because increased salinity levels had been observed during prior usage. The location of any future wells could be a significant factor in utilizing the resource without further degradation. Earlier surficial mapping and test drilling had defined the contours and limits of the aquifer along the front of a steep bluff and leading directly across a gravel bar to the ocean (fig. 2). Both the lateral and lower limits of the aquifer were defined by the test drilling and were found to be controlled by permafrost within the otherwise permeable beach gravels of the bar on which the city is located. Flow within the aquifer was determined to be predominantly to the north, into the ocean.

Two new monitoring wells were installed to allow recording of aquifer response to continued high volume pumping at the existing production well. The location of these wells was chosen so as to reveal as much information as possible, based on information gained from the mapping of the aquifer (fig. 2).

This report deals primarily with the results of observations at the test wells and includes a review of the observations taken from the pumping well at the pumphouse. No extensive hydrologic interpretation of the data is made; however, interpretations of the graphs and tables are made to facilitate understanding of the data. Some cautions are also expressed due to the severity of the environment and the anomalies indicated by the data.

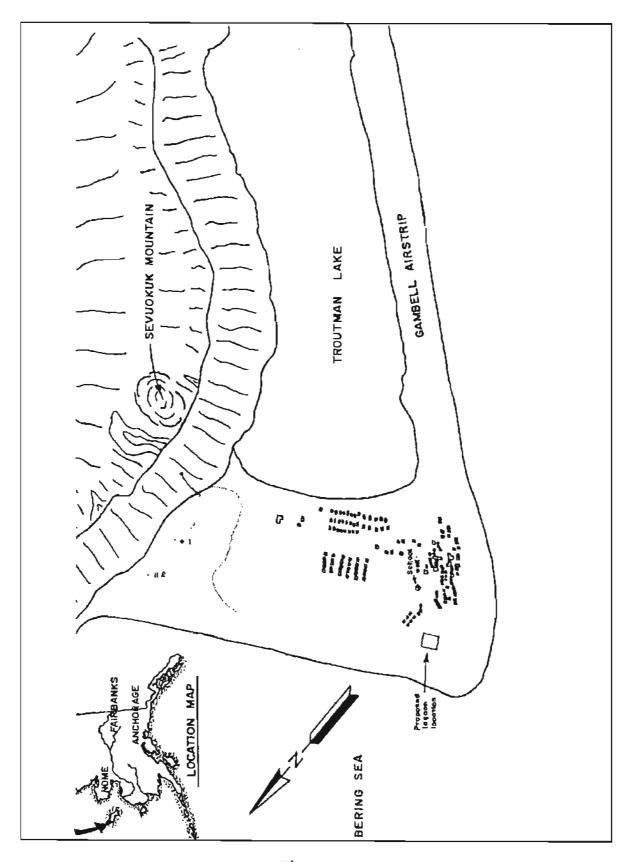


Figure 1

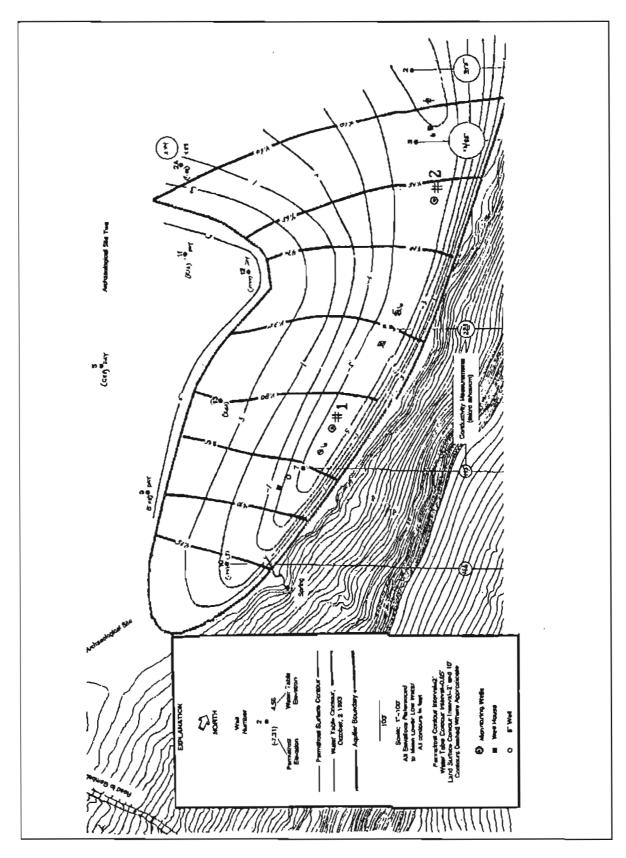


Figure 2

#### GEOLOGIC SETTING

The City of Gambell (fig. 1) is located near the tip of a gravel spit on the northwest of St. Lawrence Island in the northern Bering Sea. To the south of the community, Troutman Lake is separated from the Bering Sea by a narrow gravel bar to the west and a much broader gravel bar (up to 4000 ft) to the north, on which the community is located. The lake, with a level of about 2 ft above mean low low water (MLLW), is isolated from the aquifer in this northern portion of the spit by permafrost (discontinuous in the area at depths from 7- 10 ft, RZA, Inc, 1985) in the northern banks of the lake and the gravel bar beyond, over a distance of about 900 ft. Some drainage into the aquifer (Figure 2), under study in this report, may take place (Waller, 1959). Sevuokuk Mountain, rising to an elevation of 614 ft above MLLW forms the eastern boundary of both the aquifer and the lake.

Two larger springs, that flowed from the steep bluffs of Sevuokuk Mountain and disappear into the gravel about 1100 ft and 1600 ft respectively from the northern edge of the lake, formed a major source of water to the aquifer. The aquifer also received water from runoff from the mountain and bluffs via a series of minor springs and seeps, and from surface infiltration from an annual precipitation of about 16 inches (Phil Johnson Engineering, 1972). No subsurface entry of fresh water, other than possible flow from Troutman Lake, has been found. If any flow from the lake occurred, it was minimal since the aquifer was fresh while the lake was often brackish. Water in the aquifer flowed to the north and drained into the Bering Sea, about 3200 ft from the spring. Aufeis that formed on the springs during the extended "winter" (late December through early June in terms of aquifer response) indicated some continued flow into the aquifer, at least during the early months.

Gravel beds on the bar were found to be highly permeable. They are comprised of varying amounts of sands and assorted beach gravels with minor amounts of silts and clays. Ice-bound permafrost pervaded the area of the aquifer lessening towards the Bering Sea (Munter, 1994). Storm surges and blown spray contribute saline materials to the aquifer, as would any inflow from Troutman Lake which is generally brackish due to the same storm surges. Any reduction in head in the aquifer would allow saline water to enter into the aquifer from the sea to the north.

#### INSTRUMENTATION

Chuck Eggener Consulting Engineers installed two monitoring wells (fig. 2, Gambell #1 and Gambell #2) at sites deemed to be critical to the study. Gambell #2 (fig 5) was 800 ft from the pumphouse and Gambell #1 (fig 6) was 200 ft from the pumphouse. The pumphouse is about 700 ft from the upper spring and about 300 ft from the lower spring. It is about 900 ft from the southern edge of the aquifer, which is inferred to extend somewhat to the south of the upper spring, the exact distance being undetermined because of archeological digs in the area. Instrument shelters were provided by Chuck Eggener Consulting Engineers (fig. 3). They consisted of modified 55 gal drums set over the above ground portions of the test wells. Some radiant heating and cooling affects were anticipated because of the drums. Instrumentation was subsequently installed in the wells by AHS personnel (fig. 4).

Instrumentation NorthWest 5 psi pressure transducers were selected to measure the level of the water within the well column. Pressure transducers sense the depth of water above the transducer and can be used to determine the depth to water in a well. The 5 psi model has a range of 10 ft, which is greater than any fluctuations expected in any of the wells at the site. The stainless steel transducer assembly was suspended by its data cable within a few inches from the bottom of the well. The depth to water from the top of casing (TOC) and the depth of water over the transducer (DOS) were recorded and the cable was marked and measured as a check on the location of the transducer.

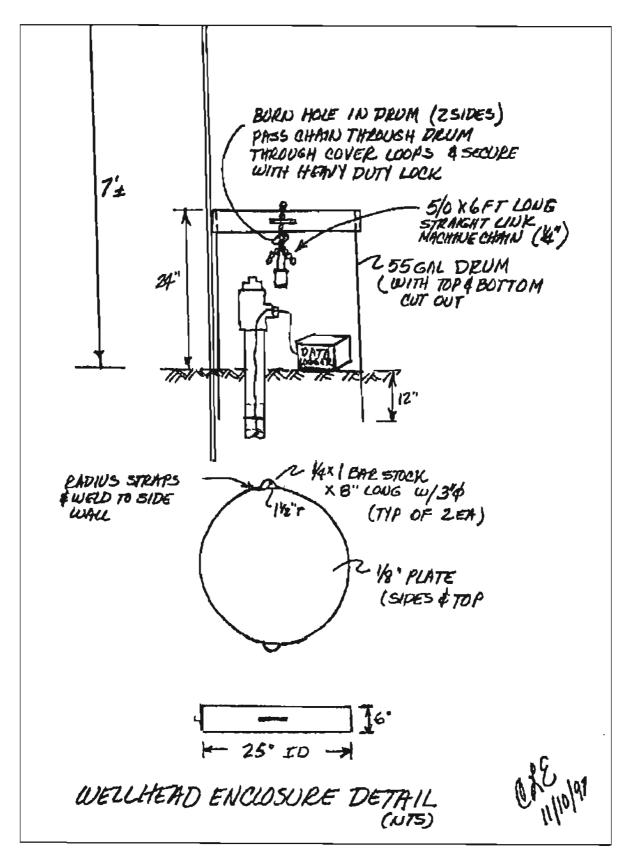


Figure 3

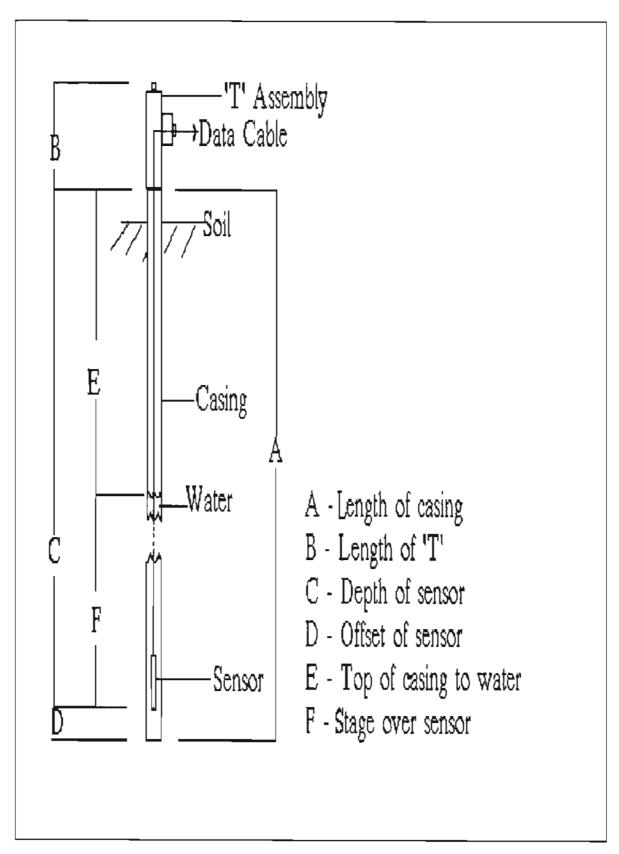


Figure 4

### STATE OF ALASKA DEPARTMENT OF NATURAL RESOURCES DIVESTON OF WATER WATER WELL RECORD

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Figure 5

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Figure 6

Great Lakes Instruments 3625e2t electrodeless probes were selected to monitor the conductivity of the water contained within each well. Monitoring the relation of conductivity to temperature would allow for recallibration, if required. The conductivity probe was set to read specific conductance, loosely referred to as "conductivity" both here and in the instrumentation literature, when exposed to temperatures of 15 °C. A correction factor of 1.13 was included to correct to  $(0 \pm .3)$  °C. Because the probe was an electrodeless device, temperature dependant metal/solution interface problems were avoided. A correction factor obtained from regression analysis with laboratory samples was also applied to the conductivity data to correct for initial probe conditions, standard procedure for conductivity studies. Post calibration verified results and correlated with precalibration tests.

Dryden Instrumentation temperature probes were selected to monitor both air and water temperature. In each case, a temperature probe and a conductivity probe were attached as close to the pressure transducer as possible. This allowed monitoring of water conditions at the bottom of the well and, by inference, water that flowed through the aquifer. Air temperature was monitored to provide environmental data for the location of each of the test wells. This monitoring was to show if the wells were similarly influenced by weather conditions in the local environment. The temperature probes are stable and regulated, and so required no recalibration.

Omnidata 900 data loggers were chosen to monitor and record water conditions in the wells. These instruments allowed timed scanning of the probes and transducers, timed switching of external power supplies to the transducers, and extended data recording capabilities. Multiple inputs and power supply regulation were both handled by the logger.

#### DATA COLLECTION

The data loggers were set to scan the probes and transducers, and to record the data observed, at three hour intervals. The data storage modules had excess capacity, but were serviced as frequently as possible to allow early detection of potential data recording problems. During each of the field trips to Gambell by DEC personnel, the data storage modules on the recorders were retrieved and replaced with a fresh modules. The retrieved modules were returned to the AHS to be digitally read and prepared for reuse. This process required some computer manipulation of the raw data to get it into suitable formats; however, the values in the data were not modified. The regression correction for conductivity was only applied after post calibration had taken place.

Four days from the end of the data recording stage of the project, the sensor in the monitoring well Gambell #2 froze and started giving invalid data (later edited out from the dataset). The aberrant data was an indication of damage to the pressure transducer. This sensor was not removed in the final field trip because it was frozen to the bottom of the well. Electronic failure prevented data from being recovered during the final two months from the other observation well, Gambell #1. This was the only data loss for either recorder during the period of observation.

The probes and transducer from Gambell #1 were recovered and underwent recalibration. Both the pressure transducer and the two temperature probes returned correct readings during the calibration procedure while the conductivity probe showed a small offset, with the magnitude of change being insignificant relative to the numbers being observed in the field. This drift was corrected by linear interpolation, but had no overall significance (app. A, Table 1) in terms of shape or placement of the curve. The conductivity data showed that conductivity varied independently of the temperature at the probe, an indication that the temperature compensation within the conductivity probe functioned correctly.

The cables were measured and did not show any evidence of stretching during the monitoring period. This was as expected due to the low mass of the combined probes and transducer, and the inherent strength of the combined cables. No correction in stage data was required. The well

casings and static water levels in the wells had been carefully measured at installation and again at the cessation of data gathering. An error of less than .01 ft between the two measurements was determined (app. A, Table 2), which was insignificant relative to the range in stage observed (-0.8 ft through 5.2 ft). All stage data was then back-calculated to absolute stage (water surface elevation) relative to MLLW.

Since the probes and transducer were not recovered from the Gambell #2 well, the same manipulation of the data as with Gambell #1 well data took place. This was justified by the equipment having been identical in both instances, and the respective environments also having been very similar. Perusal of the graphs and data also indicated that using the same conversions was a valid technique.

Pumping data from the pumphouse was provided for the first three months of the monitoring period and for the 14 months before, by the City of Gambell (app. B, a listing of manually entered data from the production wells as supplied to the Division of Water, by Chuck Eggener Consulting Engineers). The irregular nature of this data required some interpolation for the numerous missing observations - often data was read on alternate days and sometimes only partial data was recorded. These are indicated in app. B. Steady trends that continued over time facilitated this interpolation.

Both pumphouse data and observation well data (app. C & D, accumulated data from each monitoring well in two column format) were converted to standard units of measurement and were concatenated into larger databases as the data was retrieved. Conductivity data also were corrected using linear regression. The three datasets were subsequently were combined and the daily averages for all data were calculated. This provided a smaller, comprehensive dataset for more rapid perusal and use of the data (app. E). Comparison of results with the original databases showed only very minor changes between the average data and the recorded data. This indicated that the smaller dataset (app. E) was valid, and could be used to generate interpretative graphs (app. F). In the graphs, data from the production well were smoothed using a 24 observation moving average, due to the erratic nature of the observations. This allowed trends to be discerned from the data by eliminating any short term variability which might have depended as much on the observer as on the parameter being observed.

#### SUMMARY

Aquifer water temperature dropped to below 0.0 °C, with freezing at the perimeter. There was evidence, in the freezing of the pressure transducer, that the permafrost underlaying the aquifer had risen towards the surface, and had possibly reduced the size of the aquifer as overall temperature dropped. This freezing occurred in early August, and could not have been affected by heat loss to the well which was exposed to warm surface temperatures. Water elevation and temperature were somewhat inversely related, but the response time for temperature was retarded by the thermal inertia of the aquifer. Pumping during periods of low water elevation would reduce the thermal reservoir within the aquifer. Gambell #1 had a higher year round water temperature than Gambell #2 because it was further from the source of recharge water with higher temperatures and had a longer period of time to dissipate heat to the environment.

Water surface elevation rose and dropped rapidly above the 1 ft above MLLW, but more slowly below this level, and eventually reached levels near 1 ft below MLLW (-0.85 ft). Water surface elevation in the aquifer, even at the most remote site, dropped below MLLW, and created a gradient conducive to infiltration of saltwater. Storm surges and other high tide events could enlarge any intrusion because of higher saltwater elevations. Evidence of high tidal events (app F, Graph 9) were observed at Gambell #2, in the paired minor peaks on the conductivity graph occurring during the periods March 3 -17, 1994 and May 27 - June 7, 1994. These peaks were more distinct at Gambell #2 than at Gambell #1, and were not observed at the production well. Water elevation was only dependant on rates of pumping during the seasonal lows, which occurred during the

period from late December through early June. The large periodic differences in water surface elevations, which repeat annually, allowed two seasons to be determined: a recharge season when the water surface elevation was high; and a non-recharge "winter" season when the water surface elevation was low. The aquifer responded rapidly to the influx of fresh water during the recharge season (app F, Graph 14), and showed rapid rises early in the recharge season and subsequent falls in water elevation as the season ended, without much relation to rates of pumping. During the period of non-recharge, the aquifer showed an ability to maintain itself, only slowly falling to below MLLW, especially when stressed by high rates of pumping. This stability may have been due to the steady back pressure of the saltwater from the ocean. There was an indication of a steady state water elevation of about 3 inches (+0.25 ft) above MLLW during seasonal lows. The production well was most affected by pumping and Gambell #2 the least.

Aquifer conductivity rose and dropped sharply, and showed an anomalous recovery. Conductivity appeared to be cyclic, with lows occurring at the times of high water surface elevation within the aquifer, and to have similar magnitude at corresponding times between cycles (app f. Graph 1). Water elevation and conductivity were inversely related, but were not proportional to each other, due to storage within the aquifer. Conductivity appeared to be unrelated to temperature at the levels of conductivity observed. Gambell #2 was most affected by increasing conductivity and the production well the least. Two anomalies occurred; firstly, Gambell #1 had a higher conductivity than Gambell #2 for the period May 7 - 23, 1994, and second, when conductivity briefly rose as water surface elevation rose at Gambell #2 during the period May 9 - 29, 1994, a reversal of the regular inverse relationship was seen both here and at the other wells.

#### CONCLUSIONS

High rates of extraction of water from the production well affected the conductivity of the water at the sites of the monitoring wells (and hence the aquifer in general), especially during periods of low water elevation in the aguifer. Continued high rates of extraction could degrade the aguifer by allowing incursion of strongly saline water into the body of the aquifer and also by expansion of the permafrost boundaries thereby reducing the size of the aquifer. The thermal stability of the aquifer was uncertain due to the short monitoring period, but the volume of water removed during periods of low water elevation could reduce the available reservoir of thermal energy. The volume of fresh recharge water may not have been sufficient to rapidly or completely flush the aquifer of saltwater once a certain level of salinity has been achieved, nor may it have had sufficient heat content to replace the heat lost to pumping and to the latent heat of freezing if ice had to be melted to restore the size of the aquifer. While this level had apparently not been reached, the anomalous drop in conductivity at Gambell #2 indicated that this level may not have been far removed. The freezing of the transducer and probes to the bottom of the well in early August implied a negative impact on the aquifer, and indicated a delayed restoration of the thermal environment. It would be prudent to limit pumping to less than 16 gpm (23,000 gallons per day) during period of low water elevation from late December to late May. It appeared that rates of 21 gpm (30,000 gallons per day) might be sustainable during periods of high surface water elevation, but insufficient data exists to confirm this.

#### **ACKNOWLEDGEMENTS**

Chuck Eggener Consulting Engineers - Chuck Eggener and others. DEC, Village Safe Water Program - Steve Eng. Bristol Environmental - James Munter. Alaska Hydrologic Survey.

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#### Appendix A - Reconciliation Tables

#### Conductivity standardization

Standards	Precal.			Standardized	
	readings	readings	data	data	
			(mean)	(formula	#1)
1415.0	1229.8	1240.0	1234.9	1407.2	
750.0	665.7	680.2	673.0	767.5	
362.0	322.9	302.0	312.5	357.1	
147.0	131.7	115.5	i 123.€	142.2	

Formula : (std data) = 
$$1.138301342$$
 (normal data) +  $1.48387108$  (y =  $1.138301342$  x +  $1.48387108$ )

Interpretation: A precalibration value of 1229.8 and a post calibration value of 1240.0 average out to a value of 1234.9 (normalized). When standardized using the formula, it becomes 1407.2

Procedure: To Normalize data between pre and post calibrations, simply average the pre and post calibration readings to get a new reading that correlates to the standard. Then, to standardize data to "in lab" standards (from normalized field data), apply the above formula.

#### Regression Output:

Constant	1.48387108
Std Err of Y Est	14.3956356
R Squared	0.99955424
No. of Observations	4
Degrees of Freedom	2
<pre>X Coefficient(s)</pre>	1.138301342
Std Err of Coef.	0.016997617

#### Appendix A - Reconciliation Tables

#### Gambell Wells

Depth of sensor reconciliation: observed data versus field measurements

		Gambell #1	Gambell #2
Top of casing (TOC) to water	01/06/94	10.7 ft	6.5 ft
Stage (DP900)	01/06/94	3.6 ft	6.8 ft
TOC to Sensor (sum of above)		14.3 ft	13.3 ft
Length of 'T' assembly		1.42 ft	1.42 ft
Top of 'T' to sensor		15.72 ft	14.72 ft

Verification measurements	08/11/94		
Length of cable, top of casing to sensor		14.21 ft	(frozen)ft
Length of cable, top of 'T' to sensor		15.63 ft	(frozen)ft
Maximum error, less than		0.09 ft	(frozen)ft

#### Calculation of Absolute Stage (Water Surface Elevation), Relative to MLLW

Total well depth, casing	14.5 ft	13.6 ft
Length of 'T'	1.42 ft	1.42 ft
Total well depth, Top of 'T'	15.92 ft	15.02 ft

Total well depth	15.92 ft	15.02 ft
Depth to sensor	-15.72 ft	-14.72 ft
Offset of sensor from bottom	0.2 ft	0,3 ft

Elevation of top of 'T'	13.16 ft	8.83 ft
Total depth from top of 'T'	-15.92 ft	-15.02 ft
Offset of sensor from bottom	0.2 ft	0.3 ft
Elevation of sensor	-2.56 ft	-5.89 ft
Elevation of water relative to MLLW (formula)	(stage - 2.56) ft	(stage - 5.89) ft

Appendix B

Gambell Pumphouse Well Data

Date	Well	Static Feet	Static (		Temp °F	Static Level	Water Elevation	Meter n Reading	GPM	Gals/Day
Notes Cla	vation of	uall ba	uon in 1	4.	nalneći	4.a. MI	ш			
20-Oct-97		10	0.75	150	36.00	10.06	4.35	160531	14-41	20752.00
21-Oct-92		9	10.5	160	38.00	9.88	4.54	181283	14.46	20823.00
22-0ct-92		9	7.25	170	38.00	9.60	4.81	202106	14,47	20833.00
23-Oct-92	1	9	6	170	38.00	9.50	4.91	222939	14.39	20721.00
24-0ct-92	1	9	6.75	170	38.00	9.56	4.85	243660	14.90	21458.00
25-Oct-92		9	5.25	170	38.00	9.44	4.97	265118	14.40	20738.38
02-Nov-92		10	0.75	170	38.00	10.06	4.35	431025	14.53	20920,00
03-Nov-92		10	2.0625	190	39.00	10.17	4.24	451945	14.58	20989.00
04-Nov-92 05-Nov-92		10 10	3 4.0625	190 190	39.00 37.00	10.25 10.34	4.16 4.07	472934 493344	14.17	20410.00 20390.00
06-Nov-92		10	4.1875	200	39.00	10.34	4.06	513734	14.21	20466.00
07-Nov-92		10	3.865	210	38.00	10,32	4.09	534200	13.34	19203.00
08-Nov-92		10	4	210	38.00	10.33	4.08	553403	14.21	20463.13
16-Nov-92	1	10	8.75	200	38,00	10.73	3.68	717108	14.30	20597.00
17-Nov-92		10	10	200	38.00	10.83	3.58	737705	14.25	20522.00
18-Nov-92		10	10.75	180	38.00	10.90	3.51	758227	14.07	20254.00
19-Nov-92		10	11.5	180	38.00	10.96	3.45	778481	14.08	20271.00
20-Nov-92 21-Nov-92		10	11.75	200	38.00	10.98	3.43	798752	12.70	18288.00
22-Nov-92		10 10	11.25 10	190 200	38.00 38.00	10.94 10.83	3.47 3.58	817040 839149	15.35 15.36	22109.00 22122.00
23-Nov-92		10	2.5	200	38.00	10.21	4.20	861271	14.28	20560.00
24-Nov-92		9	4	220	36.00	9.33	5.08	881831	14.60	21018.00
25-800-92	2 1	9	2	200	36.00	9.17	5.24	902849	14.41	20749.00
27-Nov-92	2 1	9	7	240	35.00	9.58	4.83	944347	13.80	19878.00
30-Nov-92		10	2		37.00	10.17	4.24	1003981		20357.00
01-Dec-92		10	4.5		36.00	10.38	4.04	1024338		19999.00
02-Dec-92		10	6.75		37.00	10.56	3.85	1044337		20270.00
03-Dec-92 04-Dec-92		10 10	8.75 10.75		37.00	10.73	3.68 3.51	1064607		20265.00
05-Dec-92		11	0.75		40.00 39.00	10.90 11.06	3.35	1084872 1104911		20039.00 19913.00
06-Dec-92		11	3		37.00	11.25	3.16	1124824		19581.00
07-Dec-92		11	4.75	210	39.00	11.40	3.01	1144405		19503.00
08-Dec-92	2 1	11	5.75	200	38.00	11.48	2.93	1163908		19611.00
09-Dec-92		11	7.5	500	38.00	11.63	2.79	1183519	13.69	19710.00
10-Dec-92		11	9	210	38.00	11.75	2.66	1203229		19739.00
11-Dec-92 13-Dec-92		11	10.75	200	37.00	11.90	2.51	1222968		18186.50
14-Dec-92		12 12	1.25 2	210 160	37.00 36.00	12.10 12.17	2.31 2.24	1259341 1268815		9474.00 4402.00
15-Dec-92		12	2.5	160	38.00	32.21	2.20	1273217		NA
16-Dec-92	_	12	3.5	170	38.00	12.29		estimated		0.00
17-Dec-92	2 3	12	5	200	37.00	12.42		estimeted		0.00
18-Dec-92	_	12	5.75	200	38.00	12.48	1.93	estimated	13.20	0.00
19-Dec-92		12	7.5	200	38.00	12.63		estimated		0.00
20-Dec-92		12	8	200	38.00	12.67		estimated		0.00
21-Dec-92 22-Dec-92		12 12	8 8.5	190 200	37.00 37.00	12.67 12.71	1.74	estimated	13.20	0.00
27-Dec-92		13	0.0	200	38.00	13.00		estimated estimated		0,00 0,00
28-Dec-92		13	Õ	210	38.00	13.00		estimated		0.00
01-Jan-93		13	4	200	36.00	13.33		estimated		0.00
07-Jan-93		13	1	210	37.00	13.08		estimated		0.00
08-Jan-93		13	1.5	220	38.00	13.13		estimated		0.00
09-Jan-93		13	1.5	220	37.00	13.13		estimated		0.00
10-Jan-93		13	1	220	37.00	13.08		estimated		0.00
11-Jan-93 12-Jan-93		13 13	1	230 220	37.00 37.00	13.08 13.08		estimated estimated		0.00 0.00
16-Jan-93		13	2	230	35.00	13.17		estimated estimated		0.00
17-Jan-93		13	3	230	35.00	13.25		estimated		0.00
18-Jan-93		13	3	230	35.00	13.25		estimated	_	0.00
19-Jan-93		13	3	230	34.00	13.25		estimated		0.00
20-Jan-93		13	3	550	37.00	13.25		estimated	_	0.00
25 - Jan - 93		13	8	304	36.00	13.67		estimated		0.00
26-Jan-93		13 13	8 7	308	35.00	13.67		estimated		0.00
27-Jan-93	3 3,4	כו	1	200	34.00	13.58	0.83	estimated	13.20	0.00

This is the manually gathered data submitted by the City of Gambell, the raw data used to compile app. E.

Appendix B

Gambell Pumphouse Well Data

28-Jan-93 3,4 13 8 216 37.00 13.67 0.74 estimated 13.20 0.00 0.00 1-rela-93 3,4 13 11 199 88.00 13.67 0.74 estimated 13.20 0.00 0.00 1-rela-93 3,4 13 11 199 88.00 13.92 0.49 estimated 13.20 0.00 0.00 0-rela-93 3,4 13 10.5 277 38.00 13.92 0.49 estimated 13.20 0.00 0.00 0-rela-93 3,4 13 10.5 277 38.00 13.92 0.49 estimated 13.20 0.00 0.00 0-rela-93 3,4 13 10.5 277 38.00 13.92 0.49 estimated 13.20 10.00 0.7-rela-93 3,4 13 10.5 277 38.00 13.92 0.49 estimated 13.20 10.00 0.7-rela-93 3,4 13 10.5 277 38.00 13.92 0.49 12.528 13.80 82 14.228.00 0.7-rela-93 3,4 13 10 198 36.00 13.00 1.41 134.528.28 13.80 1993.30 0.9-rela-93 3,4 14 1 20 20 4 37.00 13.00 1.41 134.528.28 13.80 1993.30 0.9-rela-93 3,4 14 1 20 20 4 37.00 13.00 1.41 134.528.28 13.80 1993.30 0.9-rela-93 3,4 14 1 20 36 37.00 14.08 0.33 14205417.00 24560.00 11-rela-93 3,4 14 1 21 37.00 14.08 0.33 14205417.00 24560.00 11-rela-93 3,4 14 1 314 37.00 14.08 0.33 1460542 10.0 24560.00 11-rela-93 3,4 14 1 314 37.00 14.08 0.33 1460542 10.0 2523.00 13-rela-93 3,4 14 1 314 37.00 14.08 0.33 1450513 18.49 26626.00 13-rela-93 3,4 14 1 332 36.00 14.08 0.33 155358 17.53 26991.00 13-rela-93 3,4 14 1 332 36.00 14.08 0.33 155358 17.53 26991.00 13-rela-93 3,4 14 1 332 36.00 14.08 0.33 155358 17.52 26991.00 13-rela-93 3,4 14 1 332 36.00 14.08 0.33 155239 13.79 20119.00 13-rela-93 3,4 14 1 330 37.00 14.08 0.33 155239 13.79 20119.00 13-rela-93 3,4 14 1 330 37.00 14.08 0.33 155358 17.52 26991.00 13-rela-93 3,4 14 1 330 37.00 14.08 0.33 155358 17.52 26991.00 13-rela-93 3,4 14 1 330 37.00 14.08 0.33 155359 17.52 26991.00 13-rela-93 3,4 14 1 330 37.00 14.08 0.33 155358 17.52 26991.00 13-rela-93 3,4 14 1 330 37.00 14.08 0.33 155358 17.52 26991.00 13-rela-93 3,4 14 1 330 37.00 14.08 0.33 155358 17.52 2690.00 13-rela-93 3,4 14 1 330 37.00 14.08 0.33 155358 17.52 2690.00 13-rela-93 3,4 14 1 330 37.00 14.08 0.33 155358 17.52 2690.00 13-rela-93 3,4 14 1 330 37.00 14.08 0.33 155358 17.52 2690.00 13-rela-93 3,4 14 14 1 330 37.00 14.08 0.33 155358 17.52 2690.00 13-rela-93 3,4 14 14 1 330 37.00 14.0	Date	Well	Static Feet		Conduc tivity	Temp °F	Static Level	Water Elevati	Meter on Reading	GPM	Gals/Day
29-Jan-93 3,4 13 6 193 38.00 13.07 0.74 setfmated 13.20 0.00 02-Feb-93 3,4 13 11 199 38.00 13.02 0.49 estimated 13.20 0.00 02-Feb-93 3,4 13 10.5 277 38.00 13.02 0.49 estimated 13.20 0.00 00-5-Feb-93 3,4 13 10.5 277 38.00 13.02 0.49 estimated 13.20 0.00 00-6-Feb-93 3,4 13 11 124 38.00 13.02 0.49 1295208 20.88 30074.00 06-Feb-93 3,4 13 11 124 38.00 13.02 0.49 1295208 20.88 30074.00 06-Feb-93 3,4 13 0 198 36.00 13.00 1.41 1325202 13.86 19963.00 08-Feb-93 3,4 15 0 204 34.00 13.00 1.41 1325202 13.86 19963.00 08-Feb-93 3,4 15 0 204 34.00 13.00 1.41 1325202 13.86 19963.00 10-Feb-93 3,4 14 1 124 37.00 14.08 0.33 1374183 14.98 21578.00 10-Feb-93 3,4 14 1 1345 37.00 14.08 0.33 1445011 17.03 26530.01 12-Feb-93 3,4 14 1 1315 37.00 14.08 0.33 1445011 17.03 26530.01 12-Feb-93 3,4 14 1 1325 37.00 14.08 0.33 1445011 17.03 26530.01 12-Feb-93 3,4 14 1 1325 37.00 14.08 0.33 1459613 18.49 26620.01 14-Feb-93 3,4 14 1 1325 37.00 14.08 0.33 1545635 18.49 26620.01 14-Feb-93 3,4 14 1 1325 37.00 14.08 0.33 1545635 18.49 26620.01 14-Feb-93 3,4 14 1 1325 37.00 14.08 0.33 1545635 18.49 26620.01 14-Feb-93 3,4 14 1 1330 37.00 14.08 0.33 1545635 18.49 26620.01 14-Feb-93 3,4 14 1 1330 37.00 14.08 0.33 1545635 18.49 26620.01 14-Feb-93 3,4 14 1 1330 37.00 14.08 0.33 1545635 18.49 26620.01 14-Feb-93 3,4 14 1 1330 37.00 14.08 0.33 1545635 18.49 26620.01 14-Feb-93 3,4 14 1 1330 37.00 14.08 0.33 1545635 18.49 26620.01 14-Feb-93 3,4 14 1 1330 37.00 14.08 0.33 1545636 18.49 26620.01 18-Feb-93 3,4 14 1 1330 37.00 14.08 0.33 1545636 18.29 227-Feb-93 3,4 14 1 1330 37.00 14.08 0.33 1545636 18.29 227-Feb-93 3,4 14 1 330 37.00 14.08 0.33 1545636 18.29 227-Feb-93 3,4 14 1 1330 37.00 14.08 0.33 164561 18.29 227-Feb-93 3,4 14 1 1330 37.00 14.08 0.33 164561 18.29 228-Feb-93 3,4 14 1 1330 37.00 14.08 0.33 164561 18.29 228-Feb-93 3,4 14 1 1330 37.00 14.08 0.33 164561 18.29 228-Feb-93 3,4 14 1 1330 37.00 14.08 0.33 164561 18.29 228-Feb-93 3,4 14 14 1 330 37.00 14.08 0.33 164561 18.29 228-Feb-93 3,4 14 14 1 330 36.00 14.08 0.33 164561 18.29 228-Feb-93 3,4 14 14 1 3	28-Jan-93	3.4	13	8	216	37,00	13.67	0.74	estimated	13.20	0.00
02-Feb-93 3,4 13 11 199 38.00 13.92 0.49 estimated 13.20 0.00 03-Feb-93 3,4 13 10.5 277 38.00 13.08 0.49 1275208 0.88 3007-00 06-Feb-93 3,4 13 11 214 38.00 13.02 0.49 1275208 0.88 3007-00 06-Feb-93 3,4 13 0 198 36.00 13.00 1.41 1325282 13.86 19963.00 08-Feb-93 3,4 13 0 204 34.00 13.00 1.41 1325282 13.86 19963.00 08-Feb-93 3,4 14 1 207 37.00 14.08 0.33 1374183 14.98 21578.00 09-Feb-93 3,4 14 1 124 37.00 14.08 0.33 1374183 14.98 21578.00 10-Feb-93 3,4 14 1 1345 37.00 14.08 0.33 142561 17.02 24560.00 11-Feb-93 3,4 14 1 1315 37.00 14.08 0.33 1445011 17.03 24550.00 12-Feb-93 3,4 14 1 1325 37.00 14.08 0.33 142561 17.03 24560.00 14-Feb-93 3,4 14 1 1325 37.00 14.08 0.33 1456024 20.13 28089.00 14-Feb-93 3,4 14 1 1325 37.00 14.08 0.33 1545361 81.49 26626.00 14-Feb-93 3,4 14 1 1325 37.00 14.08 0.33 1545361 81.49 26626.00 14-Feb-93 3,4 14 1 1325 37.00 14.08 0.33 1545361 81.49 26626.00 14-Feb-93 3,4 14 1 1330 37.00 14.08 0.33 1545361 81.49 26626.00 14-Feb-93 3,4 14 1 1330 37.00 14.08 0.33 1545361 81.49 26626.00 14-Feb-93 3,4 14 1 1330 37.00 14.08 0.33 1545361 81.49 26626.00 14-Feb-93 3,4 14 1 1330 37.00 14.08 0.33 1545361 81.49 26626.00 14-Feb-93 3,4 14 1 1330 37.00 14.08 0.33 1545361 81.49 26626.00 14-Feb-93 3,4 14 1 1330 37.00 14.08 0.33 1545361 81.49 26626.00 14-Feb-93 3,4 14 1 1330 37.00 14.08 0.33 1545361 81.49 26626.00 14-Feb-93 3,4 14 1 1330 37.00 14.08 0.33 1545361 81.72 24875.00 14-Feb-93 3,4 14 1 1330 37.00 14.08 0.33 1545361 81.72 24875.00 14-Feb-93 3,4 14 1 1330 36.00 14.08 0.33 164561 81.72 24875.00 14-Feb-93 3,4 14 1 1330 36.00 14.08 0.33 164561 81.72 24875.00 14-Feb-93 3,4 14 1 1330 36.00 14.08 0.33 164561 81.72 24875.00 14-Feb-93 3,4 14 1 1330 36.00 14.08 0.33 164561 81.72 24875.00 14-Feb-93 3,4 14 1 1330 36.00 14.08 0.33 164561 81.72 24850.00 14-Feb-93 3,4 14 1 1330 36.00 14.08 0.33 164561 81.72 24850.00 14-Feb-93 3,4 14 1 1330 36.00 14.08 0.33 164561 81.72 24850.00 14-Feb-93 3,4 14 1 1330 36.00 14.08 0.33 164561 81.72 24850.00 14.08 0.33 164561 81.72 24850.00 14.08 0.33 164561 81.72 24850.00 14.08 0.33 164			13				13.67	0.74			0.00
03-Feb-93 3,4 13 10.5 277 38.00 13.08 0.54 estimated 13.20 NA Feb-93 3,4 13 11 198 37.00 13.02 0.49 1273780 1.88 21428.00 05-Feb-93 3,4 13 0 198 36.00 13.00 1.41 1325282 13.86 199-30 07-Feb-93 3,4 14 1 200 14.08 0.33 1374181 1.98 12760 09-Feb-93 3,4 14 1 1 200 34.00 13.00 1.41 1325282 13.86 199-30 09-Feb-93 3,4 14 1 1 200 14.08 0.33 1374181 1.70 12 24780.00 11-Feb-93 3,4 14 1 1 304 37.00 14.08 0.33 1420541 17.02 24780.00 11-Feb-93 3,4 14 1 1 304 37.00 14.08 0.33 1420541 17.00 24503 11-Feb-93 3,4 14 1 1 304 37.00 14.08 0.33 1420541 17.00 24502 10.11-Feb-93 3,4 14 1 1 304 37.00 14.08 0.33 1420541 17.00 24502 10.11-Feb-93 3,4 14 1 1 304 37.00 14.08 0.33 1420541 17.00 24502 10.13-Feb-93 3,4 14 1 1 304 37.00 14.08 0.33 142054 17.00 24626.00 13-Feb-93 3,4 14 1 1 304 37.00 14.08 0.33 145054 17.00 24626.00 13-Feb-93 3,4 14 1 1 304 37.00 14.08 0.33 150545 13.07 2019-26626.00 15-Feb-93 3,4 14 1 1 302 34.00 14.08 0.33 150545 13.07 2019-26626.00 15-Feb-93 3,4 14 1 1 302 34.00 14.08 0.33 1570349 16.88 24315 0.15 14-Feb-93 3,4 14 1 1 320 34.00 14.08 0.33 1570349 16.88 24315 0.15 14-Feb-93 3,4 14 1 1 320 34.00 14.08 0.33 1570349 16.88 24315 0.15 14-Feb-93 3,4 14 1 1 330 37.00 14.08 0.33 1570349 16.88 24315 0.15 14-Feb-93 3,4 14 1 1 331 34.00 14.08 0.33 1570349 16.88 24315 0.15 14-Feb-93 3,4 14 1 1 331 34.00 14.08 0.33 1570349 17.22 24807.00 19-Feb-93 3,4 14 1 1 331 34.00 14.08 0.33 1570349 17.22 24807.00 19-Feb-93 3,4 14 1 1 331 34.00 14.08 0.33 161887 17.8 24275.00 19-Feb-93 3,4 14 1 1 330 34.00 14.08 0.33 161887 17.2 24875.00 19-Feb-93 3,4 14 1 1 330 34.00 14.08 0.33 161887 17.2 24875.00 19-Feb-93 3,4 14 1 1 340 34.00 14.08 0.33 161887 17.2 24875.00 19-Feb-93 3,4 14 1 1 340 34.00 14.08 0.33 171816 17.2 24875.00 19-Feb-93 3,4 14 1 1 340 34.00 14.08 0.33 171816 17.2 24875.00 19-Feb-93 3,4 14 1 1 340 34.00 14.08 0.33 171816 17.2 24875.00 19-Feb-93 3,4 14 14 1 340 34.00 14.08 0.33 171816 17.2 24875.00 19-Feb-93 3,4 14 14 1 340 34.00 14.08 0.33 171816 17.2 24875.00 19-Feb-93 3,4 14 14 1 340 34.00 14.08 0.33 171816 17.2 24875.00											
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16-Mar-93 3,4,5 NA NA 372 36.00 NA NA 2278871 18.22 26241.00 17-Mar-93 3,4,5 14 9 367 36.00 14.75 -0.34 2305112 18.28 26330.00 18-Mar-93 3,4,5 NA NA 364 36.00 NA NA 2331442 18.41 26512.00 19-Mar-93 3,4,5 NA NA 364 36.00 NA NA 2331442 18.41 26512.00 20-Mar-93 3,4,5 NA NA 356 36.00 NA NA 2410831 18.49 26620.00 21-Mar-93 3,4,5 NA NA 321 36.00 NA NA 2410831 16.07 23135.00 22-Mar-93 3,4,5 NA NA 372 37.00 NA NA 2466833 15.91 22911.00 23-Mar-93 3,4,5 NA NA 372 37.00 NA NA 2466833 15.91 22911.00 24-Mar-93 3,4,5 NA NA 446 37.00 NA NA 2519466 16.89 24317.50 25-Mar-93 3,4,5 NA NA 446 37.00 NA NA 2519466 16.89 24317.50 27-Mar-93 3,4,5 NA NA 446 37.00 NA NA 2642381 17.52 25230.00 30-Mar-93 3,4,5 NA NA 374 37.00 NA NA 2642381 17.52 25230.00 31-Mar-93 3,4,5 NA NA 374 37.00 NA NA 2642381 17.52 25230.00 31-Mar-93 3,4,5 NA NA 374 37.00 NA NA 2642381 17.52 25230.00 31-Mar-93 3,4,5 NA NA 302 37.00 NA NA 2695603 19.90 28649.00 01-Apr-93 3,4,5 NA NA 434 36.00 NA NA 2774252 15.32 22064.00 03-Apr-93 3,4,5 NA NA 463 36.00 NA NA 2771295 18.60 26790.00 05-Apr-93 3,4,5 NA NA 463 36.00 NA NA 2771295 18.60 26790.00 05-Apr-93 3,4,5 NA NA 416 36.00 NA NA 2824825 19.56 28160.00											
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24-Mar-93 3,4,5											
25-Mar-93 3,4,5 NA NA 446 37.00 NA NA 2519466 16.89 24317.50 27-Mar-93 3,4,5 14 11 388 37.00 14.92 -0.51 2568101 16.89 24315.00 29-Mar-93 3,4,5 14 11 355 37.00 14.92 -0.51 2616731 17.81 25650.00 30-Mar-93 3,4,5 NA NA 374 37.00 NA NA 2642381 17.52 25230.00 31-Mar-93 3,4,5 NA NA 374 37.00 NA NA 2667611 19.44 27992.00 01-Apr-93 3,4,5 NA NA 302 37.00 NA NA 2695603 19.90 28649.00 02-Apr-93 3,4,5 NA NA 302 37.00 NA NA 2695603 19.90 28649.00 02-Apr-93 3,4,5 NA NA 434 36.00 NA NA 2746316 17.35 24979.00 04-Apr-93 3,4,5 NA NA 463 36.00 NA NA 2771295 18.60 26790.00 05-Apr-93 3,4,5 NA NA 463 36.00 NA NA 2771295 18.60 26790.00 05-Apr-93 3,4,5 NA NA 416 36.00 NA NA 2824825 19.56 28160.00											
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31-Mar-93 3,4,5 14 11 411 37.00 14.92 -0.51 2667611 19.44 27992.00 01-Apr-93 3,4,5 NA NA 302 37.00 NA NA 2695603 19.90 28649.00 02-Apr-93 3,4,5 NA NA 434 36.00 NA NA 2746316 17.35 24979.00 03-Apr-93 3,4,5 NA NA 434 36.00 NA NA 2746316 17.35 24979.00 04-Apr-93 3,4,5 NA NA 463 36.00 NA NA 2771295 18.60 26790.00 05-Apr-93 3,4,5 NA NA 416 36.00 NA NA 2824825 19.56 28160.00											
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05-Apr-93 3,4,5 14 9 426 36.00 14.75 -0.34 2798085 18.57 26740.00 06-Apr-93 3,4,5 NA NA 416 36.00 NA NA 2824825 19.56 28160.00											
06-Apr-93 3,4,5 NA NA 416 36.00 NA NA 2824825 19.56 28160.00											

Appendix B

Gambell Pumphouse Well Data

					·					
Date	Well	Static		Conduc	) emp	Static	Water	Meter	<b>GPM</b>	Gals/Day
		Feet	Inches	tivity	۰F	Level	Elevation	Reading		
					74.00					
08-Apr-93 09-Apr-93		NA 14	NA 10	408 420	36.00 36.00	NA 1/ DZ	NA O / 7	2877467		26458.00
10-Apr-93	3.4.5	NA.	10 NA	440	36.00	14.83 NA	-0.42 NA	2903925 2931112		27187.00 26191.00
11-Apr-93		NA	NA NA	474	36.00	AK	NA	2957303		25535.00
12-Apr-93	3,4,5	14	11	483	36.00	14.92	-0.51	2982838		25267.00
13-Apr-93	3,4,5	NA	NA	456	36.00	МA	NA	3008105		26217.00
14-Apr-93	3,4,5	14	9	435	37.00	14.75	-0.34	3034322	-	25903.00
15-Apr-93 16-Apr-93	3,4,5	₩A 15	HA 1	445 400	37.00	NA 15 OB	NA -0.47	3060225		25970.00
28-Apr-93		NA.	NA.	\$27	38.00 35.00	15.08 NA	-0.67 NA	3086195 3377707		24292.67 23564.00
29-Apr-93	- ,	NA	NA	493	35.00	NA	NA	3401271		28644.00
30-Apr-93		NА	NA	524	35.00	NA	NA	3429915		22626.08
24-May-93		NA	NA	292	36.00	NA	NA	3972941	14.25	20520.00
25-May-93		NA	NA	296	36.00	NA	NA	3993461		19837.00
28-May-93		NA MA	AK	283	37.00	AK	NA	4052972		19936.75
01-Jun-93 03-Jun-93		NA NA	NA NA		38.00 36.00	AK VA	NA VA	4132719 4179821		23551.00
05-Jun-93		NA.	NA NA		36.00	AK AK	NA NA	4226973		23576.00 13454.00
07-Jun-93		AK	NA		36.00	NA	NA	4253881		21106.00
09-Jun-93	4	8	8		36.00	8.67	5.74	4296093		19295.00
11-Jun-93		8	10		36.00	8.83	5.58	4334683	14.15	20381.14
18-Jun-93		8	9	137	36.00	8.75	5.66	4477351		20856.67
21-Jun-93 22-Jun-93		NA	AK	136	36.00	NA	NA	4539921		20874.00
24-Jun-93	_ ,	NA 7	NA 9	132 137	36.00 36.00	NA 7.75	NA 6.66	4560795 4606424		22814.50 21951.00
25-Jun-93		8	11	137	20.00	8.92	5.49	4628375		21402.33
28-Jun-93		8	0	140	37.00	8.00	6.41	4692582		24158.00
29-Jun-93	,	9	1	140	37.00	9.08	5.33	4716740	15.54	22384.00
02 - Jul - 93		9	0	143	37.00	9.00	5.41	4783892		18191.67
05-Jul-93		NA MA	NA	148	37.00	NA	NA	4838467		26339.00
07-Jul-93 08-3ul-93	•	ИА 9	<b>N</b> A 6	151 151	37.00 37.00	NA 9.50	NA 4.91	4891145 4917445		26300.00
09-Jul-93		ý	7	144	37.00	9.58	4.83	4938460		21015.00 22369.00
12-Jul-93		9	9	150	37.00	9.75	4.66	5005567		22937.00
14-Jul <i>-9</i> 3	•	9	10	151	37.00	9.83	4.58	5051441		20489.00
16-Jul-93	•	9	10	150	37.00	9.83	4.58	5092419		21106.67
19-Jul-93	•	10	0	158	37.00	10.00	4.41	5155739		21425.50
21-Jul-93 23-Jul-93	• .	10 10	0 3.5	162 182	37.00	10.00	4.41	5198590		21189.00
26-Jul-93		10	5.5	169	39.00 38.00	10.29 10.46	4.12 3.95	5240968 5303622		20884.67 22107.50
28-Jul-93	•	10	7.5	216	36.00	10.63	3.79	5347837		20787.50
30-Jul-93		10	8.5	202	36.00	10.71	3.70	5389412		22642.67
02-Aug-93	3,4	10	10.5	182	36.00	10.88	3.54	5457340		21788.50
04-Aug-93		10	8.5	183	36.00	10.71	3.70	5500917		22082.00
06-Aug-93		11 11	0	182	36.00	11.00	3.41	5545081		23353.00
09-Aug-93 11-Aug-93		11	1 2	186 179	36.00 36.00	11.08	3.33 3.24	5615140 5658794		21827.00 22476.50
13-Aug-93		11	3	230	36.00	11.25	3.16	5703747		22894.00
16-Aug-93		11	1.5	186	37.00	11.13	3.29	5772429		22741.00
18-Aug-93		11	0.5	194	37.00	11.04	3.37	5817911		22070.50
20-Aug-93		10	4.5	186	37.00	10.38	4.04	5862052		23231.33
23-Aug-93		9	10	189	38.00	9.83	4.58	5931746		20770.50
25-Aug-93 27-Aug-93	•	10 10	0.5 1.5	177 179	38.00	10.04 10.13	4.37	5973287		21871.00
30-Aug-93	3,4	NA NA	NA	185		NA	4.29 NA	6017029 6041916		8295.67 NA
31-Aug-93		NA.	NA NA	182		AK	AK	19908	9.81	14133.25
08-Sep-93		10	3,5	195	40.00	10.29	4.12	132974	14.09	20289.50
10-Sep-93		10	6	195	40.00	10.50	3.91	173553	16.26	23413.00
13-Sep-93	•	10	10	193	36.00	10.83	3.58	243792	12.62	18170.50
15-Sep-93		10	6.5	189	36.00	10.54	3.87	280133	15.27	21992.50
17-Sep-93 20-Sep-93		11 10	0 8.5	191 186	38.00 39.00	11.00	3.41 3.70	324118	15.65	22529.33
22-Sep-93		10	5.5	192	40.00	10.71	3.70	391706 437434	15.88 15.01	22864.00 21620.50
24-Sep-93		10	3.4	190	40.00	10.33	4.08	480675	15.37	22134.33
27-Sep-93	3,4	10	7.5	189	38.00	10.63	3.79	547078	15.26	21981.50
29-Sep-93	3,4	10	7.5	188	38.00	10.63	3.79	591041	14.02	20192.50

Appendix B

Gambell Pumphouse Well Data

Date	Well	Static Feet		Conduc tivity	Temp °F	Static Level	Water Elevation	Meter Reading	GPM	Gals/Day
01-0ct-93		9	10	205	38.00	9.83	4.58	631426	14.25	20524.20
06-0ct-93		9	9	189	36.00	9.75	4.66	734047	13.66	19675.50
08-Oct-93	•	9	10	186	36.00	9.83	4.58	773398	14.63	21071.00
11-0ct-93		9	11.5	188	36.00	9.96	4.45	836611	14.83	21353,50
13-Oct-93		9	11	197	36.00	9.92	4.49	879318	14.61	21039.50
15-0ct-93	,	9	10.5	201	38.00	9.88	4.54	921397	18.93	27262.00
18-0ct-93		10	1.5	195	42.00	10.13	4.29	1003183	6.57	9462.50
20-Oct-93		10	2	207	39.00	10.17	4.24	1022108	11.34	16332.00
22-Oct-93		10	1.5	200	39.00	10.13	4.29	1054772	13.49	19428.40
01-Nov-93		10	5	198	39.00	10.42	3.99	1249056		16768.00
03-Nov-93	•	10	4.5	195	41.00	10.38	4.04	1282592		19385.00
05-Nov-93		10	2	198	40.00	10.17	4.24	1321362		17750,00
08-Nov-93		10	0.5	193	39.00	10.04	4.37	1374612		15400.50
10-Nov-93		9	7.5	192	39.00	9.63	4.79	1405413		15982.00
12-Nov-93	- •	8	6.5	198	39.00	8.54	5.87	1437377		18886.00
15-Nov-93		7	_10	215	39.00	7.83	6.58	1494035		16539.00
17-Nov-93	•	8	5.5	212	39.00	8.46	5.95	1527113		18359.50
19-Nov-93		9	2	211	39.00	9.17	5.24	1563832		16456.60
24-Nov-93	•	10	0	214	38.00	10.00	4.41	1646115		19254.00
26-Nov-93		10	0.5	221	39.00	10.04	4.37	1684623		18386.67
29-Nov-93	•	10	5.5	215	39.00	10.46	3.95	1739783		18575.50
01-Dec-93		10	6.5	225	39.00	10.54	3.87	1776934		19638.50
03-Dec-93	,	11	2	227	37.00	11.17	3.24	1816211		17598.00
06-Dec-93		11	0	230	36.00	11.00	3.41	1869005		19878.50
08-Dec-93		11	2.5	233	39.00	11.21	3.20	1908762		17760.50
10-Dec-93		11	6.5	247	39.00	11.54	2.87	1944283		17806.67
13-Dec-93		12	0	249	37.00	12.00	2.41	1997703		19145.00
15-Dec-93		12	1	250	37.00	12.08	2.33	2035993		19519.00
17-Dec-93		12	0	249	37.00	12.00	2.41	2075031		19175.00
20-Dec-93 22-Dec-93	•	12 12	5 4	243 245	36.00	12.42	1.99	2132556		22096.00
18-Jan-94	•	14	1.5	261	36.00 39.00	12.33 14.13	2.08 0.29	2176748 2827255		24092.85 15316.00
20-Jan-94	,	14	1.3	271	39.00	14.17	0.24	2857887		29470.50
22-Jan-94		34	1	271	39.00	14.08	0.24	2916828		44850.00
24-Jan-94		14	ò	285	39.00	14.00	0.41	3006528		4348.00
26-Jan-94		13	11.5	288	39.00	13.96	0.45	3015224		56474.50
28-Jan-94		13	10.5	288	39.00	13.88	0.54	3128173		28274.00
31-Jan-94		14	6	294	39.00	14.50	-0.09	3212995		28809.00
02-Feb-94	•	14	6	295	39.00	14.50	-0.09	3270613		30244.50
04 - Feb - 94		14	6	297	39.00	14.50	-0.09	3331102		29907.00
07-Feb-94		14	5	293	39.00	14.42	-0.01	3420823		28035.00
09-Feb-94	•	14	4	316	39.00	14.33	0.08	3476893		28958.50
11-Feb-94	_ '	14	4	328	39.00	14.33	0.08	3534810		28913.29
28-Feb-94		14	9.5	363	39.00	14.79	-0.38	4026336		40788.00
01-Mar-94	_ •	14	9	356	39.00	14.75	-0.34	4067124		37630.00
03-Mar-94		14	10	355	39.00	14.83	-0.42	4142384		21062.50
07-Mar-94		15	0	354	39.00	15.00	-0.59	4226634		30875.50
09-Mar-94	•	15	1	359	39.00	15,08	-0.67	4288385		46063.50
11-Mar-94		15	2	365	39.00	15.17	-0.76	4380512		14264.33
14-Mar-94		15	3	372	40.00	15.25	-0.84	4423305		27568.00
16-Mar-94	3,4	15	3	368	40.00	15.25	-0.84	4478441		27293.00
16-Mar-94		15	3	392	40.00	15.25	-0.84	4533027		26619.00
22-Mar-94		15	3	416	39.00	15.25	-0.84	4639503		134.81

Appendix C
Gambell Observation Well #1

Ħm	Dd	Υу	Яг	Mn	Ss AirT	WaterT	Stage	Conductivity	Mon	D	d Y	У	Нг	Mn	Ss AirT	₩aterĭ	Stage	Conductivity
1	5	94	17	31	59 -10.1	0.74	3.65	247	1	1	0 9	4	17	31	59 -12.7	8.0	3.38	264
i	Š	94	20	31	59 -6.52	0.82	3.64	235	1	1	0 9	4	20	31	59 -12.8	0.8	3.37	263
ì	5	94	23	31	59 -7.5	0.83	3.63	232	1	1	0 9	4	23	31	59 -13.2	0.8	3.36	263
1	6	94	2	31	59 -8.44	0.84	3.62	231	1	1			2	31	59 -13.6	0.79	3.36	262
1	6	94	5	31	59 -8.86	0.85	3.61	232	1	1			5	31	59 -13.8	0.79	3.35	263
1	6	94	8	31	59 -9,01	0.85	3.6	238	1	1			8	31	59 -14.1	0.79	3.35	263
1	6	94	11	31	59 -9.06	0.85	3.6	249	1	1			11	31	59 -14-5	0.79	3.34	263
1	6	94	14	31	59 -8.9	0.85	3.61	256	1		1 9		14	31	59 -14-6	0.79	3.33	261
1	6	94	17	31	59 -8.78	0.85	3.61	253	1		1 9		17	31	59 -14.8	0.78	3.33	263
1	6	94	20	31	59 -8.75	0.85	3.6	252	1	1			20	31	59 -15.1	0.78	3.32	261
1	6	94	23	31	59 -9.03	0.84	3.6	249	1	1	•	-	2.3	31	59 -15.2	0.78	3.31	261
1	7	94	2	31	59 -9.39	0.84	3.59	247	1		2 9		2	31	59 -15-4	0.78	3.31	261
1	7	94	5	31	59 -9.22	0.84	3.59	247	1		2 9		5	31	59 -15-3	0.78	3.3 3.29	258 258
1	7	94	8	31	59 -9.33	0.84	3.59	246	1		2 9		8	31	59 -15.4	0.78 0.77	3.28	258
1	7	94	11	31	59 -9.43	0.83	3.58	246	1		2 9		11 14	31 31	59 -15.8 59 -16.2	0.77	3.27	258 258
1	7	94	14	31	59 -9.62	0.83	3.58	246	1		2 9			31	59 -16.2 59 -16	0.77	3.27	260
1	7	94	17	31	59 -9.73	0.83	3.57	246	1		2 9		17 20	31	59 -16.5	0.77	3.26	257
1	7	94	20	31	59 -9.95	0.83	3.56	251	1		2 9		23	31	59 -16.8	0.77	3.25	258
1	7	94	23	31	59 -10-4	0.83	3.56 3.55	277 279	1		3 9		2	31	59 ~16.4	0.76	3.24	259
1	8	94	2	31	59 -11-3	0.83	3.54	277	1		3 9		5	31	59 -16.1	0.76	3.23	258
1	8	94	5	31	59 -11.8 59 -12.8	0.82 0.82	3.53	276	1		3 9		8	31	59 -15.7	0.76	3.23	256
1	8	94	8	31	59 -12.8	0.82	3.52	273	1		3 9	-	11	31	59 -15-6	0.76	3.22	258
1	8 8	94 94	11 14	31 31	59 -12.0	0.82	3.51	273	1		3 9		14	31	59 -15.3	0.76	3.21	259
1	8	94	17	31	59 -12.2	0.82	3.5	273	1		3 9		17	31	59 -15.6	0.76	3.21	258
- 1	8	94	20	31	59 -12.6	0.82	3.5	271	i		3 9		20	31	59 ~16	0.76	3.2	259
1	8	94	23	31	59 -12.9	0.82	3.49	272	1		3 9		23	31	59 -16.1	0.75	3.19	258
1	9	94	2	31	59 -12-9	0.81	3.48	271	1		4 9		2	31	59 ~16	0.75	3.19	259
ì	9	94	5	31	59 -12.9	0.81	3.47	272	1	1	4 9	4	5	31	59 -16.2	0.75	3.18	259
1	ó	94	8	31	59 -13	0.81	3,46	271	1	1	4 9	4	8	31	59 -16.3	0.75	3.18	260
1	ģ	94	11	31	59 -12.9	0.81	3,46	269	1	1	4 9	4	11	31	59 -16.2	0.74	3.17	261
ì	9	94	14	31	59 -12-6	0.81	3.45	269	1	1	4 9	4	14	31	59 -15.6	0.74	3.17	261
1	9	94	17	31	59 -12.3	0.81	3.44	270	1	1	4 9		17	31	59 -14.9	0.74	3.16	262
1	9	94	20	31	59 -12.2	0.81	3.43	270	1	_	4 9		20	31	59 -14.3	0.74	3.15	262
1	9	94	23	31	59 -12.1	0.81	3.43	269	1		4 9		23	31	59 -13.9	0.74	3.15	263
1	10	94	2	31	59 -12	0.81	3.42	267	1		5 9		2	31	59 -13.5	0.74	3.14	264
1	10	94	5	31	59 -12.1	0.8	3.41	265	1		5 9		5	31	59 -13.2	0.74	3.13	266
1	10	94	8	31	59 -12.4	0.8	3.4	264	1		5 9		8	31	59 -13.1	0.73	3.13	266
1	10	94	11	31	59 -12.4	0.8	3.39	263	1		5 9		11	31	59 -13.2	0.73	3.12	266
1	10	94	14	31	59 -12.6	0.8	3.39	263	1	1	5 9	4	14	31	59 -13.2	0.73	3.11	266

This is the raw data as recorded by the data logger, and is raw data for app. E.

Appendix C
Gambell Observation Well #1

Mm	Dd	Υу	Hr	Mn	Ss AirT	WaterT	Stage	Conductivity	Man	Do	d Yy	Кr	Mn	Ss AirT	WaterT	Stage	Conductivity
1	15	94	17	31	59 -13.3	0.73	3.11	266	1	20	94	23	31	59 -14.8	0.69	2.86	254
1	15	94	20	31	59 -13.5	0.73	3.1	267	i	21		2	31	59 -14.7	0.69	2.86	255
1	15	94	23	31	59 -13.6	0.73	3.1	266	ì	21		5	31	59 -14.5	0.69	2.86	254
1	16	94	2	31	59 -14.2	0.73	3.09	266	1	21		8	31	59 -14.2	0.68	2.86	254
1	16	94	5	31	59 ~14.5	0.73	3.09	265	1	21	94	11	31	59 -14	0.68	2.85	255
i	16	94	8	31	59 -14.6	0.73	3.08	266	1	21	94	14	31	59 -13.8	0.68	2.85	255
1	16	94	11	31	59 -14.8	0.72	3.07	265	1	21	94	17	31	59 -13.3	0.68	2.84	256
1	16	94	14	31	59 -14.5	0.72	3.07	264	1	21	94	20	31	59 -12.9	0.68	2.84	256
1	16	94	17	31	59 -14.3	0.72	3.07	264	1	21	94	23	31	59 -12.5	0.69	2.84	256
ì	16	94	20	31	59 -14.2	0.72	3.06	265	1	22	94	2	31	59 -12.3	0.68	2.83	256
1	16	94	23	31	59 -13.8	0.72	3.06	264	1	22	94	5	31	59 -12.1	0.68	2.83	257
1	17	94	2	31	59 -13.7	0.71	3.05	265	1	22		8	31	59 -12	0.68	2.82	256
1	17	94	5	31	59 ~13.6	0.71	3.05	265	1	22	2 94	13	31	59 ~11.9	0.68	2.82	257
1	17	94	8	31	59 -13.6	0.71	3.04	264	1	22		14	31	59 -11.7	0.68	2.82	259
1	17	94	11	31	59 -13.9	0.71	3.04	263	1	22		17	31	59 -11.6	0.69	2.81	260
1	17	94	14	31	59 -14.3	0.71	3.03	262	1	2,2		20	31	59 -11.6	0.68	2.81	259
1	17	94	17	31	59 -14.5	0.71	3.02	262	1	22		23	31	59 -11.6	0,68	2,81	261
1	17	94	20	31	59 -14-3	0.71	3.01	762	1	23		2	31	59 -11.7	0-68	2.8	262
1	37	94	23	31	59 -14.3	0.71	3.01	261	1	23		5	31	59 -11.9	0.68	2.8	262
1	18	94	2	31	59 -14-1	0.7	3	261	1	23		8	31	59 -12.3	0.68	2.8	264
1	18	94	5	31	59 -14	0.7	2.99	261	1	23		11	31	59 -12.7	0.68	2.79	266
1	18	94	8	31	59 -14	0.7	2.98	261	1	2.3		14	31	59 -13.4	0.68	2.79	266
1	18	94	11	31	59 -14-2	0.7	2.98	261	1	23		17	31	59 -14	0.68	2.79	269
1	18	94	14	31	59 -14	0.7	2.97	260	1	23		20	31	59 -14.9	0.68	2.78	270
1	18	94	17	31	59 -13.9	0.7	2.96	260	,	23		23	31	59 -15.8	83.0 83.0	2.78	271 27 <b>3</b>
1	18	94	20	31	59 -14	0.7	2.95	259	!	24	-	2	31	59 -16.4 59 -16.9	0.68	2.77	274
1	18	94	23	31	59 -14-2	0.7	2.95	259	1	24		5	31 31	59 - 17.5	0.68	2.77	276
1	19	94	2	31	59 -14-4	0.7	2.94	258	1	24		8 11	31	59 - 17.7	0.68	2.77	277
1	19	94	5	31	59 -14.5	0.7	2.93	257	- 1	24		14	31	59 -17.9	0.68	2.76	277
1	19	94	.8	31	59 -14.7	0.7	2.92	258 257		24		17	31	59 -17.9	0.68	2.76	278
1	19	94	11	31	59 -14.8 59 -14.8	0.69	2.92	257	1	24		20	31	59 -18.2	0.68	2.76	280
1	19	94 94	14	31	59 -14.8	0.69	2.9	256	1	24	-	23	31	59 -18.1	0.68	2.75	282
ı	19 19	94	17 20	31 31	59 -14.7	0.69 0.69	2.9	256	1	25		2	31	59 -17.9	0.68	2.75	283
,	19	94	23	31	59 -14.6	0.69	2.89	256	i	25		5	31	59 -17.6	0.68	2.74	285
	20	94	23	31	59 -14.9	0.69	2.89	256	i	25		8	31	59 -17.5	0.68	2.74	288
4	50	94	5	31	59 -15	0.69	2.88	256	i	25		11	31	59 -17.5	0.68	2.74	290
4	20	94	8	31	59 -15.3	0.69	2.88	257	1	25		14	31	59 -17.4	0.68	2.73	292
1	20	94	11	31	59 -15.6	0.69	2.87	255	1	25		17	31	59 -17.4	0.69	2.73	293
1	20	94	14	31	59 -15.8	0.69	2.87	255	i	25		20	31	59 -17.8	0.68	2.73	294
	20	94	17	31	59 -15.5	0.69	2.87	254	1	25		23	31	59 -17.9	0.69	2.72	296
4	20	94	20	31	59 -14.9	0.69	2.86	255	i	26		2	31	59 -18	0.69	2.72	297
	40	74	20	٦.	27 1417	V.07	2.00		•	~-		-	-	·-			

Appendix C
Gambell Observation Well #1

Иm	Dď	Υу	Нг	Mn	Ss AirT	WaterT	Stage (	Conductivity	Mm	Dd	Yу	Hr	Mn	Ss AirT	WaterT	Stage (	Conductivity
1	26	94	5	31	59 -18	0.69	2.72	299	1	31	94	11	31	59 -7.82	0.69	2,62	322
4	26	94	8	31	59 -18.5	0.69	2.71	301	1	31	94	14	31	59 -7.08	0.69	2.62	324
1	26	94	11	31	59 -18-6	0.69	2.71	302	1	31	94	17	31	59 ~6.36	0.69	2.63	324
í	26	94	14	31	59 -18.4	0.69	2.71	304	1	31	94	20	31	59 -6.09	0.69	2.62	324
1	26	94	17	31	59 -18.2	0.69	2.71	305	1	31	94	23	31	59 -5.59	0.69	2.62	325
1	26	94	50	31	59 -18.2	0.69	2.71	306	2	1	94	2	31	59 -5.27	0.69	2.62	324
1	26	94	23	31	59 -18.2	0.69	2.71	307	2	1	94	5	31	59 -4.99	0.69	2-62	326
1	27	94	2	31	59 -18	0.69	2.7	307	2	1	94	8	31	59 -4.62	0.68	2.62	326
1	27	94	5	31	59 -18.1	0.69	2.7	309	2	1	94	11	31	59 -4.23	0.68	2.63	326
1	27	94	8	31	59 -18.2	0.69	2.7	309	2	1	94	14	31	59 -4.33	0.68	2.63	325
1	27	94	11	31	59 -18.4	0.69	2.7	309	2	1	94	17	31	59 -4.34	0.68	2-64	326
1	27	94	14	31	59 -18.3	0.7	2.7	311	5	1	94	20	31	59 -4.14	0.68	2.63	326
1	27	94	17	31	59 -18.2	0.7	2.7	312	2	1	94	23	31	59 -4-01	0.67	2.64	327
1	27	94	50	31	59 -18.3	0.7	2.7	312	2	2		2	31	59 -3.84	0.67	2.64	327
1	27	94	23	31	59 ~18.5	0.7	2.69	313	2	2		5	31	59 -4-01	0.67	2.64	326
1	28	94	2	31	59 -18-4	0.7	2.69	313	2	2		8	31	59 -4.49	0.67	2.64	326
1	28	94	5	31	59 -18.3	0.7	2.69	314	5	2		11	31	59 -4.61	0.66	2.65	326
1	28	94	8	31	59 -18.2	0.7	2.68	314	2	2		14	31	59 -4-65	0.66	2.65	326
1	28	94	11	31	59 -18.1	0.7	2.68	314	2	2		17	31	59 ~4.61	0.66	2.65	326 327
1	28	94	14	31	59 -17.8	0.7	2.68	315	2	2		20	31	59 -4.39	0.66	2.65	
3	28	94	17	31	59 ~17-6	0.7	2.67	316	2	2		23	31	59 -4.45	0.66	2.65 2.65	327 329
1	28	94	20	31	59 -17.3	0.7	2.67	317	2	3		2	31	59 ~4.45	0.65	2.66	328
1	28	94	23	31	59 -16.9	0.7	2.67	317	2	3		5	31	59 -4.4 59 -4.49	0.65 0.65	2.66	329
3	29	94	5	31	59 -16.3	0.7	2.67	317	2	3		8	31 31	59 -4.63	0.64	2.66	328
1	29	94	5	31	59 -15.7	0.7	2.66	320	2	3		11 14	31	59 -4.67	0.64	2.66	328
1	29	94	8	31	59 -15.3	0.7	2.66	319	2	3 3		17	31	59 -4.72	0.64	2.67	329
1	29	94	11	31	59 -15	0.7	2.66	319 319	2	ب 3		20	31	59 -4.89	0.64	2.67	330
1	55	94	14	31	59 -14-6	0.7	2.65	319	2	3		23	31	59 -4.96	0.63	2,67	330
1	29	94	17 20	31 31	59 -14.4 59 -14.3	0.7 0.7	2.65 2.65	320	2	4	94	2	31	59 -5.12	0.63	2.67	330
1	29	94 94	23	31	59 -14.2	0.7	2.65	320	2	4	94	5	31	59 -5.07	0.63	2.67	330
1	29 30	94	2	31	59 -14.2	0.7	2.64	319	2	4	94	á	31	59 -4.97	0.62	2.67	331
1	30	94	5	31	59 -13.9	0.7	2.64	319	2	7	94	11	31	59 -4.88	0.62	2.68	331
	30	94	8	31	59 -13.5	0.7	2.64	319	2	4	94	14	31	59 -4.79	0.62	2.68	331
4	30	94	11	31	59 -13	0.7	2.64	320	2	4	94	17	31	59 -4.69	0.62	2.68	333
1	30	94	14	31	59 -12.4	0.7	2.63	319	2	4	94	20	31	59 -4.59	0.61	2.68	332
4	30	94	17	31	59 -11.3	0.69	2.63	321	2	4		23	31	59 -4.54	0.61	2.69	333
1	30	94	20	3 t	59 -10	0.69	2.63	322	ž	5	94	2	31	59 -4.53	0.61	2.69	333
i	30	94	23	31	59 -9.84	0.69	2.63	320	2	5	94	5	31	59 -4.58	0.6	2.69	333
1	31	94	2	31	59 ~9.22	0.69	2.63	321	2	5	94	8	31	59 -4.62	0.6	2.7	332
1	31	94	5	31	59 -8.98	0.69	2.63	321	2	5	94	11	31	59 -4.61	0.6	2.7	333
-	31	94	8	31	59 -8.58	0.69	2.63	321	2	5		14	31	59 -4.6	0.6	2.7	332

Appendix C
Gambell Observation Well #1

2 S 94 17 31 S9 -4.54 0.59 2.7 333 2 10 94 23 31 S9 -12.6 0.48 2.86 309 2 S 94 20 31 S9 -4.54 0.59 2.7 334 2 11 94 2 31 S9 -12.8 0.48 2.85 307 2 6 94 22 31 S9 -4.54 0.59 2.71 334 2 11 94 8 31 S9 -13.5 0.48 2.85 307 2 6 94 2 31 S9 -4.54 0.59 2.71 334 2 11 94 8 31 S9 -13.5 0.48 2.84 306 2 6 94 5 31 S9 -4.44 0.59 2.71 331 2 11 94 11 31 S9 -13.5 0.48 2.84 306 2 6 94 8 31 S9 -4.45 0.58 2.72 331 2 11 94 11 31 S9 -13.6 0.47 2.84 305 2 6 94 11 31 S9 -4.45 0.58 2.72 331 2 11 94 11 31 S9 -13.4 0.47 2.84 305 2 6 94 11 31 S9 -4.45 0.58 2.72 332 2 11 94 17 31 S9 -12.9 0.47 2.84 305 2 6 94 17 31 S9 -4.45 0.58 2.73 330 2 11 94 20 31 S9 -12.7 0.47 2.83 304 2 6 94 20 31 S9 -4.45 0.58 2.73 330 2 11 94 20 31 S9 -12.6 0.47 2.83 304 2 6 94 20 31 S9 -4.45 0.57 2.74 330 2 11 94 20 31 S9 -12.6 0.47 2.83 304 2 6 94 20 31 S9 -4.46 0.58 2.73 330 2 11 94 20 31 S9 -12.6 0.47 2.83 304 2 6 94 20 31 S9 -4.46 0.58 2.73 330 2 11 94 20 31 S9 -12.6 0.47 2.83 304 2 6 94 20 31 S9 -4.46 0.58 2.73 330 2 11 94 20 31 S9 -12.6 0.47 2.83 304 2 6 94 20 31 S9 -4.46 0.58 2.75 328 2 1 94 8 31 S9 -4.8 0.46 2.82 303 2 7 94 2 31 S9 -4.48 0.57 2.75 328 2 1 94 8 31 S9 -4.8 0.46 2.82 303 2 7 94 2 31 S9 -4.64 0.56 2.76 328 2 1 2 94 8 31 S9 -12.6 0.47 2.83 304 2 7 94 5 31 S9 -4.66 0.56 2.75 328 2 1 2 94 11 31 S9 -2.6 0.46 2.81 303 2 7 94 11 31 S9 -4.66 0.56 2.76 328 2 12 94 17 31 S9 -12.5 0.46 2.81 303 2 7 94 11 31 S9 -4.66 0.56 2.76 328 2 12 94 17 31 S9 -12.6 0.45 2.79 302 2 7 94 10 31 S9 -4.65 0.55 2.78 325 2 13 94 2 31 S9 -12.6 0.45 2.79 302 2 7 94 20 31 S9 -4.65 0.55 2.78 325 2 13 94 2 31 S9 -12.6 0.45 2.79 302 2 7 94 20 31 S9 -4.67 0.56 2.77 327 2 12 94 20 31 S9 -12.6 0.45 2.79 302 2 7 94 20 31 S9 -4.67 0.56 2.77 327 2 12 94 20 31 S9 -12.6 0.45 2.79 302 2 7 94 20 31 S9 -4.67 0.55 2.78 325 2 13 94 2 31 S9 -12.6 0.45 2.79 302 2 7 94 20 31 S9 -4.67 0.56 2.77 327 2 12 94 20 31 S9 -10.8 0.44 2.75 304 2 8 94 2 31 S9 -4.69 0.55 2.78 325 2 2 13 94 2 31 S9 -10.8 0.44 2.76 303 2 8 94 2 31 S9 -4.59 0.55 2.79 324 2 13 94 17 31 S9 -10.8 0.44 2.76 303 2 8 94 2 31 S9 -4.69 0.	Mm	рd	Υу	Нr	Mn	TriA 22	₩aterĭ	\$tage	Conductivity	Man	Dd	Υу	Hr	Mn	\$s AirT	WaterT	Stage C	onductivity
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2 8 94 14 31 59 -4.95 0.54 2.82 322 2 13 94 20 31 59 -10.8 0.44 2.74 304 2 8 94 17 31 59 -4.87 0.53 2.82 321 2 13 94 23 31 59 -10.8 0.44 2.74 304 2 8 94 20 31 59 -4.98 0.53 2.83 320 2 14 94 2 31 59 -11.3 0.44 2.73 303 2 8 94 23 31 59 -4.97 0.53 2.83 321 2 14 94 5 31 59 -11.3 0.44 2.72 304 2 9 94 2 31 59 -5.19 0.52 2.84 319 2 14 94 8 31 59 -12.4 0.44 2.71 305 2 9 94 5 31 59 -5.38 0.52 2.84 318 2 14 94 11 31 59 -12.9 0.43 2.71 305 2 9 94 8 31 59 -5.66 0.52 2.84 320 2 14 94 14 31 59 -13.1 0.43 2.7 306 2 9 94 11 31 59 -5.81 0.51 2.85 318 2 14 94 17 31 59 -12.9 0.43 2.7 306		-		_						_								
2       8       94       17       31       59       -4.87       0.53       2.82       321       2       13       94       23       31       59       -10.8       0.44       2.74       304         2       8       94       20       31       59       -4.98       0.53       2.83       320       2       14       94       2       31       59       -11.3       0.44       2.73       303         2       8       94       23       31       59       -4.97       0.53       2.83       321       2       14       94       5       31       59       -11.9       0.44       2.72       304         2       9       94       2       31       59       -5.19       0.52       2.84       319       2       14       94       8       31       59       -12.4       0.44       2.71       305         2       9       94       5       31       59       -5.38       0.52       2.84       318       2       14       94       11       31       59       -12.9       0.43       2.71       306         2       9       94       18																		
2     8     94     20     31     59     -4.98     0.53     2.83     320     2     14     94     2     31     59     -11.3     0.44     2.73     303       2     8     94     23     31     59     -4.97     0.53     2.83     321     2     14     94     5     31     59     -11.9     0.44     2.72     304       2     9     94     2     31     59     -5.19     0.52     2.84     319     2     14     94     8     31     59     -12.4     0.44     2.71     305       2     9     94     5     31     59     -5.38     0.52     2.84     318     2     14     94     11     31     59     -12.9     0.43     2.71     305       2     9     94     8     31     59     -5.66     0.52     2.84     320     2     14     94     14     31     59     -13.1     0.43     2.7     306       2     9     94     11     31     59     -5.81     0.51     2.85     318     2     14     94     17     31     59     -12.9     0.43 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>																		
2 8 94 23 31 59 -4.97 0.53 2.83 321 2 14 94 5 31 59 -11.9 0.44 2.72 304 2 9 94 2 31 59 -5.19 0.52 2.84 319 2 14 94 8 31 59 -12.4 0.44 2.71 305 2 9 94 5 31 59 -5.38 0.52 2.84 318 2 14 94 11 31 59 -12.9 0.43 2.71 305 2 9 94 8 31 59 -5.66 0.52 2.84 320 2 14 94 14 31 59 -13.1 0.43 2.7 306 2 9 94 11 31 59 -5.81 0.51 2.85 318 2 14 94 17 31 59 -12.9 0.43 2.7 306		_																
2 9 94 2 31 59 -5.19 0.52 2.84 319 2 14 94 8 31 59 -12.4 0.44 2.71 305 2 9 94 5 31 59 -5.38 0.52 2.84 318 2 14 94 11 31 59 -12.9 0.43 2.71 305 2 9 94 8 31 59 -5.66 0.52 2.84 320 2 14 94 14 31 59 -13.1 0.43 2.7 306 2 9 94 11 31 59 -5.81 0.51 2.85 318 2 14 94 17 31 59 -12.9 0.43 2.7 306		_								_								
2 9 94 5 31 59 -5.38 0.52 2.84 318 2 14 94 11 31 59 -12.9 0.43 2.71 305 2 9 94 8 31 59 -5.66 0.52 2.84 320 2 14 94 14 31 59 -13.1 0.43 2.7 306 2 9 94 11 31 59 -5.81 0.51 2.85 318 2 14 94 17 31 59 -12.9 0.43 2.7 306																		
2 9 94 8 31 59 -5.66 0.52 2.84 320 2 14 94 14 31 59 -13.1 0.43 2.7 306 2 9 94 11 31 59 -5.81 0.51 2.85 318 2 14 94 17 31 59 -12.9 0.43 2.7 306																		
2 9 94 11 31 59 -5.81 0.51 2.85 318 2 14 94 17 31 59 -12.9 0.43 2.7 306		-		-														
	2	9	94	14	31	59 -6.11	0.51	2.85	318	2	14	94	20	31	59 -13.1	0.43	2.69	307
2 9 94 17 31 59 -6.68 0.51 2.86 317 2 14 94 23 31 59 -13.8 0.43 2.69 308		-																
2 9 94 20 31 59 -7.5 0.51 2.86 315 2 15 94 2 31 59 -14.2 0.43 2.68 309																-		
2 9 94 23 31 59 -8.76 0.51 2.86 315 2 15 94 5 31 59 -14.5 0.43 2.67 309																		
2 10 94 2 31 59 -9.13 0.5 2.87 314 2 15 94 8 31 59 -14.9 0.43 2.67 310		-																
2 10 94 5 31 59 -9.97 0.5 2.87 313 2 15 94 11 31 59 -14.9 0.42 2.66 310																		
2 10 94 8 31 59 -10.7 0.5 2.87 313 2 15 94 14 31 59 -14.6 0.42 2.66 312										2								
2 10 94 11 31 59 -11.2 0.49 2.87 312 2 15 94 17 31 59 -14 0.42 2.65 312										2								
2 10 94 14 31 59 -11.5 0.49 2.87 311 2 15 94 20 31 59 -13.7 0.42 2.65 313																		
2 10 94 17 31 59 -11.9 0.49 2.87 310 2 15 94 23 31 59 -13.8 0.42 2.64 314		-								_								
2 10 94 20 31 59 -12.4 0.48 2.86 309 2 16 94 2 31 59 -14.1 0.42 2.63 316																		

Appendix C
Gambell Observation Well #1

Mm	ρd	Yy	Ħг	Mn	Ss AirT	WaterT	Stage	Conductivity	Mm	Do	ł Yy	Hr	Mn	Ss AirT	WaterT	Stage C	onductivity
2	16	94	5	31	59 -14-4	0.42	2.63	316	2	21	94	11	31	59 -13.2	0.37	2.49	389
5	16	94	8	31	59 -14.7	0.42	2.62	318	2	21		14	31	59 -13.3	0.37	2.48	390
2	16	94	11	31	59 -14.6	0.42	2.62	319	ž	21		17	31	59 -13.1	0.37	2.48	392
2	16	94	14	31	59 -14.6	0.41	2.61	320	ž	21		20	31	59 ~13	0.37	2.48	393
2	16	94	17	31	59 -14.5	0.41	2.61	322	ž	21		23	31	59 -12.9	0.37	2.48	394
2	16	94	20	31	59 -14.5	0.41	2.6	322	2	22		2	31	59 -12.8	0.37	2.48	397
2	16	94	23	31	59 -14.5	0.41	2.6	323	2	22		5	31	59 -12.8	0.36	2.48	397
5	17	94	2	31	59 -14.5	0.41	2.59	325	2	22		8	31	59 -13	0.36	2.47	399
ž	17	94	5	31	59 -14.6	0.41	2.59	327	2	22	94	11	31	59 -13-1	0.36	2.47	401
ž	17	94	8	31	59 ~15.1	0.41	2.58	328	2	22	94	14	31	59 -12.9	0.36	2.47	400
2	17	94	13	31	59 -15.5	0.41	2.58	330	2	22	94	17	31	59 -12.6	0.36	2.47	401
2	17	94	14	31	59 - 15.7	0.4	2.57	331	2	22		20	31	59 -12.4	0.36	2.47	403
Ž	17	94	17	31	59 -15.5	0.4	2.57	333	2	22		23	31	59 -12.2	0.36	2.47	404
2	17	94	SO	31	59 -15.6	0.4	2.56	334	2	23		2	31	59 -12.1	0.35	2.47	405
2	17	94	23	31	59 ~15.8	0.4	2.56	337	2	23		5	31	59 -12.1	0.35	2.47	406
2	18	94	2	31	59 -16	0.4	2.55	338	2	23		8	31	59 ~12	0.35	2.47	407
2	18	94	5	31	59 -16-1	0.4	2.55	340	2	23		11	31	59 -12	0.35	2.47	407
2	18	94	8	31	59 -15.6	0.4	2.55	342	2	53		14	31	59 -11.9	0.35	2.47	410
2	18	94	11	31	59 -15.5	0.4	2.54	343	2	23		17	31	59 -11.8	0.35	2.47	410
2	18	94	14	31	59 -15.4	0.4	2.54	346	2	23		20	31	59 -11.6	0.35	2.46	411
2	18	94	17	31	59 -15	0.39	2.54	347	2	2.3		23	31	59 -11.5	0.35	2.46	412
2	18	94	20	31	59 -14.7	0.39	2.54	348	2	24		Z	31	59 -11.4	0.34	2-46	413 414
2	18	94	23	31	59 -14.4	0.39	2.53	350	2	24		5	31	59 -11.5	0.34 0.34	2.46 2.46	414
2	19	94	2	31	59 -14.2	0.39	2.53	353	2	24		8	31	59 -11.9	0.34	2.46	415
2	19	94	5	31	59 -14	0.39	2.53	355	2	24		11	31 31	59 -12.4 59 -12.8	0.34	2.40	416
2	19	94	8	31	59 -13.7	0.39	2.53	357	2	24		14	31	59 -12.9	0.34	2.45	416
S	19	94	11	31	59 -13.5	0.39	2.52	359	2	24		17 20	31	59 - 12.9	0.34	2.45	417
S	19	94	14	31	59 -13.2	0.39	2.52	361	2	24		23	31	59 -13.2	0.33	2.44	418
2	19	94	17	31	59 ~12.9	0.39	2.52	364 366	2	25		2	31	59 -13.5	0.33	2.44	419
2	19	94	20	31	59 -12.7	0.39	2.52 2.51	369	2	25		5	31	59 -13.5	0.33	2.44	419
2	19	94	23	31	59 -12.5	0.39 0.38		371	2	25		8	31	59 -13.6	0.33	2.44	420
2	20	94	2	31	59 ~12.4 59 ~12.3	0.38	2.51 2.51	373	2	25		11	31	59 -13.7	0.33	2.43	422
2	20	94	5	31 31	59 -12.2	0.38	2.51	374	2	25		14	31	59 -13.5	0.33	2.43	422
2	20	94	8	31	59 -12.2	0.38	2.5	376	2	25		17	31	59 -13.2	0.33	2.43	423
2	20	94 94	11 14	31	59 -12.1	0.38	2.5	377	2	25		20	31	59 -12.9	0.33	2.42	423
2	20 20	94	17	31	59 -12.1	0.38	2.5	380	2	25		23	31	59 -12.8	0.33	2.42	424
2	20	94	20	31	59 -12.1	0.38	2.5	381	2	26		2	31	59 -12.7	0.32	2.42	425
2	20	94	23	31	59 -12.2	0.37	2.49	382	2	26		5	31	59 -12.6	0.32	2.41	426
2	21	94	2	31	59 -12.4	0.37	2.49	384	2	26		8	31	59 -12.6	0.32	2.41	426
2	21	94	5	31	59 -12.4	0.37	2.49	385	2	26		11	31	59 -12.7	0.32	2.41	427
2	21	94	ź.	31	59 -12.8	0.37	2.49	388	2	26		14	31	59 -12-7	0.32	2.4	428

Appendix C
Gambell Observation Well #1

Mm	Ðd	Yу	Нг	Ħn	Ss AirT	Waterĭ	Stage	Conductivity	Man	Dď	Yy	Нг	Яn	Ss AirT	WaterT	Stage (	Conductivity
2	26	94	17	31	59 -12.9	0.32	2.4	429	3	3	94	23	31	59 -21.9	0.26	2.23	448
2	26	94	20	31	59 -13.2	0.32	2.39	430	3	4	94	2	31	59 -21.9	0.26	2.22	447
2	26	94	23	31	59 -13-8	0.31	2.39	431	3	4	94	5	31	59 -21.9	0.26	2.22	447
2	27	94	2	31	59 -14-6	0.31	2.38	433	3	4	94	8	31	59 -21.9	0.26	2.21	447
2	27	94	5	31	59 -15.1	0.31	2.38	432	3	4	94	11	31	59 -21.7	0.26	2.21	446
2	27	94	8	31	59 -15.7	0.31	2.38	434	3	4	94	14	31	59 -21	0.26	2.2	448
2	27	94	11	31	59 -16-4	0.31	2.37	434	3	4	94	17	31	59 ~20.4	0.26	2.2	447
ž	27	94	14	31	59 -16.9	0.31	2.37	434	3	4	94	20	31	59 -20.1	0.26	2.19	449
2	27	94	17	31	59 -17	0.31	2.37	436	3	4	94	23	31	59 -20.2	0.26	2.19	447
2	27	94	20	31	59 - 17.3	0.3	2.36	435	3	5	94	2	31	59 -20.1	0.26	2.18	448
2	27	94	23	31	59 -18	0.3	2.36	436	3	5	94	5	31	59 -20.3	0.26	2.17	446
2	28	94	2	31	59 -18.2	0.3	2.36	439	3	5	94	8	31	59 -21	0.25	2.17	447
2	28	94	5	31	59 -18.7	0.3	2.35	439	3	5	94	11	31	59 -20.8	0.25	2.16	448
2	28	94	8	31	59 -19.4	0.3	2.35	438	3	5	94	14	31	59 -20.3	0.25	2.16	448
2	28	94	11	31	59 -19.7	0.3	2.34	439	3	5	94	17	31	59 -19.8	0.25	2.15	448
2	28	94	14	31	59 -19.5	0.3	2.34	439	3	5	94	20	31	59 -19.6	0.25	2.15	448
2	28	94	17	31	59 - 19.1	0.29	2.34	439	3	5	94	23	31	59 -19.6	0.25	2-14	448
2	28	94	20	31	59 -18.9	0.29	2.33	440	3	6	94	2	31	59 -19.5	0.25	2.14	447
2	28	94	23	31	59 -18-9	0.29	2.33	441	3	6	94	5	31	59 -19.5	0.25	2.13	448
3	1	94	2	31	59 -19	0.29	2.33	442	3	6	94	8	31	59 -19.5	0.25	2.13	448
3	1	94	5	31	59 -19.1	0.29	2.32	441	3	6	94	11	31	59 -19.6	0.25	2.13	448 448
3	1	94	8	31	59 -19.2	0.29	2.32	442	3	6	94	14	31	59 -19.4 59 -19.1	0.25 0.24	2.12 2.12	449
3	1	94	11	31	59 -20	0.29	2.31	443	3	6	94	17	31		0.24	2.12	448
3	1	94	14	31	59 -20.2	0.29	2.31	444	3	6	94	20	31	59 -19 59 -19-1	0.24	2.12	448
3	1	94	17	31	59 -20.2	0.29	2.31	444	3	6 7	94 94	23 2	31 31	59 -19.1	0.24	2.11	449
3	1	94	50	31	59 -20.8	0.28	2.3	445	3 3	7	94	5	31 31	59 - 19.1	0.24	2.11	448
3	1	94	23	31	59 -21	0.28	2.3	446	3	7	94	8	31	59 -19.1	0.24	2.1	450
3	2	94	2	31	59 -21.5	0.28	2.29	447 447	3	7	94	11	31	59 -19	0.24	2.1	449
3	2	94	5	31	59 -21.8	0.28	2.29	448	3	7	94	14	31	59 -18.9	0.24	2.1	452
3	2	94	8	31	59 -22.3	0.28	2.28	448	3	7	94	17	31	59 -18.6	0.24	2.09	452
5	2	94	11	31	59 -22.6	0.28	2.28 2.27	446	3	7	94	20	31	59 -18.4	0.24	2.09	453
3	2	94	14	31	59 -22.7	0.28		447	3	7	94	23	31	59 -18.4	0.24	2.09	453
2	2	94 94	17	31	59 -22.7 59 -23.1	0.28 0.27	2.27	448	3	8	94	2	31	59 -18.6	0.23	2.08	453
3	2		20	31 31			2.26	446	3	8	94	5	31	59 -18.7	0.23	2.08	453
3	2	94 94	23	31	59 -23.3 59 -23.4	0.27 0.27	2.26	447	3	8	94	8	31	59 -18.7	0.23	2.08	454
3	3		2	31	59 -23.4		2.25	447	3	8	94	11	31	59 -18.7	0.23	2.08	454
3	3	94 94	5 8	31	59 -23.4 59 -23.4	0.27 0.27	2.25	447	3	8	94	14	31	59 -18.6	0.23	2.07	455
3	3	94	_	31	59 -23.4 59 -23.1	0.27	2.24	449	3	8	94	17	31	59 -18.4	0.23	2.07	455
3	2		11 14	31	59 -22.6	0.27	2.24	448	3	8	94	20	31	59 -18.3	0.23	2.06	456
3	2	94 94	17	31	59 -22.2	0.27	2.23	447	3	8	94	23	31	59 -18.3	0.23	2.06	456
3	3	94	20	31	59 -22	0.27	2.23	447	3	9	94	2	31	59 -18.3	0.23	2.06	458
4	2	74	20	וכ	37 -22	0.21	د.2	447	,	,	,,	_		27 (0.0		~	

Appendix C
Gambell Observation Well #1

Mm	Dd	Yy	КГ	Mn	Ss AirT	WaterT	Stage	Conductivity	Mm	Dđ	Yy	Нr	Mn	Ss AirT	WaterT	Stage	Conductivity
3	9	94	5	31	59 -18.3	0.23	2.05	458	3	14	94	11	31	59 -17	0.2	1.88	472
3	ó	94	8	31	59 -18.4	0.23	2.05	458	3	14	94	14	31	59 -16.7	0.2	1.88	473
3	ó	94	11	31	59 -18.5	0.23	2.04	458	3	14	94	17	31	59 -16.4	0.2	1.88	474
3	ģ	94	14	31	59 -18.5	0.22	2.04	460	3	14	94	20	31	59 -16.1	0.2	1.88	476
3	ģ	94	17	31	59 -18.3	0.23	2.03	460	3	14	94	23	31	59 -16.1	0.2	1.88	476
3	ý	94	20	31	59 -18.3	0.22	2.03	459	3	15	94	2	31	59 -16	0.2	1.88	477
3	ģ	94	23	31	59 -18.4	0-22	2.03	460	3	15	94	5	31	59 -16	0-2	1.88	478
3	10	94	5	31	59 -18.5	0.22	2.02	460	3	15	94	8	31	59 -16	0.2	1.88	479
3	10	94	5	31	59 -18.7	0.22	2.02	461	3	15	94	11	31	59 -15.9	0.2	1.88	479
3	10	94	8	31	59 -18.8	0.22	2.01	461	3	15	94	14	31	59 -15.7	0.2	1.89	481
3	10	94	11	31	59 -18.9	0.22	2.01	461	3	15	94	17	31	59 -15.4	0.2	1.89	483
3	10	94	14	31	59 -18.8	0.22	2	462	3	15	94	20	31	59 -15.1	0.2	1.89	484
3	10	94	17	31	59 -18.5	0.22	1.99	463	3	15	94	23	31	59 - 15	0.19	1.89	486
3	10	94	20	31	59 -18.4	0.22	1.99	463	3	16	94	2	31	59 -14.8	0.19	1.89	488
3	10	94	23	31	59 -18.4	0.22	1.98	463	3	16	94	5	31	59 -14.7	0.19	1.89	490
3	13	94	2	31	59 -18.6	0.22	1.98	465	3	16	94	8	31	59 -14.7	0.19	1.89	491
3	11	94	5	31	59 -18.7	0.22	1.97	466	3	16	94	11	31	59 -14.6	0.19	1-9	492
3	11	94	8	31	59 -18.9	0.21	1.97	465	3	16	94	14	31	59 -14.5	0.19	1.9	493
3	11	94	11	31	59 -18.9	0.21	1.96	465	3	16	94	17	31	59 -14.3	0.19	3.9	496
3	11	94	14	31	59 -18.7	0.21	1.96	466	3	16	94	20	31	59 -14.2	0.19	1.9	499
3	11	94	17	31	59 -18-3	0.21	1.96	466	3	16	94	23	31	59 -14.1	0.19	1.9	500
3	11	94	50	31	59 -18.5	0.21	1.95	466	3	17	94	2	31	59 -14.1	0.19	1.9	503 503
3	11	94	23	31	59 -19	0.21	1.95	467	3	17	94	5	31	59 -14.2	0.19	1-9	503 507
3	12	94	2	31	59 -19.4	0.21	1.94	467	3	17	94	8	31	59 -14.3	0.19	1.9	510
3	12	94	5	31	59 -19.8	0.21	1.94	467	3	17	94 94	11	31 31	59 -14.3 59 -14.2	0.19 0.19	1.91 1.91	514
3	12	94	8	31	59 -20.2	0.21	1.94	467	3	17		14	-		0.19	1.91	518
3	12	94	11	31	59 -20.4	0.21	1.93	467	3	17 17	94 94	17 20	31 31	59 -14 59 <b>-13.</b> 9	0.18	1.92	521
3	12	94	14	31	59 -20	0.21	1.93	467	3	17	94	23	31	59 -13.8	0.18	1.92	524
3	12	94	17	31	59 -19.4	0.21	1.92	467 468	3	18	94	23	31	59 -13.8	0.18	1.92	529
3	12	94	20	31	59 -19-2	0.21 0.2	1.92	467	3	18	94	5	31	59 -13.8	0.18	1.92	532
3	12	94 94	23	31 31	59 ~19.4 59 -19.4	0.2	1.91 1.91	469	3	18	94	8	31	59 -13.9	0.18	1.93	537
3	13	94	2 5	31	59 - 19.4	0.2	1.9	468	3	18	94	11	31	59 -14.3	0.18	1.93	540
3	13 13	94	8	31 31	59 -19.7	0.2	1.9	468	3	18	94	14	31	59 -14.7	0.18	1.93	543
3	13	94	11	31	59 - 19.8	0.2	1.89	469	3	18	94	17	31	59 -14-8	0.18	1.93	547
3	13	94	14	31	59 -19.2	0.2	1.89	468	3	18	94	20	31	59 -15.4	0.18	1.94	552
3	13	94	17	31	59 -18.5	0.2	1.89	469	3	18	94	23	31	59 -16.3	0.17	1.94	555
3	13	94	20	31	59 -18	0.2	1.89	470	3	19	94	_2	31	59 -17.1	0.17	1.94	560
3	13	94	23	31	59 -17.7	0.2	1.89	469	3	19	94	5	31	59 -16.9	0.17	1.94	562
3	14	94	2	31	59 -17-5	0.2	1.88	470	3	19	94	8	31	59 -17.3	0.17	1.94	566
3	14	94	5	31	59 -17-3	0.2	1.88	470	3	19	94	11	31	59 -17.4	0.17	1.94	570
3	14	94	8	31	59 -17.1	0.2	1.88	471	3	19	94	14	31	59 -17	0.17	1.94	574

Appendix C

Gambell Observation Well #1

Mim	Dd	Υy	Hr	Mn	Ss Airĭ	Waterĭ	Stage	Conductivity	Mm	Dď	۲у	Нг	Mn	\$s AirT	₩aterT	Stage (	Conductivity
3	19	94	17	31	59 -16.6	0.17	1.94	579	3	24	94	23	31	59 -24.3	0.12	1.88	744
3	19	94	20	31	59 -16.6	0.16	1.94	583	3	25	94	2	31	59 -24	0.11	1.88	747
3	19	94	23	31	59 -17-4	0.17	1.94	587	3	25	94	5	31	59 -24.2	0.11	1.88	750
3	20	94	2	31	59 -17.8	0.16	1.94	591	3	25	94	8	31	59 -23.9	0.11	1.87	753
3	20	94	5	31	59 -18.1	0.16	1.94	595	3	25	94	11	31	59 -23.4	0.11	1,87	757
3	20	94	ã	31	59 -18	0.16	1.94	598	3	25	94	14	31	59 -21.8	0.11	1.87	763
3	20	94	11	31	59 -18	0.16	1.93	602	3	25	94	17	31	59 -21.1	0.11	1.87	771
3	20	94	14	31	59 -17.3	0.16	1.93	607	3	25	94	20	31	59 -21.3	0.11	1.87	776
3	20	94	17	31	59 -16.7	0.16	1.93	610	3	25	94	23	31	59 -21	0.11	1.87	778
3	20	94	20	31	59 -16.4	0.16	1.93	613	3	26	94	2	31	59 -20.6	0.11	1.87	782
3	20	94	23	31	59 -16.7	0.15	1.93	617	3	26	94	5	31	59 -20	0.11	1.87	788
3	21	94	5	31	59 -17.6	0.15	1.93	620	3	26	94	8	31	59 -19.5	0.11	1.86	794
3	21	94	5	31	59 -18.3	0.15	1.93	625	3	26	94	11	31	59 -19.2	0.11	1.86	799
3	21	94	8	31	59 -18.5	0.15	1,93	628	3	26	94	14	31	59 -18.8	0.11	1.86	803
3	21	94	11	31	59 - 18.8	0.15	1,92	633	3	26	94	17	31	59 -18.4	0.11	1.86	808
3	21	94	14	31	59 -20.3	0.15	1_93	644	3	26	94	20	31	59 -18.1	0.11	1.87	811
3	21	94	17	31	59 -20.4	0.15	1.93	650	3	26	94	23	31	59 -17.7	0.11	1.87	816
3	21	94	20	31	59 -21.8	0.14	1.93	656	3	27	94	2	31	59 -17.3	0.11	1.87	820
3	21	94	23	31	59 -22.8	0.14	1-92	659	3	27	94	5	31	59 -16.9	0.1	1.87	824
3	22	94	2	31	59 -24	0.14	1.92	662	3	27	94	8	31	59 -16.9	0.1	1.87	828
3	22	94	5	31	59 -24.5	0.14	1.91	665	3	27	94	11	31	59 -16.8	0.1	1.87	831
3	22	94	8	31	59 -25	0.14	1.91	667	3	27	94	14	31	59 -16.8	0.1	1.87	834
3	22	94	11	31	59 -25.4	0.14	1.91	669	3	27	94	17	31	59 -16.7	0.1	1.86	838
3	22	94	14	31	59 -25.3	0.13	1.91	673	3	27	94	20	31	59 -16.8	0.1	1.86	841
3	22	94	17	31	59 -25	0.13	1.91	676	3	27	94	23	31	59 -16-8	0.1	1.87	845
3	22	94	20	31	59 -26	0.13	1.9	680	3	28	94	2	31	59 -16.8	0.1	1.86	847
3	22	94	23	31	59 -26.4	0.13	1.9	684	3	28	94	5	31	59 -16.8	0.1	1.86	851
3	23	94	2	31	59 -26.4	0.13	1.9	687	3	28	94	8	31	59 -16.7	0_1	1.86	854
3	23	94	5	31	59 -26.8	0.13	1.89	689	3	28	94	11	31	59 -16.6	0_1	1.86	858
3	23	94	8	31	59 -27-2	0.13	1.89	691	3	28	94	14	31	59 -16.5	0.1	1.86	862
3	23	94	11	31	59 ~27	0.13	1.89	699	3	28	94	17	31	59 -16.4	0.1	1.86	865
3	23	94	14	31	59 -25.5	0.12	1.89	705	3	28	94	20	31	59 -16.3	0.09	1.86	869
3	23	94	17	31	59 -25	0.12	1.89	710	3	28	94	23	31	59 -16.3	0.09	1.86	872
3	23	94	20	31	59 -25.4	0.12	1.89	712	3	29	94	2	31	59 -16.2	0.09	1.86	875
3	23	94	23	31	59 -26.1	0.12	1.89	716	3	29	94	5	31	59 -16.1	0.09	1.86	878
3	24	94	2	31	59 -26.7	0.12	1.89	720	3	29	94	8	31	59 -16.1	0.09	1.85	882
3	24	94	5	31	59 -26.8	0.12	1.89	722	3	29	94	11	31	59 -16	0.09	1.85	885
3	24	94	8	31	59 -26.7	0.12	1.89	724	3	29	94	14	31	59 -15.7	0.09	1.85	889
3	24	94	11	31	59 -26.3	0.12	1.88	727	3	29	94	17	31	59 -15.4	0.09	1.85	891
3	24	94	14	31	59 -24.9	0.12	1.88	732	3	29	94	50	31	59 -15.3	0,09	1.85	894
3	24	94	17	31	59 -23.9	0.12	1.88	739	3	29	94	23	31	59 -15.2	0.09	1.84	897
3	24	94	20	31	59 -24.1	0.12	1.88	741	3	30	94	2	31	59 -15.1	0.09	1.84	901

Appendix C

# Gambell Observation Well #1

Stage Conductivity	1026	1033	1035	1041	1043	1047	1049	1051	1055	1058	1060	1064	1068	1070	1073	1075	1078	1081	1086	1089	2601	1096	1099	1102	1104	1109	1114	1119	1123	1127	1129	1132	1134	1138	1141	1145	1168	1150	1150	4452	551-
Stage Co	1.86	1.87	1.87	8 8	1.89	1.89	1.89	1.89	1-9	1,9	1.9	1.9	1.91	1.91	1.91	1.91	1.91	1.91	1.91	1.91	1.91	1-91	1.9	1.91	1.91	1.91	1.9	1.91	1.92	1.92	1.92	1.92	1.92	1.92	1.93	1.92	1 0	1 00	26.	26.1	76-1
<b>WaterT</b>	0.05	0.05	0.05	0.0	0,05	0.05	0.04	0.04	0.04	0.0	0.0	0.04	0.04	0.04	0.04	0.04	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.02	0.03	0,02	0.02	0.02	0.02	0.02	0.02	0.02	0.02		20.0		5 6	5.0
Ss AirT	59 -8.51				59 -7.58															59 -8.77																				7, 7, 7, 7, 7, 7, 7, 7, 7, 7, 7, 7, 7, 7	9.0T- 96
Ē	2.5	. <del>.</del> .	31	<u>۲</u> ک	3.5	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31	3	31	31	31	3	31	31	31		5 5	7 5	- -	7;	5
¥	11	<u>.</u>	딣	უ ^	1 V	αo	Ξ	5	۲	ನ	Ŋ	~	2	80	<u></u>	7		20	ສ	2	ľ	ø	=	14	12	2	23	~	'n	æ	=	2	17	2	23	۸ ا	) W	n 6	<b>»</b> :	= :	7.
_ <u>}</u>	7 %	. 75	76	<b>*</b> 8	8	76	76	76										76																						<b>*</b> 7	*
B	4 4	7	4	4 U	· ~	2	2	s	2	S	Ŋ	9	9	φ	9	8	•	9	9	~	_	7	^	7	7	7	~	80	∞	æ	ထ	æ	œ	<b>60</b>	00	0	٠.	> 0	<b>&gt;</b> (	> 0	>
£	4 4	7	7	<b>5</b> 7	4	7	7	7	4	7	4	4	7	4	4	4	7	4	4	7	4	4	4	4	4	4	7	7	4	7	•	7	*	4	7	4	r <	<b>*</b> ~	<b>.</b>	<b>.</b>	4
: Conductivity	903																																								
Stage Conductivity	1.84 903																																								
WaterI Stage Conductivity		<u>.</u> 2	7.8	1.83	3 8	1,83	1.83	1.83	1.83	1.83	1,83	1.83	1.83	1.84	7.8	7.8	1.85	1.85	1.85	1.86	1,86	1.86	1.86	1.86	1.86	1.87	1.87	1.87	.86	1.86	1.86	1.86	1.86	1.86	8	3 2	8 9	8.6	98.	8.	1.86
	8.1.	-15.1 0.08 1.84	-14.9 0.08 1.84	-14.6 0.08 1.83	-14.4 0.08 1.83 -14.3 0.08 1.83	-14,1 0,08 1,83	-13.9 0.08 1.83	-13.5 0.08 1.83	-13.1 0.08 1.83	-12.5 0.08 1.83	-11.9 0.08 1.83	-11,8 0.08 1.83	-11.9 0.08 1.83	-12 0.08 1.84	-12.1 0.08 1.84	-12.1 0.07 1.84	-12.1 0.07 1.85	-12.1 0.07 1.85	-12 0.07 1.85	-11.9 0.07 1.86	-11.8 0.07 1.86	-11.6 0.07 1.86	-11.5 0.07 1.86	-11.3 0.07 1.86	-11.1 0.07 1.86	-10.5 0.07 1.87	-9.98 0.07 1.87	-9.79 0.07 1.87	-9.75 0.06 1.86	~9.66 0.06 1.86	-9.97 0.06 1.86	-10,1 0.06 1.86	-10.1 0.06 1.86	9.99 0.06 1.86	20 50 0 06 1 86	78 1 70 0 67 0	00.1 00.0 24.6	-9.53 U.U6 1.86	-9.16 0.06 1.86	-9 0.06 1.86	~8.84 D.05 1.86
Airī Waterī	-15.1 0.09 1.84	59 -15.1 0.08 1.84	59 - 14.9 0.08 1.84	59 -14.6 0.08 1.83	59 - 14.3 0.08 1.83	59 -14.1 0.08 1.83	59 - 13.9 0.08 1.83	59 - 13.5 0.08 1.83	59 -13.1 0.08 1.83	59 - 12.5 0.08 1.83	59 -11.9 0.08 1.83	59 -11.8 0.08 1.83	59 -11.9 0.08 1.83	59 -12 0.08 1.84	59 -12.1 0.08 1.84	59 -12.1 0.07 1.84	59 - 12.1 0.07 1.85	59 -12.1 0.07 1.85	59 -12 0.07 1.85	59 -11.9 0.07 1.86	59 -11.8 0.07 1.86	59 -11.6 0.07 1.86	59 -11.5 0.07 1.86	59 -11.3 0.07 1.86	59 -11.1 0.07 1.86	59 -10.5 0.07 1.87	59 -9.98 0.07 1.87	59 -9.79 0.07 1.87	59 -9.75 0.06 1.86	59 ~9.66 0.06 1.86	59 -9 -9 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0	59 -10,1 0.06 1.86	59 -10.1 0.06 1.86	59 -9.99 0.06 1.86	20 - 0 50 0 0 0 1 86	78 1 70 0 67 0 05	00.1 00.0 24.4.40	59 -9.33 0.06 1.86	59 -9.16 0.06 1.86	59 -9 0.06 1.86	59 -8.84 0.05 1.86
Ss Airī WaterT	59 -15.1 0.09 1.84	31 59 -15.1 0.08 1.84	31 59 -14.9 0.08 1.84	31 59 - 14.6 0.08 1.83	31 59 14.3 0.08 1.83	31 59 -14.1 0.08 1.83	31 59 - 13.9 0.08 1.83	31 59 13.5 0.08 1.83	31 59 -13.1 0.08 1.83	31 59 -12.5 0.08 1.83	31 59 -11.9 0.08 1.83	31 59 -11.8 0.08 1.83	31 59 -11.9 0.08 1.83	31 59 -12 0.08 1.84	31 59 -12.1 0.08 1.84	31 59 - 12.1 0.07 1.84	31 59 -12.1 0.07 1.85	31 59 -12.1 0.07 1.85	31 59 -12 0.07 1.85	31 59 -11.9 0.07 1.86	31 59 -11.8 0.07 1.86	31 59 -11.6 0.07 1.86	31 59 -11.5 0.07 1.86	31 59 -11.3 0.07 1.86	31 59 -11.1 0.07 1.86	31 59 -10.5 0.07 1.87	31 59 -9.98 0.07 1.87	31 59 -9.79 0.07 1.87	31 59 -9.75 0.06 1.86	31 59 ~9.66 0.06 1.86	31 59 -9 -9 7 0.06 1.86	31 59 -10.1 0.06 1.86	31 59 -10.1 0.06 1.86	31 59 -9.99 0.06 1.86	71 50 0 50 0 186	34 50 0 67 0 68	00.1 00.0 54.77 01.00	51 59 -9.33 0.06 1.86	31 59 -9.16 0.06 1.86	31 59 -9 0.06 1.86	31 59 8.84 0.05 1.86
Mn Ss Airī Waterī	31 59 -15.1 0.09 1.84	11 31 59 -15.1 0.08 1.84	14 31 59 -14.9 0.08 1.84	77 31 59 -14.6 0.08 1.83	23 31 59 14.4 0.08 1.83	2 31 59 -14.1 0.08 1.83	5 31 59 -13.9 0.08 1.83	8 31 59 -13.5 0.08 1.83	11 31 59 -13_1 0.08 1.83	14 31 59 -12.5 0.08 1.83	17 31 59 -11.9 0.08 1.83	20 31 59 -11,8 0.08 1.83	23 31 59 -11.9 0.08 1.83	2 31 59 -12 0.08 1.84	5 31 59 -12.1 0.08 1.84	8 31 59 - 12.1 0.07 1.84	11 31 59 -12.1 0.07 1.85	14 31 59 -12.1 0.07 1.85	1. 3 אין 1.0 12 0.07 1.85	20 31 59 -11.9 0.07 1.86	23 31 59 -11.8 0.07 1.86	2 31 59 -11.6 0.07 1.86	5 31 59 -11.5 0.07 1.86	8 31 59 -11.3 0.07 1.86	11 31 59 -11.1 0.07 1.86	14 31 59 -10.5 0.07 1.87	17 31 59 -9.98 0.07 1.87	20 31 59 -9.79 0.07 1.87	23 31 59 -9.75 0.06 1.86	2 31 59 ~9.66 0.06 1.86	5 31 59 -9.97 0.06 1.86	8 31 59 -10,1 0.06 1.86	11 31 59 -10.1 0.06 1.86	1, 31 59 -9.99 0.06 1.86	1 50 -0 50 1 1 86	24	00'1 00'0 24'6' 6C 1C 02	23 51 59 -9.35 0.06 1.86	2 31 59 -9.16 0.06 1.86	5 31 59 -9 0.06 1.86	8 31 59 8.84 0.05 1.86
Hr Mn Ss Airī Vaterī	5 31 59 -15.1 0.09 1.84	94 1 31 59 -15,1 0.08 1.84	94 14 31 59 -14.9 0.08 1.84	94 17 31 59 -14.6 0.08 1.83	94 20 31 59 14.4 0.08 1.83	94, 2 31 59 -14.1 0.08 1.83	94 5 31 59 -13,9 0.08 1.83	94 8 31 59 13.5 0.08 1.83	94 11 31 59 -13.1 0.08 1.83	94 14 31 59 -12.5 0.08 1.83	94 17 31 59 -11,9 0.08 1,83	94 20 31 59 -11.8 0.08 1.83	94 23 31 59 -11.9 0.08 1.83	94 2 31 59 -12 0.08 1.84	5 31 59 -12.1 0.08 1.84	8 31 59 - 12.1 0.07 1.84	11 31 59 -12.1 0.07 1.85	14 31 59 -12.1 0.07 1.85	1. א	94 20 31 59 -11.9 0.07 1.86	94 23 31 59 -11.8 0.07 1.86	2 31 59 -11.6 0.07 1.86	94 5 31 59 -11.5 0.07 1.86	94 8 31 59 -11.3 0.07 1.86	94 11 31 59 -11.1 0.07 1.86	94 14 31 59 -10.5 0.07 1.87	94 17 31 59 -9.98 0.07 1.87	94 20 31 59 -9.79 0.07 1.87	94 23 31 59 -9.75 0.06 1.86	94 2 31 59 -9.66 0.06 1.86	94 5 31 59 -9 97 0.06 1.86	94 8 31 59 -10.1 0.06 1.86	94, 11 31 59 -10.1 0.06 1.86	98.1 90.0 66.6-65 12 71 76	77 77 76 76 76 76 76 76 76 76 76 76 76 7	2010 C7 O- 02 12 0C 70	00°1 00°0 24°6 60 10 02 %	94, 23, 51, 59, -9.33, 0.06, 1.86	94 2 31 59 -9.16 0.06 1.86	94 5 31 59 -9 0.06 1.86	94 8 31 59 -8.84 0.05 1.86

Appendix C
Gambell Observation Well #1

₩m	Dd	Yy	Hr	Ħn	\$s AirT	WaterT	Stage	Conductivity	Mm	Dd	Yy	Hr	Mn	\$s AirT	₩aterT	\$tage C	onductivity
4	9	94	17	31	59 -10.7	0.01	1,92	1154	4	14	94	23	31	59 -12	-0.01	1.76	1209
4	ģ	94	20	31	59 -10.7	0.01	1.92	1156	4	15		2	31	59 ~12.5	-0.01	1.76	1213
4	ģ	94	23	31	59 -10.8	0.01	1.92	1159	4	15		5	31	59 -13	-0.01	1.76	1216
4	10	94	2	31	59 -10.8	0.01	1.92	1161	4	15		8	31	59 -13.6	-0.01	1.76	1219
4	10	94	5	31	59 -11	0.01	1.91	1163	4	15		11	31	59 -13.4	-0.01	1.76	1220
4	10	94	8	31	59 ~11.2	0.01	1.91	1165	4	15		14	31	59 -12.9	-0.01	1.76	1219
4	10	94	11	31	59 -11-2	0.01	1.91	1167	4	15		17	31	59 -12.5	-0.01	1.76	1219
4	10	94	14	31	59 -10.9	0.01	1.9	1166	4	15	94	20	31	59 -12.6	-0_01	1.76	1221
4	10	94	17	31	59 -10.7	0.01	1.89	1167	4	15	94	23	31	59 -12.8	-0_01	1.75	1222
i.	10	94	20	31	59 -10.6	0.01	1.89	1167	4	16	94	2	31	59 -13.2	-0.01	1.75	1226
4	10	94	23	31	59 -10.6	0	1.89	1169	4	16	94	5	31	59 -13.8	-0.01	1.75	1230
4	11	94	2	31	59 -10-5	O	1.88	1170	4	16	94	8	31	59 -14.2	-0.01	1.75	1235
4	11	94	5	31	59 -10.6	0	1.88	1172	4	16	94	11	31	59 -14.2	-0.01	1.75	1236
4	13	94	8	31	59 -10.7	0	1.87	1174	4	16	94	14	31	59 -13.8	-0.01	1.75	1234
4	11	94	11	31	59 -10.7	0	1.87	1174	4	16		17	31	59 -13.4	-0.02	1.75	1235
4	11	94	14	31	59 -10.5	0	1.87	1174	4	16	94	20	31	59 -13.3	-0.02	1.75	1238
4	11	94	17	31	59 -10.4	0	1.87	1176	4	16		23	31	59 -13.7	-0.02	1.75	1241
4	11	94	\$0	31	59 -10.3	0	1.86	1177	4	17		2	31	59 -14.2	~0.02	1.75	1246
4	11	94	23	31	59 -10.4	0	1.86	1178	4	17		5	31	59 -14.7	-0.02	1.75	1251
4	12	94	2	31	59 -10.8	Đ	1.85	1181	4	17		8	31	59 -14.9	-0.02	1.75	1253
4	12	94	5	31	59 -11.1	0	1.85	1183	4	17		11	31	59 -14.6	-0.02	1.75	1254
4	12	94	8	31	59 -11.5	0	1.84	1188	4	17		14	31	59 -14.1	-0.02	1.75	1256
4	12	94	11	31	59 -11.5	0	1.84	1188	4	17		17	31	59 -13.7	-0.02	1.76	1256
4	32	94	14	31	59 -11.4	0	1.83	1186	4	17		20	31	59 -13.4	-0.02	1.76	1257
4	12	94	17	31	59 -11.3	0	1.83	1189	4	17		23	31	59 -13.6	-0.02	1.76	1261
4	12	94	50	31	59 -11.2	0	1.82	1189	4	18		2	31	59 -14	-0.02	1.76	1265
4	12	94	23	31	59 -11.6	0	1.82	1193	4	18		5	31	59 -14-1	-0.02	1.76	1268 1269
4	13	94	2	31	59 -11.9	-0.01	1.82	1195	4	18		8	31	59 -14.2	-0.02	1.76	
4	13	94	5	31	59 -12.2	0	1.81	1199	4	18		11	31	59 -14.1	-0.02	1.76 1.77	1272 1272
4	13	94	8	31	59 -12-4	0	1.8	1200	4	18		14	31	59 -13.7 59 -13.3	-0.02 -0.02	1.77	1274
4	13	94	11	31	59 -12.2	-0.01	1.8	1199	4	18 18		17 20	31 31	59 -13.3	-0.02	1.77	1277
4	13	94	14	31	59 -11.8	0	1.8	1198	4			23	31	59 -12.9	-0.02	1.77	1279
4	13	94	17	31	59 -11.5	0	1.79	1197	4	18 19		2	31	59 -13.1	-0.02	1.77	1283
- 4	13	94	20	31	59 -11.3	-0.01	1.79	1197	4	19		5	31 31	59 -13.4	-0.02	1.77	1285
4	13	94	23	31	59 -11.3	-0.01	1.79	1199	4	19		8	31	59 -13.4	-0.02	1.77	1286
4	14	94	2	31	59 -11.6	-0.01	1.78	1201 1204	4	19		11	31	59 -13.3	-0.02	1.77	1288
4	14	94	5	31	59 -12	-0.01	1.78	1204	4	19		14	31	59 -12.9	-0.02	1.77	1289
4	14	94	8	31	59 -12.3	-0.01	1.78		4	19		17	31	59 -12.5	-0.02	1.77	1290
4	14	94	11	31	59 -12.3	-0.01	1.77 1.77	1207 <b>1</b> 206	4	19		20	31	59 -12.2	-0.03	1.77	1291
4	14	94	14	31 31	59 -12 59 -11.7	-0.01	1,77	1205	4	19		23	31	59 -12.1	-0.03	1.77	1292
4	14	94	17 20	31 31	59 -11.7 59 -11.6	-0.01 -0.01	1.76	1205	4	20		2	31	59 -12.2	-0.03	1.77	1295
4	14	94	20	31	3A - 11'0	-0.01	1.70	1203	•	2.0	,-	6-	31	27 14.6	0.03		

Appendix C
Gambell Observation Well #1

Mm	Dd	Υу	Ħг	Kn	Ss Airī	WaterT	Stage	Conductivity	Mm	Dc	ł Yy	Нг	Mn	Ss AirT	WaterT	Stage	Conductivity
4	20	94	5	31	59 -12.4	-0.03	1.77	1297	4	25	94	11	31	59 -10.2	-0.04	1.71	1344
4	20	94	8	31	59 -12.5	-0.03	1.77	1300	Ž	25		14	31	59 -9.87	-0.04	1,71	1346
4	20	94	11	31	59 -12.4	-0.03	1.77	1301	4	25		17	31	59 -9.55	-0.04	1.71	1349
4	20	94	14	31	59 -12.1	-0.03	1.76	1301	Ž	25		20	31	59 -9-26	-0.04	1,71	1349
7	20	94	17	31	59 -11.8	-0.03	1.76	1303	7	25		23	31	59 -9-24	-0.04	1.71	1351
4	20	94	20	31	59 -11.5	-0.03	1.76	1303	Ž	26		2	31	59 -9.41	-0.04	1.71	1352
4	20	94	23	31	59 -11.4	~0.03	1.75	1304	4	26		5	31	59 -9.56	-0.04	1.71	1355
7	21	94	ž	31	59 -11.6	-0.03	1,75	1307	4	26		8	31	59 -9.61	-0.04	1.71	1357
4	21	94	5	31	59 -11.8	-0.03	1.75	1310	į.	26		11	31	59 -9-45	-0.04	1.71	1358
4	21	94	8	31	59 -12	-0.03	1.75	1310	4	26		14	31	59 -9-15	-0.04	1.71	1359
4	21	94	11	31	59 -11.8	-0.03	1.75	1311	4	26		17	31	59 -8.82	-0.04	1.71	1360
4	21	94	14	31	59 -11.5	-0.03	1.74	1311	4	26		20	31	59 -8.55	-0.04	1.71	1362
4	21	94	17	31	59 -11.1	-0.03	1,74	1311	4	26		23	31	59 ~8.46	-0.04	1.71	1363
4	21	94	20	31	59 -10-7	-0.03	1.74	1312	4	27		-2	31	59 -8.47	-0.04	1.71	1364
4	21	94	23	31	59 -10-8	-0.03	1.74	1314	4	27		5	31	59 -8.49	-0.04	1.71	1366
4	22	94	2	31	59 -11-1	-0.03	1.74	1316	4	27		8	31	59 -8.52	~0.05	1.71	1367
4	22	94	5	31	59 -11-6	-0.03	1.74	1319	4	27		11	31	59 -8.43	~0.04	1.71	1368
4	22	94	8	31	59 -11.8	-0.03	1.74	1321	4	27		14	31	59 -8.26	-0.04	1.71	1370
4	22	94	11	31	59 -11.5	-0.03	1.74	1322	4	27	94	17	31	59 -7.98	-0.05	1.7	1372
4	22	94	14	31	59 -11-1	-0.03	1.73	1321	4	27	94	20	31	59 -7.74	~0.05	1.7	1373
4	22	94	17	31	59 -10.7	-0.03	1.73	1320	4	27		23	31	59 -7.74	-0.04	1.7	1375
4	22	94	20	31	59 -10.5	-0.03	1.73	1320	4	28	94	2	31	59 -7.81	~0.05	1.7	1375
4	22	94	23	31	59 -10.7	-0.03	1.73	1322	4	28	94	5	31	59 -7.98	-0.05	1.7	1376
4	23	94	S	31	59 -11.1	-0.04	1.73	1325	4	28	94	8	31	59 -8.08	-0.05	1.69	1378
4	23	94	5	31	59 -11.4	~0.03	1.72	1326	4	28		11	31	59 ~8.03	-0.05	1.69	1378
4	23	94	8	31	59 -11.5	-0.03	1.72	1329	4	28		14	31	59 ~7.87	-0.05	1.69	1379
4	23	94	11	31	59 -11.2	-0.03	1.72	1327	4	28		17	31	59 -7.57	-0.05	1.69	1380
4	23	94	14	31	59 -10.9	-0.04	1.72	1328	4	28		20	31	59 ~7.3	-0.05	1.69	1381
4	23	94	17	31	59 ~10.6	-0.03	1.72	1329	4	28		23	31	59 -7.05	-0.05	1.68	1383
4	23	94	20	31	59 -10.3	-0.04	1.72	1329	4	29	94	2	31	59 -7.04	-0.05	1.68	1384
4	23	94	23	31	59 -10.5	-0.04	1.72	1332	4	29		5	31	59 -6.92	-0.05	1.68	1384
4	24	94	2	31	59 ~10.7	-0.04	1.71	1333	4	29		8	31	59 -6.86	-0.05	1.68	1385
4	24	94	5	31	59 -10.6	-0.04	1.71	1335	4	29		11	31	59 -6.62	-0.05	1.68	1387
4	24	94	8	31	59 -10.8	-0.04	1.71	1336	4	29		14	31	59 -6.03	-0.05	1.68	1389
4	24	94	11	31	59 ~10.6	-0.04	1.71	1335	4	29		17	31	59 -5.89	-0.05	1.68	1390
4	24	94	14	31	59 -10.3	-0.04	1.71	1336	4	29		20	31	59 -5.63	-0.05	1.68	1392
4	24	94	17	31	59 -9.98	-0.04	1.71	1337	4	29		23	31	59 -5.84	-0.05	1.68	1394
4	24	94	20	31	59 -9.7	-0.04	1.71	1338	4	30		2	31	59 -6.16	-0.05	1.68	1396
4	24	94	23	31	59 -9.64	-0.04	1.71	1338	4	30		5	31	59 -6-45	-0.05	1.68	1398
4	25	94	2	31	59 -9.85	-0.04	1.71	1340	4	30		8	31	59 -6.63	-0.05	1.68	1399
4	25	94	5	31	59 -10.2	-0.04	1.71	1343	4	30		11	31	59 -6.57	-0.05	1.68	1400
4	25	94	8	31	59 -10.3	-0-04	1.71	1345	4	30	94	14	31	59 -6.39	<b>~0.05</b>	1.68	1402

Appendix C

Gambell Observation Well #1

ductivíty		1516	1518	1520	1523	1524	1525	1528	1530	1533	1536	1538	1539	1539	1541	1541	1542	1545	1547	1548	1548	1548	1550	1552	1552	1554	1555	1557	1558	1556	1556	1557	1557	1557	1560	1563	1563	1563	1562	1562	1563	1566	1568	
Stage Conductivíty		1.85	1.85	1.86	1.86	1.87	1.87	1.88	1.88	1.89	1.89	1.9	1.91	1.91	1.91	1.92	1.92	1.93	1.93	1.93	1.93	1.93	1.94	1-94	1.94	1.94	7.6	1.94	1.94	1.93	1.93	1.92	1.92	1.92	1.92	1.92	3.5	1.92	1.92	1.93	1.94	1.96	1.94	
WaterT		,0.05	-0.0	-0.05	-0.05	-0.05	-0.05	-0.05	-0-05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	.0.05	-0-05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	,0°05	-0.05	-0.05	-0.05	-0.05	
Ss AirT		59 -3.22																			59 -3.61						59 -3.15					59 -2.45											59 -3.19	
듷		31	31	3	31	31	31	31	31	31	33	33	31	2	31	31	31	31	31	31	31	31	31	31	ر ا	ž,	31	31	<u>.</u>	31	31	31	31	31	¥1	۲	3	31	31	31	3	. F	. 5	
. <del>.</del> ±		23	2	Ŋ	æ	_	7	7	0	ŭ	7	S	æ	<del>-</del>	7	_	0.	ŭ	2	2	83	_	•	<b>~</b>	ည္ ၊	<b>.</b>	~	Š	<b>~</b>	_	<u> </u>	7	0.	EJ.	~	ᅜ	ø	_	7	7	. و	, M	~ ر	,
γ,		2 %																																										
þ		Ŋ.	9	9	9	9	9	9	9	9	~	~	~	~	~	<u>~</u>	~	^	ø	œ	80	80	80	80	∞	ω	0	0	0	0	0	0	0		2								2 =	
Ē		Δ.	Ŋ	ı۸	Ŋ	v	Ŋ	Ŋ	S	2	v	S	S	5	S	Δ.	S	S	Ŋ	Ŋ	Ŋ	Ŋ	<b>∨</b>	ıΛ I	<b>1</b>	L.	2	2	ν.	Δ.	S	S	2	S	<b>∨</b>	Ŋ	s	S	~	~	ľ	٠ ١	ı v	ı
Conductivity	•	1404	1406	1410	1411	1414	1417	1418	1422	1426	1429	1434	1436	1439	1442	1445	1447	1452	1455	1458	1461	1787	1466	1470	1474	1476	1479	1483	1485	1488	1489	1492	1495	1500	1502	1503	1506	1507	1508	1508	1510	1512	1515	1
Stage Conductivity		1.69 1404	_	_							•	•	•	•				_			1.78 1461	_		_	•				•	•	•	•	•			_						•	1.85 1515	
Water Stage Conductivity		•	1.69	1.69	1.7	1.7	1.7	1.71	1.71	1,72	1.72	1.72	2.7	1.74	1.74	۲. ۲.	۲. ۲	1.76	1.77	1.7	1.78	1.78	1.73	1.79	1.79	1.8	1.8	1.8	1.81	1.81	1.81	1.82	1.82	1.82	1.83	1.83	1.83	1.83	78	78.	2 2			}
		-6.25 -0.05 1.69 1	~6.34 ~0.0 <del>5</del> 1.69 1	-6,57 -0.05 1.69 1	-6.69 -0.05 1.7	-6.8 -0.05 1.7	-6-79 -0.05 1.7	-6.56 -0.05 1.71	-6.34 -0.05 1.71	-6.17 -0.05 1.72	-6.14 -0.05 1.72	-6.38 -0.05 1.72	-6.45 -0.05 1.73	-6.53 -0.05 1.74	.6.56 .0.05 1.74	-6.48 -0.05 1.75	-6.29 -0.05 1.75 1	-6.13 -0.05 1.76 1	-6.03 -0.05 1.77 1	-5.97 -0.05 1.77	-6.06 -0.05 1.78	-6.09 -0.05 1.78	-6.07 -0.05 1.79	-5.96 -0.05 1.79	~5.75 ~0.05 1.79 1	-5.45 -0.05 1.8	-5.09 -0.05 1.8	-4.83 -0.05 1.8	-4.83 -0.05 1.81	-4.93 -0.05 1.81	-4.84 -0.05 1.81	-4.72 -0.05 1.82	-4.31 -0.05 1.82	-3.71 -0.05 1.82	-3.42 -0.05 1.83	·3.52 ·0.05 1.83	-3.6 -0.05 1.83	-3.8 -0.05 1.83	-3.9 -0.05 1.84	78 1 50 0- 58 2-	75. 70. 87.5	7 7 7 7 7 27		
Airl WaterT		59 -6.25 -0.05 1.69	59 -6.34 -0.05 1.69 1	59 -6.57 -0.05 1.69 1	59 -6.69 -0.05 1.7	59 -6.8 -0.05 1.7	59 -6.79 -0.05 1.7	59 -6.56 -0.05 1.71	59 -6.34 -0.05 1.71	59 -6.17 -0.05 1.72	59 -6.14 -0.05 1.72	59 -6.38 -0.05 1.72	59 -6.45 -0.05 1.73	59 -6.53 -0.05 1.74	59 -6.56 -0.05 1.74	59 -6.48 -0.05 1.75	59 -6.29 -0.05 1.75 1	59 -6.13 -0.05 1.76	59 -6.03 -0.05 1.77	59 -5.97 -0.05 1.77	59 -6.06 -0.05 1.78	59 -6.09 -0.05 1.78	59 -6.07 -0.05 1.79	59 -5.96 -0.05 1.79	59 ~5.75 ~0.05 1.79	59 -5.45 -0.05 1.8	59 -5.09 -0.05 1.8	59 -4.83 -0.05 1.8	59 -4.83 -0.05 1.81	59 -4.93 -0.05 1.81	59 -4.84 -0.05 1.81	59 -4.72 -0.05 1.82	59 -4.31 -0.05 1.82	59 -3.71 -0.05 1.82	59 -3.42 -0.05 1.83	59 -3.52 -0.05 1.83	59 -3.6 -0.05 1.83	59 -3.8 -0.05 1.83	78 -1 -0 -0 -2 - 65	78 1 50 0- 58 2- 65	78 1 50 0. 87 5. 05	20 - 2 / 2 - 0 7 1 85	24.5 -0.05 1.85	70.0
Ss AirT WaterT		31 59 -6.25 -0.05 1.69 1	31 59 6.34 -0.05 1.69 1	31 59 -6,57 -0.05 1.69 1	31 59 -6.69 -0.05 1.7	31 59 -6.8 -0.05 1.7	31 59 -6.79 -0.05 1.7	31 59 -6.56 -0.05 1.71	31 59 -6.34 -0.05 1.71	31 59 -6.17 -0.05 1.72	31 59 -6.14 -0.05 1.72	31 59 -6.38 -0.05 1.72	31 59 -6.45 -0.05 1.73	31 59 -6.53 -0.05 1.74	31 59 6.56 0.05 1.74	31 59 -6.48 -0.05 1.75	31 59 -6.29 -0.05 1.75	31 59 -6.13 -0.05 1.76 1	31 59 -6.03 -0.05 1.77	31 59 -5.97 -0.05 1.77	31 59 -6.06 -0.05 1.78	31 59 -6.09 -0.05 1.78	31 59 -6.07 -0.05 1.79	31 59 -5.96 -0.05 1.79	31 59 -5.75 -0.05 1.79 1	31 59 -5.45 -0.05 1.8	31 59 -5.09 -0.05 1.8	31 59 -4.83 -0.05 1.8	31 59 -4.83 -0.05 1.81	31 59 -4.93 -0.05 1.81	31 59 -4.84 -0.05 1.81	31 59 -4.72 -0.05 1.82	31 59 -4.31 -0.05 1.82	31 59 -3.71 -0.05 1.82	31 59 -3.42 -0.05 1.83	31 59 -3.52 -0.05 1.83	31 59 -3.6 -0.05 1.83	31 59 -3.8 -0.05 1.83	21 59 -3.9 -0.05 1.84	78 1 50 0 58 2 65 12	73 1 20 0 27 27 184	20 1 20 0 77 2- 03 12	20.0 0.0 0.5 1.85	2017
Mn Ss AirT WaterT		17 31 59 -6.25 -0.05 1.69 1	20 31 59 -6.34 -0.05 1.69 1	23 31 59 -6,57 -0.05 1.69 1	2 31 59 -6.69 -0.05 1.7	5 31 59 -6.8 -0.05 1.7	8 31 59 -6.79 -0.05 1.7	11 31 59 -6.56 -0.05 1.71	14 31 59 -6.34 -0.05 1.71	17 31 59 -6.17 -0.05 1.72	20 31 59 -6.14 -0.05 1.72	23 31 59 -6.38 -0.05 1.72	2 31 59 -6.45 -0.05 1.73	5 31 59 -6.53 -0.05 1.74	8 31 59 -6.56 -0.05 1.74	11 31 59 -6.48 -0.05 1.75	14 31 59 -6.29 -0.05 1.75 1	17 31 59 -6.13 -0.05 1.76	20 31 59 -6.03 -0.05 1.77	23 31 59 -5.97 -0.05 1.77	2 31 59 -6.06 -0.05 1.78	5 31 59 -6.09 -0.05 1.78	8 31 59 -6.07 -0.05 1.79	11 31 59 -5.96 -0.05 1.79	14 31 59 -5.75 -0.05 1.79	17 31 59 -5.45 -0.05 1.8	20 31 59-5.09 -0.05 1.8 1	23 31 59 -4.83 -0.05 1.8	2 31 59 -4.83 -0.05 1.81	5 31 59 -4.93 -0.05 1.81	8 31 59 -4.84 -0.05 1.81	11 31 59 -4.72 -0.05 1.82	14 31 59 -4.31 -0.05 1.82	77 31 59 -3.71 -0.05 1.82	20 31 59 -3.42 -0.05 1.83	23 31 59 -3.52 -0.05 1.83	2 31 59 -3.6 -0.05 1.83	5 31 59 -3.8 -0.05 1.83	8 71 50 -0 0 1.84	78 1 50 0- 58 2- 65 12 14	1, 21 50 0. 84 5. 02 15 11	28 1 20 0 77 2- 03 12 24		50.0
Hr Mn Ss AirT WaterT		94 17 31 59 -6.25 -0.05 1.69 1	20 31 59 -6.34 -0.05 1.69 1	94 23 31 59 -6.57 -0.05 1.69 1	94 2 31 59 -6.69 -0.05 1.7	7.1 50.0- 8.9 -6.8 5.75	8 31 59 -6.79 -0.05 1.7	11 31 59 -6.56 -0.05 1.71	14 31 59 -6.34 -0.05 1.71	17 31 59 -6.17 -0.05 1.72	20 31 59 -6.14 -0.05 1.72	94 23 31 59 -6.38 -0.05 1.72	94 2 31 59 6.45 -0.05 1.73		94 8 31 59 6.56 0.05 1.74	94 11 31 59 -6.48 -0.05 1.75	94 14 31 59 -6.29 -0.05 1.75 1	94 17 31 59 -6.13 -0.05 1.76	94 20 31 59 -6.03 -0.05 1.77	7.1 595.97 -0.05 1.77	94 2 31 59 -6.06 -0.05 1.78	94 5 31 59 -6.09 -0.05 1.78	94 8 31 59 -6.07 -0.05 1.79	94 11 31 59 -5.96 -0.05 1.79	94 14 31 59 -5.75 -0.05 1.79 1	94 17 31 59 -5.45 -0.05 1.8	94 20 31 59 -5.09 -0.05 1.8 1	94 23 31 59 -4.83 -0.05 1.8	94 2 31 59 -4.83 -0.05 1.81 1	94 5 31 59 -4.93 -0.05 1.81	94 8 31 59 -4.84 -0.05 1.81	94 11 31 59 -4.72 -0.05 1.82	94 14 31 59 -4.31 -0.05 1.82	94 17 31 59 -3.71 -0.05 1.82	94 20 31 59 -3.42 -0.05 1.83	94 23 31 59 3.52 0.05 1.83	94 2 31 59 -3.6 -0.05 1.83	94 5 31 59 -3.8 -0.05 1.83	78 1 20 -0 -0 -0 -0 -0 -0 -0 -0 -0 -0 -0 -0 -0	78 1 50 0- 58 2- 05 12 11 70	7 1 20 0 80 2 05 12 70 70	70 1 20 0 77 2 03 12 21 10	20 2 20 0 0 18 00	70. 70. 70. 70. 70. 70. 70. 70. 70. 70.

Appendix C
Gambell Observation Well #1

Mm	Ðd	Yy	Hr	Mn	Ss AirT	₩aterĭ	Stage	Conductivity	Mm	Do	ł Yy	Hr	Mn	Ss AirT	₩aterT	Stage (	Conductivity
5	11	94	s	31	59 -3.21	-0.05	1.94	1569	s	16	94	11	31	59 -0.59	-0.06	2.01	1612
ś	11	94	á	31	59 -3.15	-0.05	1.95	1568	5	16		14	31	59 -0.39	-0.05	2.01	1605
5	11	94	11	31	59 -3	-0.05	1.95	1569	5	16		17	31	59 -0.34	-0.06	2-02	1602
5	11	94	14	31	59 -2.82	-0.05	1.95	1569	5	16		20	31	59 -0.5	-0.06	2.03	1602
5	11	94	17	31	59 -2.63	-0.05	1.95	1570	5	16		23	31	59 -0.94	-0.06	2.04	1609
5	11	94	20	31	59 -2.64	-0.05	1.95	1570	5	17		Z	31	59 -1.38	-0.06	2.05	1614
ś	11	94	23	31	59 -2.7	-0.05	1.95	1572	5	17		5	31	59 -1.59	-0-06	2.05	1616
5	12	94	2	31	59 -2.8	-0.06	1.94	1574	5	17		8	31	59 -1.48	-0.06	2.06	1619
5	12	94	5	31	59 -2.88	-0.05	1.94	1577	5	17		11	31	59 -1.03	-0.06	2.07	1618
5	12	94	8	31	59 -2.89	-0.05	1.94	1577	5	17		14	31	59 -0.67	-0.06	2.07	1611
ś	12	94	11	31	59 -2.5	-0.05	1.94	1576	5	17		17	31	59 -0.71	-0.06	2,08	1609
5	12	94	14	31	59 -2.49	-0.05	1.94	1578	5	17	7 94	20	31	59 -0.95	-0.06	2.09	1609
5	12	94	17	31	59 -1.99	-0.05	1.94	1579	5	17	7 94	23	31	59 -1.17	-0.06	2.09	1613
ŝ	12	94	20	31	59 -1.74	-0.06	1.95	1578	5	18	3 94	2	31	59 -1,26	-0.06	2.09	1614
5	12	94	23	31	59 -1-94	-0.05	1.94	1579	5	18		5	31	59 -1.2	-0.06	2.09	1616
5	13	94	2	31	59 -2.22	-0.05	1.93	1580	5	18	3 94	8	31	59 -1.08	-0.06	2.1	1616
5	13	94	5	31	59 -2.39	-0.05	1.92	1582	5	18	3 94	11	31	59 -0.89	-0.06	2.1	1615
5	13	94	8	31	59 -2-41	-0.05	1.92	1584	5	18	3 94	14	31	59 -0.56	-0.06	2.11	1612
5	13	94	11	31	59 -2.09	-0.05	1.92	1585	5	18	94	17	31	59 -0.47	-0.06	2.11	1610
5	13	94	14	31	59 -1.67	-0.05	1.93	1585	5	18	94	20	31	59 -0.43	-0.06	2.12	1612
5	13	94	17	31	59 -1.49	-0.05	1.93	1584	5	18	94	23	31	59 -0.44	-0.06	2.13	1612
5	13	94	20	31	59 -1-64	-0.05	1,94	1585	5	- 19	94	2	31	59 -0.46	~0_05	2.14	1615
5	13	94	23	31	59 ~1.87	~0.06	1.94	1586	5	- 19	94	5	31	59 -0.49	-0.06	2.15	1616
5	14	94	2	31	59 -1.94	-0.05	1.94	1589	5	19		8	31	59 -0.47	-0.06	2.16	1619
5	14	94	5	31	59 -1.92	-0.05	1.94	1590	5	19	94	11	31	59 -0.38	-0.06	2.17	1618
5	14	94	8	31	59 -1.86	-0.05	1.94	1591	5	19		14	31	59 -0,29	-0.05	2.19	1618
5	14	94	11	31	59 -1.66	-0.05	1.94	1591	5	19		17	31	59 -0.24	-0.05	2.21	1624
5	14	94	14	31	59 -1.18	-0.06	1.94	1592	5	15		20	31	59 -0.2	-0.05	2.24	1616
5	14	94	17	31	59 -0.73	-0.06	1.95	1592	5	15		23	31	59 -0.26	-0.05	2.29	1611
5	14	94	20	31	59 -0.53	-0.06	1.96	1595	5	20		2	31	59 -0.33	-0.05	2.33	1603
5	14	94	23	31	59 -0.56	~0 <sub>-</sub> 06	1.96	1597	5	20		5	31	59 -0.38	-0.05	2.36	1598
5	15	94	2	31	59 -1.04	-0.06	1.96	1603	5	20		8	31	59 -0.34	-0.05	2.38	1593
5	15	94	5	31	59 -1.51	-0.06	1.96	1605	5	20		11	31	59 -0.27	-0.05	2.4	1585
5	15	94	8	31	59 -1.34	-0.06	1.96	1606	5	20		14	31	59 -0.15	-0.05	2-43	1584
5	15	94	11	31	59 -0.61	-0.06	1.97	1605	5	20		17	31	59 -0.07	-0.05	2.47	1584
5	15	94	14	31	59 -0.41	-0.06	1.97	1598	5	20		20	31	59 -0.04	-0.05	2.53	1581
5	15	94	17	31	59 -0.37	-0.06	1.98	1597	5	20		23	31	59 -0.08	-0.05	2.61	1578 1578
5	15	94	20	31	59 -0.44	-0.06	1.98	1599	5	21		2	31	59 -0.18	-0.05	2.67	1579
5	15	94	23	31	59 -0.59	-0.06	1.99	1602	5	21		5	31	59 -0.27	-0.05	2.72	
5	16	94	2	31	59 -0.78	-0.06	1.99	1609	5	21		.8	31	59 -0.22	~0.05	2.76	1578 1576
5	16	94	5	31	59 -0.93	-0.06	2	1611	5	21		11	31	59 -0.06	-0.05	2.79	1578
5	16	94	8	31	59 -0.86	-0.06	2	1613	5	2'	94	14	31	59 0.12	-0.05	2.82	1370

Appendix C
Gambell Observation Well #1

Mm	Вd	Yy	Яг	Mn	\$s AirT	WaterT	Stage	Conductivity	<b>М</b> т	Dd	Υу	Br	Mn	Ss Airt	WaterT	Stage	Conductivity
5	21	94	17	31	59 0.18	-0.05	2.85	1583	5	26	94	23	31	59 -0.37	-0.06	3.22	1558
<b>5</b>	21	94	20	31	59 0.13	-0.05	2.92	1576	5	27	94	2	31	59 -0.58	-0.06	3.24	1560
ŝ	21	94	23	31	59 -0.1	-0.05	3.01	1572	5	27	94	5	31	59 -0.56	-0.06	3.24	1560
ź	22	94	2	31	59 -0.23	-0.05	3.08	1572	Ś	27	94	8	31	59 -0.49	-0.06	3.24	1560
5	52	94	5	31	59 -0.27	-0-05	3.13	1572	5	27	94	11	31	59 -0.02	-0.06	3.24	1561
5	22	94	8	31	59 -0.2	-0.05	3.16	1569	5	27	94	14	31	59 0.63	-0.06	3.24	1569
5	22	94	11	31	59 -0.01	~0.05	3.19	1583	Ś	27	94	17	31	59 0.61	-0.06	3.27	1562
s s	55	94	14	31	59 0.03	-0.05	3.21	1582	5	27	94	20	31	59 0.38	-0.05	3.3	1559
5	22	94	17	31	59 -0.1	-0.05	3.22	1579	5	27	94	23	31	59 0.06	-0.06	3.33	1557
5	22	94	20	31	59 -0.23	-0.05	3.24	1580	5	28	94	2	31	59 -0.24	-0.05	3.35	1554
5	22	94	23	31	59 -0.46	-0.05	3,26	1577	5	28	94	5	31	59 -0.38	-0.05	3.37	1553
s s	23	94	2	31	59 -0.65	-0.05	3.26	1572	5	28	94	8	31	59 -0.23	-0-06	3.37	1549
5	23	94	5	31	59 -0.79	-0.05	3.27	1569	5	28	94	11	31	59 0.25	-0.05	3.38	1552
5	23	94	8	31	59 -0.75	~0.05	3.27	1571	5	28	94	14	31	59 0.7	-0.05	3.39	1543
5	23	94	11	31	59 -0.54	-0.05	3.26	1571	5	28	94	17	31	59 0.99	-0.05	3.42	1519
5	23	94	14	31	59 -0.21	-0.05	3.26	1568	5	28	94	20	31	59 1.07	-0.06	3.48	1498
5	23	94	17	31	59 -0.16	-0.05	3.26	1566	5	28	94	23	31	59 0.8	-0.05	3.57	1469
5	23	94	20	31	59 -0.39	-0.05	3.26	1565	5	29	94	2	31	59 -0.33	-0.06	3,63	1381
5	23	94	23	31	59 ~0.6	-0.05	3.25	1562	5	29	94	5	31	59 -0.46	-0.06	3.67	1319
5	24	94	2	31	59 -0-82	-0.05	3,25	1564	5	29	94	8	31	59 -0.36	-0.07	3.7	1269
5	24	94	5	31	59 -0.91	-0.05	3.24	1566	5	29	94	11	31	59 0.09	-0.07	3.72	1196
5	24	94	8	31	59 ~0.89	-0.05	3.23	1566	5	29	94	14	31	59 0.52	-0-07	3.73	1118
5	24	94	11	31	59 -0.63	-0.05	3.22	156\$	5	29	94	17	31	59 0-67	-0.07	3.75	1095
5	24	94	14	31	59 -0.2	-0.05	3.21	1565	5	29	94	20	31	59 0.4	-0.07	3.77	1082
5	24	94	17	31	59 -0-02	-0.06	3.21	1564	5	29	94	23	31	59 ~0.21	-0.07	3.79	1074
5	24	94	20	31	59 -0.32	-0.05	3.2	1561	5	30	94	2	31	59 -0.55	~0.07	3.81	1059
5	24	94	23	31	59 -0.78	-0.06	3.19	1563	5	30	94	5	31	59 -0.7	-0_08	3.82	1045
5	25	94	2	31	59 -1.05	-0.06	3.19	1567	5	30	94	8	31	59 -0.57	-0.08	3.83	1032
5	25	94	5	31	59 -1.16	-0.06	3.18	1568	5	30	94	11	31	59 -0.31	-0.08	3.83	1018
5	25	94	8	31	59 -0.98	-0.06	3.18	1570	5	30	94	14	31	59 -0.04	-0.08	3.83	1011
5	25	94	11	31	59 -0.55	-0.06	3.17	1568	5	30	94	17	31	59 0.03	-0.08	3.83	1003
5	25	94	14	31	59 0.01	-0.06	3.16	1572	5	30	94	20	31	59 -0.28	-0.08	3.82	996
5	25	94	17	31	59 0.21	-0.06	3.16	1571	5	30	94	23	31	59 -0.67	-0.08	3.82	986
5	25	94	20	31	59 0.22	-0.06	3.17	1565	5	31	94	2	31	59 -0.73	-0.08	3.81	981
5	25	94	23	31	59 -0.2	-0.06	3.18	1562	5	31	94	5	31	59 -0.67	-0.08	3.8	974
5	26	94	2	31	59 -0.56	-0.06	3.19	1560	5	31	94	8	31	59 -0.47	-0.08	3.79	970
5	26	94	5	31	59 -0.62	-0.06	3.19	1561	5	31	94	11	31	59 -0.2	-0.08	3.78	964
5	26	94	8	31	59 -0.49	-0.06	3.2	1562	5	31	94	14	31	59 0.06	-0.08	3.77	962
5	26	94	11	31	59 -0.02	-0.06	3.19	1567	5	31	94	17	31	59 0.44	-0.08	3.77	962
5	26	94	14	31	59 0.34	-0.06	3.19	1567	>	31	94	20	31	59 0.73	-0.08	3.79	961 968
5	26	94	17	31	59 0,34	-0.06	3.2	1564	?	31	94	53	31	59 0.48	-0.08	3.83	948 944
5	26	94	20	31	59 -0.1	-0.06	3.21	1561	6	1	94	2	31	59 0.06	-0.08	3.84	744

Appendix C
Gambell Observation Well #1

Mm	Dd	Υv	Hr	Mn	Ss AirT	WaterT	Stage	Conductivity	₩m	Ðd	Υy	Нr	Mn	Ss AirT	WaterT	Stage Conductivity
		,					-	•								
6	1	94	5	31	59 -0.23	-0.08	3.84	938								
6	1	94	8	31	59 -0.29	-0.08	3.85	929								
6	1	94	11	31	59 -0.02	-0.08	3.85	922								
6	1	94	14	31	59 0.5	-0.08	3.85	928								
6	1	94	17	31	59 1.11	-0.08	3.87	939								
6	1	94	20	31	59 1.15	-0.08	3.89	944								
6	1	94	23	31	59 0.68	-0.08	3.93	951								
6	2	94	2	31	59 0.08	-0.08	3.97	956								
6	2	94	5	31	59 -0.06	-0.08	3.99	950								
6	2	94	8	31	59 0.07	-0.08	4	939								

Appendix D

Gambell Observation Well #2

Mm	۵d	Υу	Hr	Mrs	Ss AîrT	WaterT	Stage	Conductivity	Mm	Ď	od 1	ſγ	Hr	Mn	Ss AirT	WaterT	Stage	Conductivity
1	6	94	13	37	42 -3.85	0.5	6.74	399	1	1	11 9	14	10	37	42 -16.1	0.53	6.53	403
1	6	94	16	37	42 -5.26	0.58	6.74	392	1	1	11 9	14	13	37	42 -16.3	0.52	6.52	402
3	6	94	19	37	42 -6.79	0.58	6.74	393	1	1	17 9	14	16	37	42 -16.3	0.52	6.52	401
1	6	94	22	37	42 -7.88	0.59	6.74	393	1	1	11 9	14	19	37	42 -16.5	0.52	6.51	402
1	7	94	1	37	42 -8.74	0.58	6.74	393	1	1	11 9	4	22	37	42 -16.7	0.52	6.5	403
1	7	94	4	37	42 -9.27	0.58	6.73	392	1	1	12 9	14	1	37	42 -16.9	0.52	6.5	403
1	7	94	7	37	42 -9.27	0.58	6.73	393	1			4	4	37	42 -17	0.51	6.49	404
1	7	94	10	37	42 -9.38	0.58	6.73	394	1			14	7	37	42 -17.1	0.51	6.48	406
1	7	94	13	37	42 -9.7	0.58	6.72	395	1	1			10	37	42 -17.2	0.51	6.48	406
1	7	94	16	37	42 -9.89	0.57	6.72	397	1	1	12 9		13	37	42 -17-4	0.51	6.47	406
1	7	94	19	37	42 -10.1	0.57	6.72	394	1				16	37	42 -17-5	0.51	6.46	405
1	7	94	22	37	42 -10.6	0.57	6.72	396	1		_		19	37	42 -17.8	0.5	6.46	406
1	8	94	1	37	42 ~11.6	0.57	6.71	395	1		_		22	37	42 -18.4	0.5	6-46	404
1	8	94	4	37	42 -13.1	0.57	6.71	395	3			4	1	37	42 -18.1	0.5	6.45	406
1	8	94	7	37	42 -14	0.57	6.7	396	1			4	4	37	42 -17.8	0.5	6.44	405
1	8	94	10	37	42 -14.7	0.57	6.69	397	1			4	.7	37	42 -17.3	0.5	6-44	404
1	8	94	13	37	42 - 34.6	0.57	6.69	396	1				10	37	42 -17.2	0.5	6.43	404
1	8	94	16	37	42 -14.3	0.56	6.68	396	1				13	37	42 -16.9	0.5	6.42	404
1	8	94	19	37	42 -14.3	0.56	6.68	396	1				16	37	42 -16.5	0.5	6.42	404
1	8	94	22	37	42 -14.4	0.56	6.67	399	!				19	37	42 -16.7	0.49	6.41	402
3	9	94	1	37	42 -14.5	0.55	6-66	397	1				22	37	42 -16.9	0.49	6.41	403
1	9	94	4	37	42 -14.8	0.55	6.66	399				4	1	37	42 -16.9	0.49	6.4	402
?	9	94	7	37	42 -14.9	0.55	6.65	398	;			14	4	37 37	42 -16.9 42 -17	0.49 0.49	6.39 6.39	402 401
1	9	94 94	10	37 37	42 -14.9	0.55 0.55	6.64	40 <b>1</b> 402	1			-	7 10	37	42 -17 42 -17	0.49	6.38	400
1	9	94	13 16	37	42 -14.7 42 -14.3	0.55	6.64	402	-				13	37 37	42 -16.7	0.48	6.38	400
1	9	94	19	37 37	42 -14.3	0.55	6.62	402 401	1				16	37	42 -16.7	0.48	6.38	401
1	9	94	22	37	42 -14-2	0.54	6.61	400	- 1				19	37	42 -15.5	0.48	6.37	400
- ;	10	94	1	37	42 -13.9	0.54	6.61	400	1				22	37	42 -15.1	0.48	6.37	400
	10	94	4	37	42 -13.9	0.54	6.6	400	1			4	1	37	42 -14.7	0.48	6.36	400
1	10	94	7	37	42 -13.9	0.54	6.59	402				4	4	37	42 -14.4	0.48	6.35	400
- 1	10	94	10	37	42 -14.1	0.54	6.58	401	i			4	7	37	42 -14.3	0.48	6.35	402
- ;	10	94	13	37	42 -14.3	0.54	6.58	402	i				10	37	42 -14.3	0.48	6.34	403
i	10	94	16	37	42 -14.4	0.54	6.57	402	i				13	37	42 -14.3	0.47	6.34	401
i	10	94	19	37	42 -14.5	0.53	6.56	402	i				16	37	42 -14.4	0.47	6.33	401
i	10	94	22	37	42 -14.7	0.53	6.55	401	i			-	19	37	42 -14.6	0.47	6.33	400
1	11	94	1	37	42 -15-1	0.53	6.55	403	i				22	37	42 -14.6	0.47	6.32	400
ì	11	94	4	37	42 -15.4	0.53	6.54	403	1			4	1	37	42 -15	0.47	6.32	402
1	11	94	7	37	42 -15.8	0.53	6.53	401	i			4	4	37	42 -15.5	0.47	6.31	402
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This is data as recorded by the data logger and is raw data for app. E.

Appendix D

Gambell Observation Well #2

Mm	Dd	Υy	Яг	Kn	Ss AirT	WaterT	Stage	Conductivity	Mm	Do	d Yy	ĦГ	Mn	Ss AirT	WaterT	Stage 0	onductivity
1	16	94	7	37	42 -15.7	0.47	6.31	402	1	21	94	13	37	42 -16.2	0.41	6.11	407
i	16	94	10	37	42 - 15.7	0.47	6.3	401	1	21		16	37	42 -15.8	0.41	6.11	407
i	16	94	13	37	42 -15-6	0.46	6.3	401	1	21	94	19	37	42 -15.3	0.41	6.11	406
i	16	94	16	37	42 -15.3	0.46	6.29	402	1	21	94	22	37	42 -14.8	0.41	6.11	406
1	16	94	19	37	42 -15.2	0.46	6.29	403	1	22	94	1	37	42 -14.1	0.43	6.11	406
1	16	94	22	37	42 -15.2	0-46	6.28	402	1	22	94	4	37	42 -13.9	0.41	6.1	406
1	17	94	1	37	42 -15.2	0.46	6.27	403	1	22		7	37	42 -13.8	0.4	6.1	406
1	17	94	4	37	42 -15.2	0.45	6.27	401	1	22		10	37	42 -13.8	0.4	6.1	405
1	17	94	7	37	42 -15.3	0.46	6.26	401	1	22		13	37	42 -13.8	0.4	6.1	405
1	17	94	10	37	42 -15.5	0,45	6.26	402	1	22		16	37	42 -13.8	0.4	6.1	404
1	17	94	13	37	42 -15-6	0.45	6.25	402	1	22		19	37	42 -13.6	0.4	6.09	405
1	17	94	16	37	42 -15.7	0.45	6.24	401	1	22		22	37	42 -13.5	0.4	6.09	404
1	17	94	19	37	42 -15.5	0.45	6.24	403	1	23		3	37	42 -13.3	0.4	6.09	404
1	17	94	22	37	42 - 15 - 6	0.45	6.23	403	1	23		4	37	42 ~13.2	0.4	6.09	403
1	18	94	1	37	42 -15.6	0.44	6.22	402	!	23		7	37	42 -13.2	0.39	6.08	403 403
1	18	94	4	37	42 -15.6	0.44	6.22	402	1	22		10	37	42 -13.3	0.39	6.08 6.08	403
1	18	94	7	37	42 -15.8	0.44	6.21	403	1	23		13	37 37	42 -13.7 42 -14.3	0.39 0.39	6.08	402
1	18	94	10	37	42 -15.9	0.44	6.21	401	!	23		16 19	37 37	42 -14.3	0.39	6.07	402
1	18	94	13	37	42 -16	0.44	6.2	403	1	Z:		22	37	42 -16.4	0.38	6.07	402
1	18	94	16	37	42 -16	0.43	6.19	401	1	24		1	37	42 -10.4	0.38	6.07	402
Ţ	18	94	19	37	42 -16.1	0.43	6.19	402 402	1	24		4	37	42 -18.3	0.38	6.06	402
1	18	94	22	37	42 -16.2	0.43	6.18 6.17	402	1	24		7	37	42 -18.8	0.37	6.06	402
!	19	94	1	37 37	42 -16.3 42 -16.4	0.43 0.43	6.17	405	i	24		10	37	42 - 19-5	0.37	6.06	402
1	19 19	94 94	7	37	42 -16.5	0.43	6.16	407	i	24		13	37	42 -20	0.37	6.05	401
1	19	94	10	37 37	42 -16.6	0.42	6.15	408	i	54		16	37	42 -20.3	0.37	6.05	401
1	19	94	13	37	42 -16.6	0.42	6.15	409	1	2/		19	37	42 -20.5	0.36	6.05	402
1	19	94	16	37	42 -16.6	0.42	6.14	408	1	24		22	37	42 -20.6	0.36	6.04	401
1	19	94	19	37	42 -16.5	0.42	6.14	410	1	25		1	37	42 -20.5	0.36	6.04	401
i	19	94	55	37	42 -16.4	0.42	6.13	410	1	25		4	37	42 -20.2	0.36	6.04	400
ì	20	94	1	37	42 -16.5	0.42	6.13	410	1	25	5 94	7	37	42 -20	0.35	6.04	400
ì	20	94	4	37	42 -16.6	0.41	6.13	411	1	25	5 94	10	37	42 -19.9	0.35	6.03	400
1	20	94	7	37	42 -16.7	0.42	6.12	411	t	25	5 94	13	37	42 -19.8	0.35	6.03	400
1	20	94	10	37	42 -17-3	0.41	6.12	412		25		16	37	42 -19.7	0.35	6.03	400
1	20	94	13	37	42 - 17.1	0.41	6.12	411	1	2		19	37	42 -19.8	0.34	6.03	400
1	SO	94	16	37	42 -17.2	0.41	6.11	410	1	25		22	37	42 -20.1	0.34	6.03	400
1	20	94	19	37	42 -16.9	0.41	6.11	409	1	26		1	37	42 -20.1	0.34	6.03	400
1	20	94	22	37	42 -16.8	0.41	6.11	408	1	26		4	37	42 -20.2	0.33	6.03	400
1	21	94	1	37	42 -16.7	0.41	6.11	407	1	20		7	37	42 -20.5	0.33	6.03	400
1	21	94	4	37	42 -16.7	0.41	6.11	407	1	20		10	37	42 ~20.8	0.33	6.02	400
1	21	94	7	37	42 -16.6	0.41	6.11	406	1	20		13	37	42 -21.1	0.32	6.02	400
1	21	94	10	37	42 -16.5	0.41	6.11	406	1	26	5 94	16	37	42 -21.1	0.32	6.02	401

Appendix D

Gambell Observation Well #2

1     26     94     19     37     42 -21.2     0.32     6.02     400     2     1     94     1     37     42 -10.4     0.21     5.96       1     26     94     22     37     42 -21.3     0.31     6.02     399     2     1     94     4     37     42 -8.96     0.2     5.96       1     27     94     1     37     42 -21.2     0.31     6.02     399     2     1     94     7     37     42 -7.97     0.2     5.97       1     27     94     7     37     42 -21.3     0.31     6.02     400     2     1     94     10     37     42 -6.61     0.2     5.98       1     27     94     7     37     42 -21.5     0.31     6.02     399     2     1     94     16     37     42 -6.05     0.2     5.98       1     27     94     10     37     42 -7.26     0.19     5.99       1     27     94     10     37     42 -7.26     0.19     5.99	396 398 398 397 396 396 395 395 395 394 394
1 26 94 22 37 42 -21.3     0.31 6.02 399     2 1 94 4 37 42 -8.96     0.2 5.96       1 27 94 1 37 42 -21.2     0.31 6.02 399     2 1 94 7 37 42 -7.97     0.2 5.97       1 27 94 4 37 42 -21.3     0.31 6.02 400     2 1 94 10 37 42 -6.61     0.2 5.98       1 27 94 7 37 42 -21.5     0.31 6.02 399     2 1 94 13 37 42 -6.05     0.2 5.98	398 398 397 396 396 395 395 395 394 394
1     27     94     1     37     42     -21.2     0.31     6.02     399     2     1     94     7     37     42     -7.97     0.2     5.97       1     27     94     4     37     42     -21.3     0.31     6.02     400     2     1     94     10     37     42     -6.61     0.2     5.98       1     27     94     7     37     42     -21.5     0.31     6.02     399     2     1     94     13     37     42     -6.05     0.2     5.98	397 396 396 395 395 395 394 394
1 27 94 4 37 42 -21.3 0.31 6.02 400 2 1 94 10 37 42 -6.61 0.2 5.98 1 27 94 7 37 42 -21.5 0.31 6.02 399 2 1 94 13 37 42 -6.05 0.2 5.98	396 396 395 395 395 394 394
1 27 94 7 37 42 -21.5 0.31 6.02 399 2 1 94 13 37 42 -6.05 0.2 5.98	396 395 395 395 394 394
	395 395 395 394 394
	395 395 394 394
1 27 94 13 37 42 -21.9 0.3 6.02 400 2 3 94 19 37 42 -7.73 0.19 5.99	395 394 394
1 27 94 16 37 42 -21.9 0.3 6.01 400 2 1 94 22 37 42 -6.94 0.18 6	394 394
1 27 94 19 37 42 -22 0.29 6.01 399 2 2 94 1 37 42 -6.19 0.18 6	394
1 27 94 22 37 42 -22.1 0.29 6.01 399 2 2 94 4 37 42 -6.09 0.18 6.01	
1 28 94 1 37 42 -22.2 0.29 6.01 399 2 2 94 7 37 42 -5.83 0.17 6.01	707
1 28 94 4 37 42 -22.1 0.29 6.01 399 2 2 94 10 37 42 -4.99 0.17 6.01	
1 28 94 7 37 42 -21.9 0.28 6.01 398 2 2 94 13 37 42 -5.03 0.17 6.02	391
1 28 94 10 37 42 -21.7 D.28 6 398 2 2 94 16 37 42 -5.31 0.16 6.02	391
1 28 94 13 37 42 -21.5 0.28 6 398 2 2 94 19 37 42 -5.16 0.16 6.03	391
1 28 94 16 37 42 -21.2 0.27 6 398 2 2 94 22 37 42 -4.85 0.16 6.03	390
1 28 94 19 37 42 -20.9 0.27 6 398 2 3 94 1 37 42 -3.84 0.15 6.03	390
1 28 94 22 37 42 -20.6 0.27 5.99 398 2 3 94 4 37 42 -3.61 0.15 6.04	390
1 29 94 1 37 42 -20.2 0.27 5.99 397 2 3 94 7 37 42 -3.88 0.15 6.04	389
1 29 94 4 37 42 -19.7 0.27 5.99 399 2 3 94 10 37 42 -3.97 0.14 6.05	388
1 29 94 7 37 42 -19.1 0.26 5.99 398 2 3 94 13 37 42 -4.18 0.14 6.05	388
1 29 94 10 37 42 -18.8 0.26 5.98 397 2 3 94 16 37 42 -4.35 0.14 6.05	386
1 29 94 13 37 42 -18.5 0.25 5.98 398 2 3 94 19 37 42 -4.55 0.13 6.06 1 29 94 16 37 42 -18.2 0.25 5.98 398 2 3 94 22 37 42 -4.76 0.13 6.06	385 386
	385
	384
1 29 94 22 37 42 -17.5 0.25 5.97 397 2 4 94 4 37 42 -4.69 0.12 6.07 1 30 94 1 37 42 -17.2 0.25 5.97 397 2 4 94 7 37 42 -4.7 0.12 6.07	383
1 30 94 4 37 42 -16.9 0.24 5.96 397 2 4 94 10 37 42 -4.93 0.12 6.07	382
1 30 94 7 37 42 -16.6 0.24 5.96 397 2 4 94 13 37 42 -5.21 0.11 6.08	382
1 30 94 10 37 42 -16.3 0.24 5.96 397 2 4 94 16 37 42 -5.34 0.11 6.08	381
1 30 94 13 37 42 -15.9 0.24 5.96 397 2 4 94 19 37 42 -5.17 0.11 6.08	381
1 30 94 16 37 42 -15.5 0.23 5.96 397 2 4 94 22 37 42 -5.09 0.11 6.08	380
1 30 94 19 37 42 -15 0.23 5.96 397 2 5 94 1 37 42 -4.99 0.1 6.08	381
1 30 94 22 37 42 -12.9 0.23 5.96 398 2 5 94 4 37 42 -4.98 0.1 6.08	381
1 31 94 1 37 42 -12.6 0.23 5.96 397 2 5 94 7 37 42 -4.94 0.1 6.09	381
1 31 94 4 37 42 -12-2 0.22 5.95 397 2 5 94 10 37 42 -4.73 0.1 6.09	383
1 31 94 7 37 42 -11.4 0.22 5.95 399 2 5 94 13 37 42 -4.43 0.09 6.09	383
1 31 94 10 37 42 -10.7 0.22 5.95 399 2 5 94 16 37 42 -4.53 0.09 6.09	383
1 31 94 13 37 42 -9.75 0.22 5.95 397 2 5 94 19 37 42 -4.71 0.09 6.1	383
1 31 94 16 37 42 -9.15 0.21 5.95 398 2 5 94 22 37 42 -3.97 0.08 6.1	384
1 31 94 19 37 42 -9.3 0.21 5.95 397 2 6 94 1 37 42 -3.62 0.08 6.11	387
1 31 94 22 37 42 -10.5 0.21 5.96 396 2 6 94 4 37 42 -3.89 0.08 6.11	388

Appendix D

Gambell Observation Well #2

Mm	Dď	Yy	Hr	Mn	\$s AirT	WaterT	Stage	Conductivity	Mm	Dď	Yy	Hr	Mn	Ss Airī	WaterT	Stage	Conductivity
2	6	94	7	37	42 -4.2	0.07	6.12	390	2	11	94	13	37	42 -13.9	-0.04	6.22	411
2	6	94	10	37	42 -4-64	0.07	6.13	391	2	11	94	16	37	42 -13.3	-0.05	6.22	411
2	6	94	13	37	42 -4.98	0.07	6.14	392	2	11	94	19	37	42 -13.1	-0.05	6.21	412
2	6	94	16	37	42 -5.03	0.06	6.15	396	2	11	94	22	37	42 -13.3	-0.05	6.2	411
ž	6	94	19	37	42 -4.93	0.06	6.15	396	ž	12	94	1	37	42 -13.6	-0.05	6.19	411
ž	6	94	22	37	42 -4.73	0.06	6.17	398	2	12	94	4	37	42 -14	-0.05	6.19	412
2	7	94	1	37	42 -4-51	0.05	6.17	400	2	12	94	7	37	42 -13.9	-0.05	6.18	411
2	7	94	4	37	42 -4.28	0.05	6.18	402	2	12	94	10	37	42 -13.6	-0.05	6.17	411
2	7	94	7	37	42 -4.18	0.04	6.19	402	2	12	94	13	37	42 -13.3	-0.05	6.16	410
2	7	94	10	37	42 -4-03	0.04	6.2	405	2	12	94	16	37	42 -13	-0.05	6.15	410
2	7	94	13	37	42 -3.9	0.04	6.21	406	2	12	94	19	37	42 -13	-0.05	6.14	411
2	7	94	16	37	42 -3.87	0.03	6.22	406	2	12	94	22	37	42 -13.2	-0.05	6.14	409
2	7	94	19	37	42 -3.86	0.03	6.23	408	2	13	94	1	37	42 ~12.8	-0.05	6.13	411
2	7	94	22	37	42 -3.89	0.03	6.24	409	2	13	94	4	37	42 -12.4	-0.05	6.12	410
2	8	94	1	37	42 -3.93	0.02	6.24	409	2	13	94	7	37	42 -12.2	-0.05	6.11	411
2	8	94	4	37	42 -3.99	0.02	6,25	409	2	13	94	10	37	42 -11.9	-0.05	6.1	411
2	8	94	7	37	42 -4.19	0.02	6.26	411	2	13	94	13	37	42 -11.7	-0.05	6.09	410
2	8	94	10	37	42 -4.37	0.01	6.26	411	2	13	94	16	37	42 -11-2	-0.05	6,08	410
2	8	94	13	37	42 -4.53	0.01	6.27	412	2	13	94	19	37	42 -11.1	-0.05	6.07	412
2	8	94	16	37	42 -4.52	0.01	6.27	413	2	13	94	22	37	42 -11.2	-0.05	6.07	412
2	8	94	19	37	42 -4.58	0.01	6.27	411	2	14	94	1	37	42 -11.9	-0.06	6.06	412
2	8	94	22	37	42 -4.64	0.01	6.28	412	2	14	94	4	37	42 -12-4	~0.06	6.05	414
2	9	94	1	37	42 -4.74	0	6.28	411	2	14	94	7	37	42 -13.6	-0.06	6.04	411
2	9	94	4	37	42 -5.04	0	6.28	412	2	14	94	10	37	42 -14.2	-0.06	6.03	412
2	9	94	.7	37	42 ~5.4	~0.01	6,29	413	2	14	94	13	37	42 -14.5	-0.06	6.02	411
2	9	94	10	37	42 -5.56	-0.01	6.29	413	2	14	94	16	37	42 ~14.1	-0.06	6.02	412
2	9	94	13	37	42 -5.73	-0.01	6.29	414	2	14	94	19	37	42 -14.1	-0.06	6.01	412
2	9	94	16	37	42 -5.75	-0.02	6.29	413	2	14	94	22	37	42 -14.4	-0.07	6	418
2	9	94	19	37	42 -6	-0.02	6.29	412	5	15	94	1	37	42 -14.5	-0.07	. 6	420 425
2	9	94	SS	37	42 -6.91	-0.02	6.3	413	2	15	94	4	37	42 -14.7	-0.07	5.99 5.98	425 426
2	10	94	1	37	42 -8.22	-0.02	6.29	414	2	15 15	94 94	7 10	37 37	42 -14.8 42 -14.9	-0.07 -0.08	5.98	421
2	10	94	4	37	42 -9.16	~0.02	6.29	413	2	15	94	13	37 37	42 -14.8	-0.08	5.97	419
2	10	94	7 10	37 37	42 -10.2 42 -10.9	-0.03 -0.03	6.29 6.28	414 414	2	15	94	16	37 37	42 -14.3	-0.08	5.96	419
2	10	94	13		42 -11.4			413	2	15	94	19	37 37	42 - 14.3	-0.08	5.96	436
2	10 10	94 94		37 37	42 -11.4	-0.03 -0.03	6.28 6.27	413	2	15	94	22	37	42 -14.3	-0.08	5.95	420
2	10	94	16 19	37 37	42 -11.0	-0.03	6.27	414	2	16	94	1	37 37	42 -14.6	-0.1	5.94	435
2	10	94	22	37	42 - 12.1	-0.03		413	2	16	94	4	37	42 -15	-0.08	5.94	426
2	11	94	1	37	42 - 12.9	-0.04	6.26 6.25	413	2	16	94	7	37	42 -15.7	-0.08	5.93	421
2	17	94	4	37 37	42 - 12.9	-0.04	6.24	413	2	16	94	10	37	42 -16.3	-0.09	5.93	435
	11	94	7	37	42 - 13.8	-0.04	6.24	411	2	16	94	13	37	42 -16.7	-0.09	5.92	439
2	11	94	10	37	42 -14.1	-0.05	6.23	412	2	16	94	16	37	42 -16.4	-0.08	5.92	446
4	1 1	<b>y</b> 4	10	31	42 -14.1	-0.05	0.43	414	2	10	74	10	,,	46 -10.4	0.00	3.72	770

Appendix D

Gambell Observation Well #2

Mm	Dď	Υy	Нг	Mn	Ss AirT	WaterT	Stage	Conductivity	Mm	Dd	Yу	Hr	Mn	Ss AirT	WaterT	Stage Co	onductivity
2	16	94	19	37	42 -16,4	-0.08	5.91	441	2	22	94	1	37	42 -13.4	-0.14	5.84	509
	16	94	22	37	42 -16.1	-0.08	5.9	431	2	22	94	4	37	42 -13.4	-0.13	5.84	524
	17	94	1	37	42 -15.9	-0.08	5.9	428	2	22	94	7	37	42 -13.4	-0.13	5.84	521
_	17	94	4	37	42 -15.8	-0.09	5.9	434	2	22	94	10	37	42 -13.5	-0,13	5.84	508
	17	94	7	37	42 -16.2	-0.09	5.89	439	2	22	94	13	37	42 -13.3	-0.13	5.83	533
	17	94	10	37	42 -16.7	-0.09	5.89	443	2	22	94	16	37	42 -13.1	-0.13	5.83	520
	17	94	13	37	42 -16.9	-0.09	5.88	431	2	22	94	19	37	42 -12.7	-0.13	5.83	517
	17	94	16	37	42 -16.7	-0.09	5.88	429	2	22	94	22	37	42 -12.5	-0.13	5.83	524
	17	94	19	37	42 -16.6	-0.09	5.88	447	2	23	94	1	37	42 -12.3	-0.14	5.83	539
_	17	94	22	37	42 -16-8	-0.09	5.87	432	2	23	94	4	37	42 -12.2	-0.16	5.83	569
	18	94	1	37	42 -17	-0.09	5.87	438	2	23	94	7	37	42 -12.2	-0.14	5.82	548
	18	94	4	37	42 -17.1	-0.1	5.87	437	2	23	94	10	37	42 -12.3	-0.14	5.82	539
_	18	94	7	37	42 -16.7	-0.1	5.87	432	2	23	94	13	37	42 -12.2	-0.15	5.82	565
	18	94	10	37	42 -16-6	-0.17	5.86	441	2	23	94	16	37	42 -11.7	-0.15	5.82	577
	18	94	13	37	42 -16.5	-0.11	5.86	444	2	23	94	19	37	42 -11.3	-0.15	5.81	591
	18	94	16	37	42 -16-1	-0.1	5.86	442	2	23	94	22	37	42 -11.2	-0.16	5.81	580
	18	94	19	37	42 -15-7	-0.09	5.86	430	2	24	94	1	37	42 -11,5	-0.16	5.81	601
	18	94	22	37	42 -15.4	-0.1	5.86	432	2	24	94	4	37	42 -12.1	-0.15	5.81	574
	19	94	1	37	42 -15.1	-0.1	5.85	448	2	24	94	7	37	42 -13.2	-0.15	5.8	571
	19	94	4	37	42 -14-7	-0_1	5.85	461	2	24	94	10	37	42 -14.4	-0.15	5.8	578
	19	94	7	37	42 -14.4	-0.1	5.85	444	2	24	94	13	37	42 -14.9	-0.15	5.8	581
	19	94	10	37	42 -14.1	-0_1	5.85	439	2	24	94	16	37	42 -14.7	-0.16	5.79	586
	19	94	13	37	42 -13.6	-0.11	5.85	455	5	24	94	19	37	42 -14.7	-0.16	5.79	591
	19	94	16	37	42 -13.2	-0.11	5.85	472	2	24	94	22	37	42 -15	-0_17	5.79	599
	19	94	19	37	42 -12.9	-0.11	5.85	447	2	25	94	1	37	42 -15.2	~0.17	5.79	606
2	19	94	22	37	42 -12.6	-0.11	5.85	457	2	25	94	4	37	42 -15.2	-0.17	5.78	607
2	20	94	1	37	42 -12.4	-0.11	5.85	450	2	25	94	7	37	42 -15.2	-0.17	5.78	611
	20	94	4	37	42 -12.3	-0.11	5.85	456	2	25	94	10	37	42 -15.2	-0.17	5.77	620
2	20	94	7	37	42 -12.2	-0.12	5.85	461	2	25	94	13	37	42 -15	-0.17	5.77	627
2	20	94	10	37	42 -12.2	-0.1	5.84	469	2	25	94	16	37	42 -14.7	-0.17	5.76	632
2	20	94	13	37	42 -12.2	-0.12	5.85	474	2	25	94	19	37	42 -14.2	-0.17	5.76	640
2	20	94	16	37	42 -12-2	-0.13	5.84	493	2	25	94	22	37	42 -14	-0.17	5,75	641
2	20	94	19	37	42 -12.3	-0.12	5.84	473	2	26	94	1	37	42 -13.8	~0.17	5.75	642
2	20	94	22	37	42 -12.5	-0.11	5.84	474	2	26	94	4	37	42 -13.6	-0.17	5.74	644
2	21	94	1	37	42 -12.8	-0.12	5.84	508	2	26	94	7	37	42 -13.5	-0.17	5.74	653
2	21	94	4	37	42 -13	-0.13	5.84	495	2	26	94	10	37	42 -13.6	-0.17	5.73	674
	21	94	7	37	42 -13.3	-0.12	5.84	503	2	26	94	13	37	42 -13.8	-0.17	5.73	693
2	21	94	10	37	42 -13.6	-0.14	5.84	511	2	26	94	16	37	42 -14	~0.17	5.72	694
2	21	94	13	37	42 -13.8	-0.12	5.84	493	2	26	94	19	37	42 -14.7	-0.16	5.71	699
	21	94	16	37	42 -13.6	-0.13	5.84	517	2	26	94	22	37	42 -15.8	-0.16	5.71	703
2	21	94	19	37	42 -13.3	-0.14	5.84	513	2	27	94	1	37	42 -16.9	-0.16	5.7	706
2	21	94	22	37	42 -13.4	-0.14	5.84	512	2	27	94	4	37	42 -17.6	-0.17	5.7	713

Appendix D

Gambell Observation Well #2

Mm	Dd	¥γ	Вr	MA	Ss AirT	WaterT	Stage	Conductivity	Mm	Dd	Yy	Яr	Ħn	Ss AirT	WaterT	Stage Co	nductivity
2	27	94	7	37	42 -18	-0.18	5.7	708	3	4	94	13	37	42 -21.9	-0.21	5.51	919
2	27	94	10	37	42 -18.6	-0.18	5.69	720	3	4	94	16	37	42 -21	-0.21	5.51	925
5	27	94	13	37	42 -19	-0.18	5.69	734	3	4	94	19	37	42 -20.6	-0.2	5.5	927
2	27	94	16	37	42 -18.8	-0.18	5.69	742	3	Ž	94	22	37	42 ~20.8	-0.21	5.5	935
2	27	94	19	37	42 -19.1	-0.18	5.68	756	3	5	94	1	37	42 -21	-0.21	5.49	935
2	27	94	22	37	42 -19.9	-0.19	5.68	769	3	ś	94	4	37	42 -21.2	-0.21	5.49	937
2	28	94	1	37	42 -20.4	-0.19	5.67	7 <b>7</b> 7		5	94	7	37	42 -22.2	-0.21	5.48	941
5	28	94	4	37	42 -20.7	-0.19	5.67	781	3	5	94	10	37	42 -22.1	-0.21	5.48	943
5	28	94	7	37	42 -21.2	-0.19	5.67	790	3	5	94	13	37	42 -21.8	-0.21	5.47	946
2	28	94	10	37	42 -21.6	-0.19	5.66	800	3	ś	94	16	37	42 -21.2	-0.21	5.47	947
2	28	94	13	37	42 -21.5	-0.19	5.66	804	3	5	94	19	37	42 -20.5	-0.21	5.46	948
2	28	94	16	37	42 -20.6	-0.19	5.66	809	3	5	94	22	37	42 -20.5	-0.21	5.46	936
2	28	94	19	37	42 -20	-0.19	5.65	811	3	6	94	3	37	42 -28.4	-0.21	5-45	939
5	28	94	22	37	42 -19.9	-0.19	5.65	813	3	6	94	4	37	42 -20.5	-0.21	5.45	932
3	1	94	1	37	42 -20.1	-0.19	5.65	816	3	6	94	7	37	42 -20.6	-0.21	5.44	943
3	•	94	4	37	42 -20.4	-0.19	5.64	801	3	6	94	10	37	42 -20.7	-0.21	5.44	941
3	1	94	7	37	42 -20.6	-0.2	5.64	818	3	6	94	13	37	42 ~20.6	-0.21	5.44	938
7	1	94	10	37	42 -21.1	-0.2	5.63	825	3	6	94	16	37	42 -20	-0.22	5.43	940
Ž	1	94	13	37	42 -21.8	-0.19	5.63	809	3	6	94	19	37	42 - 19.8	-0.21	5.43	950
٠ ۲	1	94	16	37	42 -21.5	-0.2	5.62	832	3	6	94	22	37	42 -20	-0.22	5.43	941
3	3	94	19	37	42 -21.9	-0.2	5.62	828	3	7	94	1	37	42 -20.1	-0.22	5.42	947
<b>₹</b>	,	94	22	37	42 -22	-0.19	5.61	839	ž	7	94	4	37	42 -20.2	-0.22	5.42	939
3	ż	94	1	37	42 -22.3	-0.2	5.61	844	3	7	94	7	37	42 -20.3	-0.22	5.42	940
3	2	94	i	37	42 -22.8	-0.2	5.6	833	3	7	94	10	37	42 -20.2	-0.22	5.42	943
3	ž	94	7	37	42 -23.4	-0.2	5.6	853	3	7	94	13	37	42 -19.9	-0.22	5.41	910
3	2	94	10	37	42 -23.9	-0.19	5.6	841	3	7	94	16	37	42 -19.3	-0.22	5.41	912
3	ž	94	13	37	42 -23.9	-0.2	5.59	859	3	7	94	19	37	42 -19	-0.22	5.41	914
3	2	94	16	37	42 -23.7	-0.2	5.59	857	3	7	94	22	37	42 -19	-0.22	5.4	908
3	2	94	19	37	42 -23.8	-0.19	5.58	843	3	8	94	1	37	42 -19,2	-0.22	5.4	910
3	2	94	22	37	42 -24.1	-0.19	5.58	851	3	8	94	4	37	42 -19.6	-0.22	5.4	913
3	3	94	1	37	42 -24.3	-0.19	5.57	858	3	8	94	7	37	42 -19.7	~0.22	5.39	957
3	3	94	4	37	42 -24.2	-0.19	5.57	859	3	8	94	10	37	42 -19.7	-0.23	5.39	943
3	3	94	7	37	42 -24.1	-0.2	5.56	867	3	8	94	13	37	42 -19.5	-0.23	5.38	932
3	3	94	10	37	42 -23.9	-0.19	5.56	873	3	8	94	16	37	42 - 19.1	-0.23	5.38	955
3	3	94	13	37	42 -23.4	-8.2	5.55	889	3	8	94	19	37	42 -18.9	-0.23	5.38	972
3	3	94	16	37	42 -22.9	-0.2	5.55	894	3	8	94	22	37	42 -19	-0.23	5.37	952
3	3	94	19	37	42 -22.6	-0.2	5.54	898	3	9	94	1	37	42 -19.1	-0.23	5.37	914
3	3	94	22	37	42 -22.4	-0.21	5.54	903	3	9	94	4	37	42 -19-1	-0.23	5.36	920
3	4	94	1	37	42 -22.6	-8.2	5.53	905	3	9	94	7	37	42 -19.1	-0.23	5.36	915
3	4	94	4	37	42 -22.7	-0.2	5.53	910	3	9	94	10	37	42 -19.4	-0.23	5.35	918
3	4	94	7	37	42 -22.8	-0.21	5.53	914	3	9	94	13	37	42 -19.4	-0.22	5.35	943
3	4	94	10	37	42 -22.7	-0.21	5.52	916	3	9	94	16	37	42 ~19	-0.23	5.34	936

Appendix D

Gambell Observation Well #2

Mra	Dd	Υу	Нr	Ħn	Ss Airï	Waterĭ	Stage	Conductivity	Mm	Do	d Yy	Hr	Mn	Ss AirT	Waterĭ	Stage	Conductivity
3	9	94	19	37	42 -18.9	-0.23	5.34	924	3	15	94	1	37	42 -17.8	-0.24	5.25	996
3	ģ	94	22	37	42 - 19.2	-0.22	5.33	927	3	15		4	37	42 -17.7	-0.24	5.26	988
3	10	94	1	37	42 -19-4	-0.23	5.33	935	3	15		7	37	42 -17.6	-0.24	5.26	971
3	10	94	4	37	42 - 19.6	-0.23	5.32	939	3	15		10	37	42 -17.5	-0.24	5.26	953
3	10	94	7	37	42 -19.8	-0.22	5.32	931	3	15		13	37	42 -17.4	-0.24	5.27	951
3	10	94	10	37	42 -19.9	-0.23	5.31	934	3	15		16	37	42 -17.1	-0.24	5.27	953
3	10	94	13	37	42 -19.7	-0.23	5.31	932	3	15		19	37	42 -16.7	-0.24	5.27	956
3	10	94	16	37	42 - 19.3	-0.22	5.3	935	3	15		22	37	42 -16.4	-0.23	5.28	953
3	10	94	19	37	42 -19.1	-0.23	5.3	935	3	16		1	37	42 -16.2	-0.24	5.28	954
3	10	94	22	37	42 -19	-0.22	5.29	936	3	16		4	37	42 -16	-0.24	5.28	955
3	11	94	ĩ	37	42 -19.1	-0.22	5.28	936	3	16		7	37	42 -15.7	-0.24	5.29	957
3	11	94	4	37	42 -19.3	-0.22	5.28	937	3	16		10	37	42 -14.6	-0.24	5.29	960
3	11	94	7	37	42 - 19.4	-0.22	5.27	943	3	16		13	37	42 -14	-0.24	5.29	962
3	11	94	10	37	42 -19.6	-0.22	5.27	941	3	16		16	37	42 -13.3	-0.24	5.3	971
3	11	94	13	37	42 -19-5	-0.22	5.27	942	3	16		19	37	42 -13.1	-0.24	5.3	978
3	11	94	16	37	42 -19-1	-0.22	5.26	946	3	16		22	37	42 -13.5	-0.24	5.3	988
3	11	94	19	37	42 -19	-0.23	5.26	947	3	17		1	37	42 -14	-0.24	5.31	998
3	13	94	22	37	42 -19.4	-0.22	5.25	950	3	17		4	37	42 -14.4	-0.24	5.31	996
3	12	94	1	37	42 -19.9	-0.22	5.25	949	3	17	7 94	7	37	42 -14.7	-0.25	5.32	998
3	12	94	4	37	42 -20.5	-0.23	5.24	960	3	17	94	10	37	42 ~14.7	~0.25	5.32	1003
3	12	94	7	37	42 -21	-0.23	5.24	968	3	17	7 94	13	37	42 -14.6	-0.25	5.32	989
3	12	94	10	37	42 -21.3	-0.23	5.24	987	3	17	7 94	16	37	42 -14.2	-0.25	5.33	991
3	12	94	13	37	42 -21.2	-0.23	5.24	1000	3	17	7 94	19	37	42 -13.9	-0.25	5.33	994
3	12	94	16	37	42 -20.6	-0.23	5.23	992	3	17	7 94	22	37	42 -13.9	-0.25	5.34	997
3	12	94	19	37	42 -20.1	-0.22	5.23	990	3	18	94	1	37	42 -14	-0.25	5,34	1002
3	12	94	22	37	42 -20.1	-0.23	5.23	997	3	18	3 94	4	37	42 -14.1	~0.25	5.34	1005
3	13	94	1	37	42 -20.3	~0.23	5.23	9 <b>9</b> 5	3	18	3 94	7	37	42 ~14.3	-0.25	5.35	1017
3	13	94	4	37	42 -20.5	-0.23	5.22	963	3	18	94	10	37	42 -14.7	-0.25	5.35	1016
3	13	94	7	37	42 -20.8	-0.23	5.22	961	3	18		13	37	42 -15.2	-0.25	5.35	1021
3	13	94	10	37	42 -21.4	-0.23	5.22	963	3	18		16	37	42 ~15.4	-0.26	5.35	1025
3	13	94	13	37	42 -21	-0.23	5.22	962	3	18		19	37	42 -15.9	-0.26	5.35	1028
3	13	94	16	37	42 -20.5	-0.23	5.22	961	3	18		22	37	42 -17.1	-0.26	5.35	1038
3	13	94	19	37	42 -20.1	-0.23	5.22	961	3	19		1	37	42 -18-4	-0-26	5.35	1041
3	13	94	22	37	42 -19-7	-0.23	5.23	960	3	19	-	4	37	42 -17.9	-0.26	5.35	1045
3	14	94	1	37	42 -19.4	-0.23	5.23	962	3	15		7	37	42 -18	-0.26	5.35	1048
3	14	94	4	37	42 -19.2	-0.24	5.23	1013	3	19		10	37	42 -18.1	-0.26	5.35	1053
3	14	94	7	37	42 -19	-0.24	5.23	996	3	15		13	37	42 -18	-0.26	5.35	1057
3	14	94	10	37	42 -18.8	-0.24	5.24	1014	3	19		16	37	42 -17.6	-0.26	5.35	1060
3	14	94	13	37	42 -18.7	-0.24	5.24	998	3	19		19	37	42 -17.3	-0.26	5.35	1063
3	14	94	16	37	42 -18.4	-0.24	5.24	999	3	19		22	37	42 -17.3	-0.26	5.35	1066
3	14	94	19	37	42 -18.1	-0.24	5.25	985	3	20		1	37	42 -17.3	-0.27	5.34	1070
3	14	94	2Z	37	42 - <b>17.9</b>	-0.24	5.25	1003	3	20	94	4	37	42 ~17.5	-0.27	5.34	1074

Appendix D

Gambell Observation Well #2

Mm	Dđ	Yy	Нг	Mn	Ss Airī	₩aterī	Stage	Conductivity	Мал	Dd	Yy	Кr	Mn	Ss AirT	WaterT	Stage	Conductivity
3	20	94	7	37	42 -17.3	-0.26	5.34	1076	3	25	94	13	37	42 -24.8	-0.29	5.23	1150
3	20	94	10	37	42 -17.4	-0.27	5.34	1078	3	25	94	16	37	42 -24.3	-0.29	5.23	1151
3	20	94	13	37	42 -17.3	-0.27	5.33	1079	3	25	94	19	37	42 -23.7	-0.29	5.23	1151
3	20	94	16	37	42 -17.1	-0.27	5.33	1081	3	25	94	22	37	42 -23.4	-0.29	5.23	1152
3	20	94	19	37	42 -16.8	-0.27	5.33	1079	3	26	94	1	37	42 -23.1	-0.29	5.23	1154
3	50	94	22	37	42 -17.1	-0.27	5.33	1087	3	26	94	4	37	42 -22.6	-0.29	5.23	1155
3	21	94	1	37	42 -17.2	-0.28	5.33	1101	3	26	94	7	37	42 -22.1	-0.29	5.23	1153
3	21	94	4	37	42 -17.6	-0.27	5.32	1101	3	26	94	10	37	42 -21.5	-0.29	5.22	1155
3	21	94	7	37	42 -19.7	-0.27	5,32	1104	3	26	94	13	37	42 -21	-0.28	5.22	1161
3	21	94	10	37	42 -22	-0.28	5.31	1113	3	26	94	16	37	42 -21	-0.29	5.22	1163
3	21	94	13	37	42 -23.2	-0.28	5.32	1121	3	26	94	19	37	42 -20.9	-0.29	5.23	1166
3	21	94	16	37	42 -21.7	-0.28	5.31	1112	3	26	94	22	37	42 -20.6	-0.29	5.23	1167
3	21	94	19	37	42 -22.5	-0.28	5.31	1114	3	27	94	1	37	42 -19.9	-0.29	5.22	1169
3	21	94	22	37	42 -23.6	-0.Z8	5.3	1123	3	27	94	4	37	42 -19.1	-0.29	5.23	1174
3	22	94	1	37	42 -25	-0.28	5.3	1128	3	27	94	7	37	42 -19	~0.29	5.22	1176
3	22	94	4	37	42 -26.1	-0.28	5.29	1119	3	27	94	10	37	42 -18	-0.29	5.22	1179
3	22	94	7	37	42 -26.6	-0.28	5.29	1123	3	27	94	13	37	42 -17.7	-0.29	5.22	1180
3	22	94	10	37	42 -27.3	-0.29	5.29	1125	3	27	94	16	37	42 -17.5	-0.29	5.22	1185
3	22	94	13	37	42 -27	-0.29	5.28	1143	3	27	94	19	37	42 -18	-0.2 <del>9</del>	5.23	1188
3	22	94	16	37	42 -26.4	-0.29	5.28	1143	3	27	94	22	37	42 -18.3	-0.29	5.23	1191
3	22	94	19	37	42 -26.9	-0.29	5.28	1135	3	28	94	1	37	42 -18.3	-0.29	5.23	1193
3	22	94	22	37	42 -27.7	-0.29	5.28	1137	3	28	94	4	37	42 -18.4	-0.29	5.23	1196
3	23	94	1	37	42 -27.9	-0.28	5,27	1129	3	28	94	7	37	42 -18.3	-0.29	5.23	1199
3	23	94	4	37	42 -28.1	-0.28	5.27	1126	3	28	94	10	37	42 -18	-0.29	5.23	1203
3	23	94	7	37	42 -28.7	-0.28	5.27	1128	3	28	94	13	37	42 -17.5	-0.29	5.23	1206
3	23	94	10	37	42 -29	-0.28	5.27	1129	3	28	94	16	37	42 -17-4	-0.29	5.23	1210
3	23	94	13	37	42 -27.8	-0.29	5.27	1128	3	28	94	19	37	42 - 17-4	-0.29	5.22	1212
3	23	94	16	37	42 -26.9	-0.29	5,26	1125	3	28	94	22	37	42 - 17.5	-0.29	5.22	1216
3	23	94	19	37	42 -26.9	-0.28	5.26	1126	3	29	94	1	37	42 -17.4	-0.29	5,22	1216
3	23	94	22	37	42 -27.5	-0.29	5.26	1129	3	29	94	4	37	42 -17.3	-0.3	5.22	1221
3	24	94	1	37	42 -27.9	-0,29	5.26	1131	3	29	94	. 7	37	42 -17.2	-0.29	5.21	1226
3	24	94	4	37	42 -28.2	-0.29	5.26	1135	3	29	94	10	37	42 -17.1	-0.29	5.21	1227
3	24	94	7	37	42 -28.6	-0.29	5.26	1138	3	29	94	13	37	42 -16.5	-0.29	5.21	1229
3	24	94	10	37	42 -28.5	-0.29	5.26	1136	3	29	94	16	37	42 -16.3	-0.29	5.21	1232
3	24	94	13	37	42 -27.6	-0.29	5.25	1135	3	29	94	19	37	42 -15.7	-0.29	5.21	1237
3	24	94	16	37	42 -26.4	-0.29	5.25	1137	3	29	94	22	37	42 -15.7	-0.29	5.2	1241
3	24	94	19	37	42 -25.8	-0.29	5.25	1140	3	30	94	1	37	42 -15.7	-0.3	5.2	1242
3	24	94	22	37	42 -26.5	-0.29	5.25	1140	3	30	94	4	37	42 - 15.7	-0.3	5.2	1244
3	25	94	1	37	42 -26.4	-0.28	5.24	1142	3	30	94	7	37	42 - 15.9	-0.29	5.2	1249
3	25	94	4	37	42 -26.5	-0.29	5.24	1145	3	30	94	10	37	42 -15.9	-0.3	5.2	1252
3	25	94	. 7	37	42 -25.9	-0.29	5.24	1149	3	30		13	37	42 -15.5	-0.29	5.2	1255
3	25	94	10	37	42 -25.5	-0.29	5.24	1150	3	30	94	16	37	42 -15_1	-0.3	5.2	1257

Appendix D

Gambell Observation Well #2

Mm	Dd	Yy	Hг	Mn	Ss AirT	WaterT	Stage	Conductivity	Mm	D	d Y	y H	ir Mn	Ss AirT	WaterT	Stage Co	onductivity
3	30	94	19	37	42 -14.7	-0.29	5.2	1256	4		5 94	4	1 37	42 -5.42	-0.3	5.28	1378
3	30	94	22	37	42 -14.5	-0.3	5.2	1263	4	i	5 9		4 37	42 -5.92	-0.3	5.28	1381
3	31	94	1	37	42 -14.2	-0.3	5.2	1267	Ä		5 9		7 37	42 -6.34	-0.3	5.28	1385
3	31	94	4	37	42 -14	-0.3	5.2	1268	4		5 9		0 37	42 -6.59	-0.3	5.28	1386
3	31	94	7	37	42 -13.7	-0.3	5.2	1264	4		5 94		3 37	42 -6.77	-0.3	5.29	1387
3	31	94	10	37	42 -13.4	-0.3	5.2	1271	4		5 9		6 37	42 -6.78	-0.3	5.29	1388
3	31	94	13	37	42 -12.8	-0.29	5.2	1274	7		5 9		9 37	42 -6.73	-0.3	5.29	1391
3	31	94	16	37	42 -11.9	-0.3	5.21	1275	4		5 9		2 37	42 -6.8	-0.3	5.29	1394
3	31	94	19	37	42 - 11.3	-0.3	5.21	1278	4		6 9		1 37	42 -7-08	-0.3	5.3	1397
3	31	94	22	37	42 -10.8	-0.3	5.21	1281	7		6 9		4 37	42 -7.32	-0.3	5.3	1400
4	3, 1	94	1	37	42 -10.7	-0.3	5.21	1283	4		6 94		7 37	42 -7.6	-0.3	5.29	1402
7	ì	94	4	37	42 -10.2	-0.3	5.22	1287	7.		6 9		0 37	42 -7.95	-0.3	5.29	1404
4	ì	94	7	37	42 -10.2	-0.3	5.22	1290	7.		6 9		3 37	42 -8.19	-0.3	5.3	1407
4	i	94	10	37	42 -10.2	-0.3	5.22	1292	4		6 9		6 37	42 -8.28	-0.31	5.3	1407
4	1	94	13	37	42 -10.4	-0.3	5.23	1294	4		6 9		9 37	42 -8.37	-0.31	5.29	1410
4	1	94	16	37	42 -10.2	-0.3	5.23	1297	7		6 9		2 37	42 -8.51	-0.31	5.29	1413
4	1	94	19	37	42 -10.2	-0.3	5.23	1300	7		7 9		1 37	42 -8.69	-0.31	5.29	1415
4	'n	94	22	37	42 -10.2	-0.3	5.23	1303	7		7 9		4 37	42 -8.8	-0.31	5.29	1417
	ż	94	1	37	42 -10.1	-0.3	5.24	1306	4		7 9		7 37	42 -9	-0.31	5.29	1420
4	5	94	4	37	42 -9.91	~0.3	5.24	1310	ž		7 9		0 37	42 -9.12	-0.3	5.29	1422
4	2	94	7	37	42 -9.71	-0.3	5.24	1311	4		7 9		3 37	42 -9.17	-0.31	5.29	1423
7	2	94	10	37	42 -9.7	-0.3	5.24	1314	4		7 9		6 37	42 -9.15	-0.31	5.29	1426
7.	2	94	13	37	42 -9.08	-0.3	5.25	1319	į.		7 9		9 37	42 -9.15	~0.31	5.29	1427
7.	ž	94	16	37	42 -8.69	-0.3	5.25	1322	4		7 9		2 37	42 -9.27	-0.31	5.29	1431
7.	2	94	19	37	42 -8.48	-0.3	5.25	1325	4		8 9		1 37	42 -9.4	-0.31	5.29	1433
4	2	94	22	37	42 -8.27	-0.3	5.25	1328	4		8 9		4 37	42 -9.59	~0.31	5.3	1437
7.	3	94	1	37	42 -8.24	-0.3	5.25	1331	4		8 9		7 37	42 -9-91	-0.31	5.3	1441
7	3	94	4	37	42 -8.07	-0.3	5.25	1334	4		8 9		0 37	42 -10.1	-0.31	5.3	1440
7	3	94	7	37	42 -8.38	-0.3	5.25	1336	4		8 94		3 37	42 -10.2	-0.31	5.3	1442
Ž	3	94	10	37	42 -6.76	-0.3	5.25	1342	4		8 94		6 37	42 -10.1	-0.31	5.3	1443
Ž	3	94	13	37	42 -5.42	-0.3	5.25	1346	4		8 94		9 37	42 -10-1	-0.31	5.31	1444
4	<b>3</b>	94	16	37	42 -4.31	-0.3	5.25	1349	4		8 94		2 37	42 -10.3	-0.31	5,3	1446
Ž	3	94	19	37	42 -3.33	-0.3	5.25	1352	4		9 94		1 37	42 -10.5	~0.31	5.3	1448
Ž	รี	94	22	37	42 -3.47	-0.3	5.25	1352	4		9 94		4 37	42 -10.8	-0.31	5.3	1451
Ž	4	94	1	37	42 -3.36	-0.3	5.26	1355	4		9 9		7 37	42 -11.1	-0.31	5.3	1453
4	4	94	4	37	42 -3.26	-0.3	5.26	1359	4		9 94		0 37	42 -11.2	~0.31	5.29	1454
4	4	94	7	37	42 -3.64	-0.3	5.26	1360	4		9 94		3 37	42 -11.1	-0.31	5.29	1452
4	4	94	10	37	42 -3.73	-0.3	5.26	1364	4		9 94		6 37	42 -10.9	-0.31	5.28	1456
Ž	4	94	13	37	42 -3.7	-0.3	5.27	1365	4		9 94		9 37	42 -10.8	-0.31	5.28	1459
4	4	94	16	37	42 -4.06	-0.3	5.27	1367	4		9 94		2 37	42 -10.9	-0.31	5.28	1461
4	4	94	19	37	42 -4.5	-0.3	5.27	1370	4	10		_	1 37	42 -11	-0.31	5.27	1462
4	4	94	22	37	42 -4-91	-0.3	5.27	1375	4	10			4 37	42 ~11	-0.31	5.26	1463
7	-	, ,		-,	,	<del></del>			•	-	-						

Appendix D

Gambell Observation Well #2

Mm	Dd	Υу	Hr	Mn	Ss Airī	WaterT	Stage	Conductivity	Mm	Dd	Yy	Нг	Mn	Ss AirT	WaterT	Stage (	onductivity
4	10	94	7	37	42 -11.3	-0.31	5.26	1466	4	15	94	13	37	42 -13.7	-0.31	5.08	1491
7	10	94	10	37	42 -11.3	-0.31	5.25	1468	4	15		16	37	42 -13.3	-0.31	5.08	1497
4	10	94	13	37	42 -11.2	-0.31	5.24	1469	Ž	15		19	37	42 -13.2	-0.31	5.08	1499
4	10	94	16	37	42 -11	-0.31	5.24	1469	4	15		22	37	42 -13.7	~0.31	5.08	1493
7	10	94	19	37	42 -10.8	-0.31	5.23	1471	2	16		1	37	42 -14.3	-0.31	5.08	1501
4	10	94	22	37	42 - 10.8	-0.31	5.23	1466	7	16		4	37	42 -14.9	-0.31	5.08	1504
4	11	94	1	37	42 -10.8	-0.31	5.22	1473	7.	16		7	37	42 -15.7	-0.31	5.08	1507
4	11	94	4	37	42 -10.8	-0.31	5.21	1475	4	16		10	37	42 -16.2	-0.31	5.08	1509
,	11	94	7	37	42 -11.3	-0.31	5.21	1476	7.	16		13	37	42 ~15.5	-0.31	5.09	1505
4	11	94	10	37	42 -11.5	^0.31	5.2	1472	4	16		16	37	42 -14.9	-0.32	5.09	1506
7	11	94	13	37	42 -11.2	-0.31	5.19	1477	7	16		19	37	42 -14.6	-0.31	5.09	1508
4	11	94	16	37	42 -10.9	-0.31	5.19	1477	7	16		22	37	42 -14.9	-0.31	5.09	1509
7	11	94	19	37	42 -10.7	-0.31	5.18	1478	7.	17		1	37	42 -15.5	-0.32	5.09	1511
4	11	94	22	37	42 -10.8	-0.31	5.18	1472	4	17		4	37	42 -16.1	-0.32	5.1	1514
4	12	94	1	37	42 -10.8	-0.31	5.17	1478	7.	17		7	37	42 -16.6	-0.32	5.1	1517
4	12	94	4	37	42 -11.8	-0.31	5.16	1480	7	17		10	37	42 -16.7	-0.32	5.1	1517
4	12	94	7	37	42 -12.3	-0.31	5.16	1483	4	17		13	37	42 -15.9	-0.31	5.1	1515
4	12	94	10	37	42 -12.5	-0.31	5.15	1482	7	17		16	37	42 -15.1	-0.32	5.11	1515
7	12	94	13	37	42 -12.1	-0.31	5.15	1482	7	17		19	37	42 -14.7	-0.32	5.11	1515
4	12	94	16	37	42 -11.8	-0.31	5.14	1481	7	17		22	37	42 -14.7	~0.32	5.11	1516
- <del>'4</del>	12	94	19	37	42 -11.6	-0.31	5-14	1482	7	18		1	37	42 -15.1	-0.32	5.12	1512
7	12	94	22	37	42 -11.7	-0.31	5.13	1482	7	18		4	37	42 -15.5	-0.32	5.12	1519
7	13	94	1	37	42 -12.2	-0.31	5.13	1483	4	18		7	37	42 -15.7	-0.32	5.12	1518
4	13	94	4	37	42 -12.7	-0.31	5.12	1486	4	18		10	37	42 -15.7	-0.32	5.12	1518
7.	13	94	7	37	42 -13	-0.31	5.12	1486	4	18		13	37	42 - 15	-0.32	5.12	1520
4	13	94	10	37	42 -12-9	-0.31	5.12	1485	4	18		16	37	42 -14.3	-0.32	5.13	1514
7.	13	94	13	37	42 -12.4	-0.31	5.11	1485	4	18		19	37	42 -13-8	-0.32	5.13	1514
4	13	94	16	37	42 -11.9	-0.31	5.11	1486	4	18		22	37	42 -13.6	-0.32	5.13	1521
4	13	94	19	37	42 -11-6	-0.31	5.1	1485	4	19		1	37	42 -13.6	-0.32	5.13	1522
7.	13	94	22	37	42 -11.6	-0.31	5.1	1486	4	19		4	37	42 -13-9	-0.32	5.13	1523
4	14	94	1	37	42 ~11.8	-0.31	5.1	1487	4	19		7	37	42 -14-2	-0.32	5.13	1522
7	14	94	4	37	42 -12.1	-0.31	5.1	1489	4	19		10	37	42 -14.3	-0.32	5.12	1523
7	14	94	7	37	42 -12.6	-0.31	5.09	1490	4	19		13	37	42 -13.7	-0.32	5.12	1524
4	14	94	10	37	42 -13	-0.31	5.09	1490	4	19		16	37	42 -13.1	-0.32	5.12	1524
7	14	94	13	37	42 -12.6	-0.31	5.09	1490	4	19		19	37	42 -12.7	-0.32	5.12	1525
7.	14	94	16	37	42 -12.2	-0.31	5.09	1484	4	19		22	37	42 -12.5	-0.32	5.12	1525
4	14	94	19	37	42 -12	-0.31	5.08	1491	4	20		1	37	42 -12.6	-0.32	5.12	1525
4	14	94	22	37	42 - 12.3	-0.31	5.08	1491	ž	20		4	37	42 -12.9	-0.32	5.12	1525
7	15	94	1	37	42 -12.9	-0.31	5.08	1495	4	20		7	37	42 - 13.1	-0.32	5.12	1518
4	15	94	4	37	42 -13.5	-0.31	5.08	1495	Z	20		10	37	42 -13.2	-0.32	5.11	1525
7	15	94	7	37	42 -14	-0.31	5.08	1497	4	20		13	37	42 -12.7	-0.32	5.11	1524
ž	15	94	10	37	42 -14.2	-0.31	5.08	1498	4	20		16	37	42 -12.2	~0.32	5.11	1526
4	1,5	, 4		٠,	774 1715		2.00	1775	•					·- ·			

Appendix D

Gambell Observation Well #2

Mm	Ðd	Υу	Ηг	Mn	Ss AirT	WaterT	Stage	Conductivity	Mm	D	d Y	у	Ħſ	Mn	Ss Airī	Waterĭ	Stage	Conductivity
4	20	94	19	37	42 -11.8	-0.32	5.11	1528	4	2	6 9	4	t	37	42 -9.22	-0.32	5.06	1538
4	20	94	22	37	42 -11.6	-0.32	5.1	1527	4		6 9		4	37	42 -9.44	-0.31	5.06	1538
7	21	94	1	37	42 -11.7	-0.32	5.1	1522	4		6 9		7	37	42 -9.61	~0.32	5.06	1538
4	21	94	4	37	42 -11.9	-0.32	5.1	1527	4		6 9		10	37	42 -9.55	-0.31	5.05	1538
4	21	94	7	37	42 -12.2	-0.32	5.09	1526	4		6 9		13	37	42 -9.1	-0.31	5.05	1538
4	21	94	10	37	42 -12.2	-0.31	5.09	1527	4		6 9		16	37	42 -8.68	-0.31	5.05	1539
4	21	94	13	37	42 -11.8	-0.32	5.09	1526	4	2	6 9	4	19	37	42 -8.34	-0.31	5.05	1541
4	21	94	16	37	42 -11.3	-0.31	5.08	1527	4	2	6 9	4	22	37	42 -8.23	-0.31	5.05	1542
Ž.	21	94	19	37	42 ~10.9	-0.32	5.08	1528	4	2	7 9	4	1	37	42 -8.22	-0.31	5.05	1541
4	21	94	22	37	42 -10.8	-0.32	5.08	1528	4	2	7 9	4	4	37	42 -8.26	-0.31	5.04	1542
4	22	94	1	37	42 -11.1	-0.31	5.08	1529	4	2	7 9	4	7	37	42 -8.3	-0.32	5.04	1542
4	22	94	4	37	42 -11-4	-0.31	5.07	1527	4	2	7 9	4	10	37	42 -8.25	-0,31	5.04	1543
4	22	94	7	37	42 -11.7	-0.31	5.07	1528	4	2	7 9	4	13	37	42 -8.01	-0.32	5.04	1543
4	22	94	10	37	42 -11.8	-0.32	5.07	1521	4	2			16	37	42 -7.65	-0.31	5.03	1544
4	22	94	13	37	42 -11.4	-0.31	5.06	1527	4	2			19	37	42 -7.33	-0.31	5.03	1545
4	22	94	16	37	42 -11	~0.32	5.06	1529	4	2		4	22	37	42 -7.22	-0.31	5.03	1544
4	22	94	19	37	42 -10.7	-0.31	5.06	1530	4		8 9		1	37	42 -7.3	-0.31	5.03	1545
4	22	94	22	37	42 -10.6	-0.31	5.06	1529	4		8 9		4	37	42 -7.49	-0.31	5.02	1546
4	23	94	1	37	42 -10.9	-0.31	5.06	1530	4		8 9		7	37	42 -7.75	-0.31	5.02	1546
4	23	94	4	37	42 -11.3	-0.31	5.05	1530	4		8 9		10	37	42 -7.81	-0.31	5.02	1544
4	23	94	7	37	42 -11.6	-0.31	5.05	1531	4		8 9		13	37	42 -7.65	-0.31	5.02	1545
4	23	94	10	37	42 -11.6	-0.31	5.05	1530	4		8 9		16	37	42 -7.33	-0.31	5.01	1546
4	23	94	13	37	42 -11.2	-0.32	5.05	1531	4		8 9		19	37	42 -6.93	-0.31	5.01	1546
4	23	94	16	37	42 -10.7	-0.31	5.05	1531	4		8 9		22	37	42 -6.65	-0.31	5.01	1544
4	23	94	19	37	42 -10.4	-0.31	5.05	1532	4		9 9	-	1	37	42 -6.6	-0.31	5.01	1546 1545
4	23	94	22	37	42 ~10.4	-0.32	5.05	1532	4		9 9		4	37	42 -6.61	-0.31	5.01	1546
4	24	94	1	37	42 -10.7	-0.32	5.05	1531	4		9 9		7	37	42 ~6.63	-0.31	5.01	1547
4	24	94	4	37	42 -10.7	-0.32	5.05	1531	4		9 9		10	37	42 -6.43 42 -5.82	-0.31 -0.31	5.01 5.01	1548
4	24	94	7	37	42 -10.8	-0.31	5.05	1532	4		9 9		13	37 37	42 -5.32	-0.31	5.01	1546
4	24	94	10	37	42 -10-7	-0.31	5.05	1532	4		9 9		16 19	37	42 -5.2	-0.31	5.01	1547
4	24	94	13	37	42 -10.5	-0.32	5.05	1532 1534	4		9 9		22	37	42 -5.34	-0.31	5.01	1548
4	24	94	16	37	42 -10.1	-0.31	5.05	1534	4		0 9	-	1	37	42 -5.68	-0.31	5.02	1550
4	24	94	19	37	42 -9.74	-0.31 -0.31	5.05 5.05	1534	4		0 9		4	37	42 -6.03	-0.31	5.02	1549
4	24	94	22	37 37	42 -9.61 42 -9.7	-0.31	5.05	1535	7		0 9		7	37	42 -6.28	-0.32	5.02	1548
4	25	94 94	1	37	42 -10.1	~0.31	5.05	1535	4		0 9		10	37	42 -6.39	-0.32	5.03	1548
4	25 25	94	4 7	37	42 -10-1	-0.32	5.05	1537	4		0 9		13	37	42 -6.31	-0.31	5.03	1549
4	25	94	10	37 37	42 -10.4	-0.31	5.05	1536	7		0 9		16	37	42 -6.08	-0.32	5.04	1548
- 4	25	94	13	37	42 -9.93	-0.32	5.05	1535	4		0 9		19	37	42 -5.97	-0.32	5.05	1550
- 4	25	94	16	37	42 -9.53	-0.32	5.05	1537	Ž		0 9		22	37	42 -6.11	-0.32	5.05	1550
4	25	94	19	37	42 -9.22	-0.32	5.06	1538	5		1 9		1	37	42 -6.31	-0.32	5.06	1552
4	25	94	22	37	42 -9.22	-0.32	5.06	1537	5		1 9		4	37	42 -6.46	-0.31	5.06	1553
4	43	74	~~	٦,	46 7.1	0.72	٥٠.٠٠	133,	•		. ,	*	•					

Appendix D

Gambell Observation Well #2

Mm	Dď	Υу	Нг	Mn	Ss AirT	WaterT	Stage	Conductivity	₩m	Do	ł Yy	Hr	Mn	Ss AirT	WaterT	Stage Co	nductivîty
5	1	94	7	37	42 -6.56	-0.32	5.07	1551	5	,	94	13	37	42 -3,04	-0.32	5.28	1534
5	1	94	10	37	42 -6.47	-0.32	5.08	1552	5	ě		16	37	42 -2.91	-0.32	5.28	1533
ś	1	94	13	37	42 -6.23	-0.32	5.09	1552	5	ě		19	37	42 -2.76	-0.32	5.29	1532
5	1	94	16	37	42 -5.9	~0.32	5.1	1552	5	è		22	37	42 -2.84	~0.32	5.29	1532
5	1	94	19	37	42 -5.73	-0.32	5.1	1552	5	7		1	37	42 -3	-0.32	5.3	1532
5	i	94	22	37	42 -5.81	-0.32	5.11	1552	5	7	94	4	37	42 -3.14	-0.32	5.3	1530
5	ź	94	1	37	42 -6.06	-0.32	5.12	1552	5	7	7 94	7	37	42 -3.27	-0.32	5.3	1532
5	2	94	4	37	42 ~6.18	~0.32	5,12	1551	5	7	94	10	37	42 -3.3	-0.32	5.3	1529
5	2	94	7	37	42 -6.27	-0.32	5.13	1551	5	7	94	13	37	42 -3.23	-0.32	5.31	1530
5	2	94	10	37	42 -6.23	-0.32	5.14	1550	5	7	7 94	16	37	42 -3.05	~0.32	5.31	152 <del>9</del>
5	2	94	13	37	42 -6.01	-0.32	5.14	1550	5	7	94	19	37	42 -2.96	-0.32	5.31	1529
5	2	94	16	37	42 -5.76	-0.32	5.15	1549	5	7		22	37	42 -3.03	-0.32	5.31	1528
5	2	94	19	37	42 -5.55	~0.32	5.16	1547	5	8		1	37	42 -3.08	-0.32	5.31	1529
5	2	94	22	37	42 -5.45	-0.32	5.17	1546	5	8		4	37	42 -3.12	-0.32	5.31	1528
5	3	94	1	37	42 -5.46	-0.32	5.17	1544	5	8		7	37	42 -3_17	-0.32	5.31	1530
5	3	94	4	37	42 -5.54	-0.32	5.18	1540	5	8		10	37	42 -3.1	-0.32	5.31	1527
5	3	94	7	37	42 -5.54	~0.32	5.18	1543	5	8		13	37	42 -2.91	~0.32	5.31	1527
5	3	94	10	37	42 -5.45	-0.32	5.19	1541	5			16	37	42 -2.58	-0.32	5.31	1529
5	3	94	13	37	42 -5.24	-0.32	5.19	1540	5	8		19	37	42 -2.39	-0.32	5.31	1527
5	3	94	16	37	42 -4.89	~0.32	5.2	1540	5	8		55	37	42 -2-45	-0.32	5.3	1528
5	3	94	19	37	42 -4.49	-0.32	5.2	1539	5	9		1	37	42 -2-66	-0.32	5.3	1530
5	3	94	22	37	42 -4.15	-0.32	5.2	1539	5	5		4	37	42 -2.84	-0.32	5.3	1530
5	4	94	1	37	42 -4.18	-0.32	5.2	1538	5	9		7	37	42 -2.99	~0.32	5.3	1531 1531
5	4	94	4	37	42 -4.32	-0.32	5.21	1538	5	9		10	37	42 -2.98	-0.32	5.29	1529
5	4	94	7	37	42 -4.41	-0.32	5.21	1538	5	9		13	37	42 -2.74	~0.32 -0.32	5.29 5.28	1530
5	4	94	10	37	42 -4-37	-0.32	5-21	1538	5	- 5		16	37 37	42 -2.39	-0.32	5.28	1531
5	4	94	13	37	42 -4.02	-0.32	5.22	1538	5 5	5	-	19 22	37 37	42 -2.14 42 -2.15	-0.32	5.28	1529
5	4	94	16	37	42 -3.53	-0.32	5.22	1539	5	10		1	37 37	42 -2.15	-0.32	5.28	1528
5	4	94	19	37 37	42 -3.29 42 -3.3	-0.32	5.22	1539 1536	5	10		4	37	42 -3.07	-0.32	5.28	1529
5	4	94	22	37 37	42 -3.3 42 -3.44	-0.32 -0.32	5.23 5.23	1537	5	10		7	37	42 -3.31	-0.32	5.29	1526
5	5	94 94	1	37	42 ~3.44	-0.32	5.23	1536	5	10		10	37	42 -3.15	-0.32	5.29	1526
5 5	5	94	7	37 37	42 -3.76	-0.32 -0.32	5.24	1536	ś	10		13	37	42 -2.89	-0.32	5.3	1525
5	5	94	10	37	42 -3.67	-0.32	5.24	1534	ś	10		16	37	42 -2.64	-0.32	5.31	1522
5	5	94	13	37	42 -3.43	-0.32	5.24	1536	5	10		19	37	42 -2.74	-0.32	5.31	1522
5	5	94	16	37	42 -3.18	-0.32	5.25	1537	5	10		ZŹ	37	42 -2.86	-0.32	5.32	1519
5	5	94	19	37	42 -2.96	-0.32	5.25	1537	ś	1		1	37	42 -2.93	-0.32	5.32	1518
5	5	94	22	37	42 -2.85	-0.32	5.26	1537	5	11		4	37	42 -2.95	-0.32	5.33	1516
5	6	94	1	37	42 -2.92	-0.32	5.26	1536	ś	11	. ,	7	37	42 -2.94	-0.32	5.33	1515
5	6	94	ź	37	42 -3.07	-0.32	5.26	1535	ś	11		10	37	42 -2.8	-0.32	5.33	1515
5	6	94	7	37	42 -3.21	-0.32	5.27	1535	5	11		13	37	42 -2.63	-0.32	5.33	1514
5	6	94	10	37	42 -3.22	-0.32	5.27	1533	5	11		16	37	42 -2.52	-0.32	5.33	1512
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Appendix D

Gambell Observation Well #2

Man	Dd	Υу	Hr	Mn	Ss Airī	WaterT	Stage	Conductivity	Mm	Dd	Yу	Ħг	Mn	Ss Airī	₩aterT	Stage (	Conductivity
5	11	94	19	37	42 -2.5	-0.32	5.33	1509	5	17	94	1	37	42 -0.54	-0.33	5.46	1457
ś	11	94	22	37	42 -2.45	-0.32	5.32	1509	5	17		4	37	42 -0.77	-0.33	5.47	1415
5	12	94	1	37	42 -2.5	-0.32	5.32	1508	5	17	-	7	37	42 -0.93	-0.33	5.48	1418
ś	12	94	4	37	42 -2.58	-0.32	5.32	1508	5	17		10	37	42 -0.93	-0.33	5.48	1418
s s	12	94	7	37	42 -2.62	-0.32	5.32	1505	5	17		13	37	42 -0.78	-0.33	5.48	1428
Š	12	94	10	37	42 -2.62	-0.32	5.32	1506	5	17	94	16	37	42 -0.66	-0.33	5.49	1432
5	12	94	13	37	42 -2.47	-0.32	5.31	1505	5	17	94	19	37	42 -0.69	-0.33	5.49	1433
5	12	94	16	37	42 -2.04	-0.32	5.31	1505	5	17	94	22	37	42 ~0.8	-0.33	5.5	1426
5	12	94	19	37	42 -1.78	-0.32	5.32	1504	5	18	94	1	37	42 -0.86	-0.33	5.49	1424
5	12	94	22	37	42 -1.64	-0.32	5.32	1504	5	18	94	4	37	42 -0.9	-0.33	5.49	1424
5	13	94	1	37	42 -1.82	-0.32	5.31	1503	5	18		7	37	42 -0.83	-0.33	5.5	1423
5	13	94	4	37	42 -2.03	-0.32	5.31	1501	5	18		10	37	42 -0.74	-0.33	5.5	1427
5	13	94	7	37	42 -2.16	-0.32	5.31	1500	5	18		13	37	42 -0.5	-0.32	5.5	1373
5	13	94	10	37	42 -2.1	-0.32	5.31	1499	5	18		16	37	42 -0 <b>.33</b>	-0.32	5.51	1364
5	13	94	13	37	42 -1.95	-0.32	5.31	1496	5	18		19	37	42 -0.22	-0.33	5.52	1483
5	13	94	16	37	42 -1.78	-0.32	5.32	1495	5	18		22	37	42 -0.16	-0.33	5.54	1300
5	13	94	19	37	42 -1-74	-0.32	5.33	1492	5	19		1	37	42 -0.13	-0.33	5.55	1270
5	13	94	22	37	42 -1.8	-0.32	5.33	1491	5	19		4	37	42 -0.12	-0.33	5.56	1317
5	14	94	1	37	42 -1.89	-0.32	5.32	1491	5	19		7	37	42 -0.11	-0.33	5.57	1301
5	14	94	4	37	42 -1.89	-0.32	5.32	1490	5	19		10	37	42 -0.1	-0.33	5.58	1293
5	14	94	7	37	42 -1.87	-0.32	5.33	1489	5	19		13	37	42 -0.06	-0.33	5.58	1492
5	14	94	10	37	42 -1.75	-0.32	5.34	1489	2	19		16	37	42 -0.03	-0.33	5.6	1448 1548
5	14	94	13	37	42 -1.35	-0.32	5.32	1490	ž	19		19	37	42 ~0.02	-0.32 -0.33	5.63 5.67	1547
5	14	94	16	37	42 -0.72	-0.32	5.34	1489	2	19		22	37	42 -0.01 42 -0.01	-0.33	5.71	1544
5	14	94	19	37	42 -0.42	-0.32	5.35	1489	2	20		1	37 37	42 -0.01	-0.33	5.73	1550
5	14	94	22	37	42 -0.3	-0.32	5.35	1486	5 5	20	94	4 7	37	42 -0.02	-0.33	5.76	1552
2	15	94	1	37	42 -0.38	-0.32	5.35	1486	5	20		16	37	42 0	-0.33	5.77	1510
5	35	94	4	37	42 -0.56	-0.32	5.36	1483 1483	2	20		13	37	42 0.05	-0.32	5.79	1524
5	15	94	7	37	42 -0.74	-0.32 -0.32	5.37 5.38	1482	5	20		16	37	42 0.03	-0.32	5.82	1548
5	15	94	10	37 37	42 -0.65 42 -0.47	-0.32	5.38	1479	,	20		19	37	42 0.15	-0.32	5.88	1518
5 5	15	94 94	13 16	37	42 -0.37	-0.32	5.39	1415	5	20		22	37	42 0.14	-0.32	5.94	1487
2	15 15	94	19	37	42 -0.33	-0.32	5.4	1453	5	21	94	1	37	42 0.08	-0.32	5.99	1482
5	15	94	22	37	42 -0.33	-0.32	5.4	1446	5	21	94	4	37	42 0.05	-0.32	6.03	1467
9	16	94	1	37	42 -0.35	-0.33	5.41	1439	ś	21	94	7	37	42 0.03	-0.31	6.06	1463
5	16	94	4	37	42 -0.4	-0.33	5.41	1438	5	21		10	37	42 0.1	-0.31	6.08	1481
ξ.	16	94	7	37	42 ~0_48	-0.32	5.42	1437	5	21		13	37	42 0.17	-0.31	6.1	1469
- 2	16	94	10	37	42 -0.47	-0.33	5.42	1439	5	21	94	16	37	42 0.27	-0.31	6.14	1486
2	16	94	13	37	42 -0.35	-0.33	5.43	1444	5	21		19	37	42 0.32	-0.31	6.19	1520
,	16	94	16	37	42 -0.28	-0.33	5.44	1446	5	21	94	22	37	42 0.18	~0.31	6.26	1500
5	16	94	19	37	42 -0.25	-0.33	5.45	1429	5	22		1	37	42 0.09	-0.31	6.32	1492
5	16	94	22	37	42 -0.32	-0.33	5.46	1464	5	22		4	37	42 0,04	-0.3	6.36	1506
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Appendix D

Gambell Observation Well #2

Mm	Dd	Υу	Нг	Ħп	Ss AirT	WaterT	Stage	Conductivity	Mm	рd	Υy	Hr	Mn	S& AirT	WaterT	Stage (	Conductivity
5	22	94	7	37	42 0.04	-0.31	6.39	1518	5	27	94	13	37	42 0.47	-0.31	6.43	1756
5	22	94	10	37	42 0.13	-0.31	6.4	1527	Ś	27		16	37	42 0.7	-0.31	6.45	1792
5	22	94	13	37	42 0.19	-0.31	6.42	1539	5	27	94	19	37	42 0.54	-0.31	6.48	1785
ś	22	94	16	37	42 0.16	-0.31	6.43	1540	5	27	94	22	37	42 0.37	-0.31	6.5	1771
5	22	94	19	37	42 0.09	-0.31	6.44	1530	5	28	94	1	37	42 0.12	-0.31	6.52	1736
5	22	94	55	37	42 -0.02	-0.31	6.45	1515	5	28	94	4	37	42 -0.01	-0.31	6.53	1721
Ś	23	94	1	37	42 -0.18	-0-31	6.46	1509	5	28	94	7	37	42 ~0.01	-0.31	6.54	1733
Ś	23	94	4	37	42 -0.34	-0.31	6.46	1534	5	28	94	10	37	42 0.37	-0.31	6.53	1739
5	23	94	7	37	42 -0.42	-0.31	6.46	1530	5	28	94	13	37	42 0.89	-0.31	6.54	1826
5	23	94	10	37	42 -0.42	-0.31	6.45	1535	5	28	94	16	37	42 1.12	-0.31	6.56	1828
5	23	94	13	37	42 -0.22	-0.31	6.45	1523	5	28	94	19	37	42 1.21	-0.31	6.6	1803
5	23	94	16	37	42 -0.02	-0.31	6.45	1506	5	28	94	22	37	42 1.06	-0.32	6.66	1775
5	23	94	19	37	42 -0.08	-0.31	6.45	1498	5	29	94	1	37	42 0.15	-0.32	6.72	1796
5	23	94	22	37	42 -0.24	-0.31	6.44	1499	5	29	94	4	37	42 ~0.21	-0.32	6.74	1768
5	24	94	1	37	42 -0.46	-0.31	6.44	1503	5	59	94	7	37	42 -0.18	-0.32	6.76	1755
5	24	94	4	37	42 -0.62	-0.31	6.44	1504	5	29	94	10	37	42 0.16	-0.32	6.77	1751
5	24	94	7	37	42 -0.71	-0.31	6.43	1517	5	29	94	13	37	42 0.63	-0.32	6.79	1785
5	24	94	10	37	42 -0.71	-0.31	6.42	1526	5	29	94	16	37	42 0.84	-0.32	6.8	1800
5	24	94	13	37	42 -0.41	-0.31	6.41	1541	5	29	94	19	37	42 0.7	-0.32	6.83	1791
5	24	94	16	37	42 -0.11	-0.31	6.4	1524	5	29	94	22	37	42 0.2	-0.32	6.84	1775
5	24	94	19	37	42 -0.11	-0.31	6-4	1550	5	30	94	1	37	42 -0.15	-0.32	6.85	1759
5	24	94	55	37	42 -0.49	-0.31	6.39	1558	5	30	94	4	37	42 -0.3	-0.32	6.86	1754 1751
5	25	94	1	37	42 -0.81	-0.31	6.39	1566	5	30	94	7	37	42 -0.34	-0.32 -0.32	6.87 6.86	1748
5	25	94	4	37	42 -1.06	-0.31	6.38	1578	5	30	94	10	37 37	42 -0.22	-0.32	6.86	1750
5	25	94	7	37	42 -1.17	-0.31	6.38	1566	5 5	30 30	94 94	13	37	42 0.03 42 0.14	-0.32	6.86	1760
5	25	94	10	37	42 -0.91	-0.31	6.37	1596	5	30	94	16 19	37 37	42 0.14	-0.32	6.86	1763
5	25	94	13	37	42 -0.3	-0.31	6.36	1632 1689	5	30	94	22	37	42 -0.2	-0.32	6.86	1761
5	25	94	16	37	42 0.17	-0.31	6.36 6. <b>3</b> 7	1676	5	31	94	1	37	42 -0.41	-0.32	6.85	1779
5	25	94 94	19 22	37 37	42 0.24 42 0.09	-0.31 -0.31	6.38	1657	5	31	94	4	37	42 -0.43	-0.32	6.84	1778
5 5	25		3	37		-0.31	6.39	1655	5	31	94	7	37	42 -0.31	-0.31	6.83	1776
_	26	94 94	4	37	42 -0.2 42 -0.37	-0.31	6.39	1644	ş -	31	94	10	37	42 -0.09	-0.31	6.83	1770
\$ 5	26 26	94	7	37	42 -0.37	-0.31	6.4	1640	ś	31	94	13	37	42 0.29	-0.31	6.82	1795
5	26	94	10	37	42 -0.18	~0.3	6.39	1646	5	31	94	16	37	42 0.58	-0.31	58.6	1814
5	26	94	13	37	42 D.22	-0.3	6.4	1668	ś	31	94	19	37	42 0.82	-0.31	6.83	1803
5	26	94	16	37	42 0.3	-0.31	6.4	1667	5	31	94	22	37	42 0.74	-0.31	6.86	1787
5	26	94	19	37	42 0.18	-0.3	6.41	1670	6	1	94	1	37	42 0.41	-0.31	6.87	1772
Ś	26	94	22	37	42 0.10	-0.31	6.42	1648	6	1	94	4	37	42 0.05	-0.31	6.88	1760
5	27	94	1	37	42 -0.18	-0.31	6.43	1652	6	ì	94	7	37	42 -0.06	-0.31	6.87	1750
5	27	94	4	37	42 -0.27	-0.31	6.43	1662	6	1	94	10	37	42 0.09	-0.31	6.88	1741
5	27	94	7	37	42 -0.3	-0.31	6.43	1664	6	1	94	13	37	42 0.45	-0.31	6.87	1732
ś	27	94	10	37	42 -0.03	-0.31	6.43	1675	6	1	94	16	37	42 1.03	-0.31	6.89	1769
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Appendix D

Gambell Observation Well #2

Mm	Dd	Υу	Ħг	Mn	Ss Aîrĭ	WaterT	Stage	Conductivity	Mm	D	d Y	У	Hr	Нn	Ss	AirT	WaterT	Stage	Conductivity
6	1	94	19	37	42 1.3	-0.31	6.91	1779	6		7 9	4	1	37	42	2.21	-0.31	8.22	1778
6	1	94	22	37	42 1.04	-0.31	6.94	1755	6		7 9	4	4	37	42	1.65	-0.31	8.27	1766
6	2	94	1	37	42 0.42	-0.31	6.97	1735	6		7 9	4	7	37	42	1.57	-0.31	8.3	1758
6	2	94	4	37	42 0.18	-0.31	6.98	1717	6		7 9	4	10	37	42	2.15	-0.31	8.32	1 <b>78</b> 5
6	2	94	7	37	42 0.19	-0.31	6.99	1706	6		7 9	4	13	37	42	2.89	-0.31	8.34	1772
6	2	94	10	37	42 0.46	-0.31	7	1705	6		7 9	4	16	37	42	3.01	-0.31	8.38	1756
6	Z	94	13	37	42 3.01	-0.31	7.12	1726	6		7 9	4	19	37	42	2.57	-0.31	8.46	1754
6	2	94	16	37	42 2.07	-0.31	7.02	1708	6		79	4	22	37	42		-0.31	8.55	1748
6	2	94	19	37	42 1.72	-0.31	7.07	1751	6	1	89		1	37	42		-0.31	8.62	1742
6	2	94	22	37	42 1.15	-0.31	7.14	1746	6		89		4	37	42		-0.31	8,64	1741
6	3	94	1	37	42 0.61	-0.32	7.19	1731	6		8 9		7	37	42		-0.31	8.68	1735
6	3	94	4	37	42 0.33	-0.32	7.21	1723	6		89		10	37	42		-0.31	8.67	1729
6	3	94	7	37	42 0.37	-0.32	7.24	1709	6		89		13	37	42		-0.31	8.68	1745
6	3	94	10	37	42 0.69	-0.32	7.25	1709	6		89		16	37	42		-0.31	8.71	1741
6	3	94	13	37	42 0.79	-0.32	7.27	1726	6		B 9		19	37	42		-0.31	8.76	1725
6	3	94	16	37	42 0.98	-0.32	7.29	1739	6		B 9		22	37	42		-0.31	8.82	1718
6	3	94	19	37	42 0.92	-0.32	7.34	1743	6		9 9		1	37	42		-0.31	8.87	1713
6	3	94	22	37	42 0.68	-0.31	7.37	1735	6		9 9		4	37	42		-0.31	8.89	1716
6	4	94	1	37	42 0.41	-0.32	7.4	1724	6		9 9		7	37	42		-0.31	8.91	1711
6	4	94	4	37	42 0.27	-0.32	7.43	1724	6		9 9		10	37	42		-0.3	8.92	1707
6	4	94	7	37	42 0.26	-0.31	7.47	1716	6		9 9		13	37	42		-0.31	8.96	1719
6	4	94	10	37	42 0.5	-0.32	7.48	1722	6		9 9		16	37	42		-0.3	8.97	1713
6	4	94	13	37	42 0.66	-0.32	7.49	1732	6		9 9		19	37	42		-0.3	9.06	1694
6	4	94	16	37	42 0.86	-0.32	7.52	1741	6		9 9		22	37	42		-0.3	9,19	1679
6	4	94	19	37	42 0.78	-0.31	7.56	1739	6	11			1	37	42		-0.3	9.28	1688 1688
6	4	94	22	37	42 0.53	-0.31	7.59	1733	6	11			4	37 37	42		-0.3 -0.3	9.32 9.33	1684
6	5	94	1	37	42 0.3	-0.31	7.62	1727	6	10			7	37	42		-0.3	9.33	1692
6	5	94	4	37	42 0.13	-0.31	7.63	1727	6	10			10 13	37 37	42 42		-0.3	9.33	1647
6	5	94	7	37	42 0.12	-0.31	7.64	1723	6	10			16	37 37	42		-0.3	9.4	1641
6	5	94	10 13	37 37	42 0,4 42 0,96	-0.31	7.64 7.65	1738 1781	6	10			19	37	42		-0.3	9.46	1632
6	5	94 94	16	37	42 1.39	-0.31 -0.31	7.67	1798	6	10			22	37	42		-0.29	9.57	1631
6	5	94	19	37	42 1.56	-0.31	7.75	1787	6	1			1	37	42		-0.29	9.64	1643
6	5	94	22	37	42 1.36	-0.31	7.82	1775	6	1			4	37	42		-0.3	9.64	1653
6 6	6	94	1	37	42 0.64	-0.31	7.89	1745	6	i			7	37	42		-0.3	9.65	1658
6	6	94	4	37	42 0.04	-0.31	7.92	1733	6	i			10	37	42		-0.3	9.66	1657
6	6	94	7	37	42 0.15	-0.31	7.94	1724	6	i	-		13	37	42		-0.3	9.68	1635
6	6	94	10	37	42 0.26	-0.31	7.96	1782	6	1			16	37	42		-0.29	9.73	1626
6	6	94	13	37	42 1.75	-0.31	7.99	1791	6	1			19	37	42		-0.29	9.87	1625
6	6	94	16	37	42 2.39	-0.31	8	1778	2	1			22	37	42		-0.28	9.96	1630
6	6	94	19	37	42 2.99	-0.31	8.05	1788	6	1			1	37	42		-0.29	10	1642
6	6	94	22	37	42 2.94	-0.31	8.14	1782	6	12			4	37	42		-0.29	10	1652
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Appendix D

Gambell Observation Well #2

Мпа	Dd	Yy	Нг	Mn	Ss AirT	WaterT	Stage	Conductivity	Mm	Dđ	Yy	Hr	Mn	\$s <b>A</b> îrT	WaterT	Stage C	onductivity
6	12	94	7	37	42 3.69	~0.3	9.98	1652	6	17	94	10	37	42 7.99	-0.29	10.61	1546
6	12	94	10	37	42 5.23	-0.3	9.98	1650	6	17		13	37	42 7-1	-0.29	10.64	1535
6	12	94	13	37	42 7.14	-0.3	10	1625	6	17		16	37	42 6.53	-0.29	10.63	1522
6	12	94	16	37	42 8.49	-0.29	10.01	1614	6	17		19	37	42 5.78	-0.29	10.63	1511
6	12	94	19	37	42 8.34	-0.29	10.14	1613	6	17	94	22	37	42 4.82	-0.29	10.63	1501
6	12	94	55	37	42 5.14	-0.29	10.19	1626	6	18	94	1	37	42 4.2	-0.29	10.62	1488
6	13	94	1	37	42 3.72	-0.29	10.2	1637	6	18	94	4	37	42 4.07	~0.29	10.61	1474
6	13	94	4	37	42 3.12	-0.3	10.23	1641	6	18	-	7	37	42 4.02	-0.29	10.6	1458
6	13	94	7	37	42 2.96	-0.3	10.19	1642	6	18	94	10	37	42 3.5	-0.29	10.58	1440
6	13	94	10	37	42 3.8	-0.3	10.2	1633	6	18	94	13	37	42 3.24	-0.29	10.56	1430
6	13	94	13	37	42 5.27	-0.3	10.22	1636	6	18	94	16	37	42 3-29	-0.29	10.53	1423
6	13	94	16	37	42 6	-0.3	10.24	1632	6	18	94	19	37	42 3.28	-0.29	10.52	1401
6	13	94	19	37	42 5.36	-0.29	10.29	1630	6	18	94	22	37	42 3.15	-0.3	10.53	1374
6	13	94	22	37	42 4.11	-0.3	10.34	1625	6	19	94	1	37	42 2.95	-0.29	10.49	1352
6	14	94	1	37	42 4.41	-0.3	10.36	1622	6	19	94	4	37	42 2.81	-0.3	10.48	1334
6	14	94	4	37	42 4.48	-0.3	10,37	1622	6	19	94	7	37	42 2.67	-0.3	10.46	1318
6	14	94	7	37	42 5.17	-0.3	10.36	1624	6	19	94	10	37	42 2.6	-0.29	10.44	1302
6	14	94	10	37	42 6.61	-0.3	10.38	1627	6	19	94	13	37	42 2.58	-0.3	10.42	1284
6	14	94	13	37	42 6.5	-0.3	10.37	1615	6	19	94	16	37	42 2.72	-0.3	10.4	1267
6	14	94	16	37	42 7.02	-0.29	10.41	1617	6	19	94	19	37	42 2.87	-0.3	10.38	1246
6	14	94	19	37	42 5.51	-0.29	10,48	1615	6	19	94	22	37	42 2.79	~0.3	10.37	1221
6	14	94	22	37	42 4.76	-0.3	10.47	1610	6	20	94	1	37	42 2.47	-0.3	10.38	1203
6	15	94	1	37	42 4.34	-0.3	10.5	1613	6	20	94	4	37	42 2.18	-0.3	10.36	1186
6	15	94	4	37	42 4.23	-0.29	10.46	1611	6	20	94	7	37	42 2.04	-0.3	10.34	1169
6	15	94	7	37	42 5.44	~0.3	10,41	1609	6	20		10	37	42 3-19	-0.3	10.31	1164
6	15	94	10	37	42 8.02	-0.29	10.4	1609	6	20	94	13	37	42 3.6	-0.3	10.28	1138
6	15	94	13	37	42 9.7	-0.29	10.41	1592	6	50		16	37	42 3.77	-0.3	10.29	1116
6	15	94	16	37	42 10.83	-0.29	10.46	1590	6	20	94	19	37	42 3.59	~0.3	10.26	1096
6	15	94	19	37	42 8.34	-0.29	10.57	1587	6	20	94	22	37	42 3.08	-0.3	10.28	1083
6	15	94	22	37	42 7.47	-0.29	10.56	1590	6	21	94	1	37	42 2.68	-0.3	10.22	1069
6	16	94	1	37	42 7.15	-0.29	10.58	1591	6	21	94	4	37	42 2.39	-0.3	10.21	1057
6	76	94	4	37	42 6.58	-0.29	10.57	1589	6	21	94	7	37	42 2.3	~0.3	10.22	1043
6	16	94	7	37	42 6-6	-0.29	10.54	1581	6	21	94	10	37	42 2.34	-0.3	10.18	1030
6	16	94	10	37	42 7.97	-0.29	10.51	1582	6	21	94	13	37	42 2-41	-0.3	10.16	1019
									6	21	94	16	37	42 2.61	~0.3	10.15	1008
6	16	94	13	37	42 9.79	-0.29	10.52	1585	6	21	94	19	37	42 2.73	-0.3	10.14	993
6	16	94	16	37	42 11.1	-0.29	10.54	1574	6	21	94	22	37	42 2.65	-0.3	10.13	979 967
6	16	94	19	37	42 10.81	-0.29	10.61	1561	6	22		1	37	42 2.4	-0.3	10.11	956
6	16	94	22	37	42 8.96	-0.29	10.69	1561	6	22		4	37	42 2.25	-0.31	10.12	944
6	17	94	3	37	42 6.91	-0.29	10.7	1558	6	22		7	37	42 2.13	~0.3	10.08	934
6	17	94	4	37	42 5.72	-0.29	10.67	1550	6	22		10	37	42 2.1	-0.3	10.07 10.07	926
6	17	94	7	37	42 6.11	-0.29	10.63	1544	6	22	94	13	37	42 2.13	-0.31	10.07	740

Appendix D

Gambell Observation Well #2

Mm	Dd	Yу	Нſ	Mn	Ss #	AirT	WaterT	Stage	Conductivity	Mm	Đ	d Yy	Hr	Mn	\$s	Airī	⊎aterT	Stage	Conductivity
6	22	94	16	37	42	2.18	-0.31	10.08	917	6	2	7 94	22	37	42	4.81	-0.3	9.91	650
6	22	94	19	37		2.14	-0.3	10.06	907	6	2			37	42	4.14	-0.31	9.87	644
6	22	94	22	37		2.03	-0.3	10.07	898	6	2		4	37	42	3.73	-0.3	9.86	641
6	23	94	1	37		1.94	-0.3	10.05	889	6	2		7	37	42	4.03	-0.3	9.85	638
6	23	94	4	37		1.83	-0.3	10.05	881	6	2		10	37	42	4.68	-0.3	9.84	632
6	23	94	7	37		1.77	-0.3	10.05	873	6	2	8 94	13	37	42	5.7	-0.3	9.83	631
6	23	94	10	37	_	1.75	-0.3	10.06	866	6	2	8 94	16	37	42	5.8	-0.3	9.87	628
6	23	94	13	37		1.79	-0.3	10.07	860	6	2	8 94	19	37	42	5.34	-0.3	9.87	624
6	23	94	16	37	42	2	-0.3	10.11	857	6	5	8 94	22	37	42	4.54	-0.3	9.84	618
6	23	94	19	37	42	2.13	-0.3	10.09	848	6	2	9 94	1	37	42	4.12	-0.3	9.84	614
6	23	94	22	37		2.19	-0.3	10.13	840	6	2	9 94	4	37	42	4.01	-0.31	9.83	612
6	24	94	1	37	42	2.15	-0.3	10.11	832	6	2			37	42	3.87	-0.3	9.83	610
6	24	94	4	37	42	2.09	-0.3	10.14	823	6	2	9 94	10	37	42	4.02	-0.31	9.83	606
6	24	94	7	37	42	2.04	-0.3	10.14	816	6	Z		13	37	42	4.31	-0.31	9.82	602
6	24	94	10	37	42	2.14	-0.3	10.12	810	6	2		16	37	42	4.65	-0.31	9.82	599
6	24	94	13	37	42	2-45	-0.3	10.12	809	6	2			37	42	4.4	-0.31	9.82	597
6	24	94	16	37	42	2.76	-0.31	10.1	800	6	2		22	37	42	3.94	-0.31	9.82	593
6	24	94	19	37	42	4.63	-0.3	10.07	793	6	3		1	37	42	3.57	-0.31	9.83	589
6	24	94	22	37	42	5.11	-0.3	10.11	777	6	3			37	42	3.44	-0.31	9.8	587
6	25	94	1	37	42	4.34	-0.3	10.11	773	6	3			37	42	3.59	-0.31	9.79	583
6	25	94	4	37	42	2.85	-0.3	10.1	771	6	3			37	42	3.73	-0.31	9.79	582
6	25	94	7	37	42	2.84	-0.3	10.09	763	6	3			37	42	4.23	-0.31	9.82	590
6	25	94	10	37	42	2.8	-0.3	10.08	760	6	3			37	42	4.15	-0.3	9.81	580 574
6	25	94	13	37		3.12	~0.3	10.07	758	6	3			37	42	3.95	-0.31	9.79	567
6	25	94	16	37		3.54	~0.3	10.06	746	6	3			37	42 42	3.54 3.3	-0.31 -0.31	9.78 9.77	564
6	25	94	19	37	42	3.89	-0.3	10.05	732	7 7		1 94 1 94		37 37	42	3.12	-0.31	9.79	559
6	25	94	22	37	42	4.06	-0.3	10.04	726	7		1 94		37	42 42	3.06	-0.31	9.78	556
6	26	94	1	37	42	2.87	-0.3	10.05	726	7		1 94		37	42	3.08	-0.31	9.78	556
6	26	94	4	37		1.31	-0.3	10.03	723 714	7		1 94		37	42	3.18	-0.31	9.78	553
6	26	94	7	37	42	2.06	-0.3	10.02		7		1 94		37	42	3.28	-0.31	9.77	550
6	26	94	10	37	42	2.54	-0.31	10.01	720 713	7		1 94		37	42	3.29	-0.31	9.79	548
6	26	94	13	37	42	2.93	-0.3	9.99 10	703	7		1 94		37	42	3.25	-0.31	9.77	544
6	26	94	16	37 37	_	3.36	-0.3 -0.3	9.98	691	7		2 94		37	42	3.19	-0.31	9.77	542
6	26	94	19			3.43			685	"		2 94		37	42	3.13	-0.31	9.8	540
6	26	94	22	37 37	_	3.53	-0.3 -0.3	9.98 9.96	684	7		2 94		37	42	3.08	-0.31	9.78	537
6	27	94 94	1	37	4Z 42	2.44	-0.31	9.95	680	7		2 94		37	42	3.1	-0.31	9.78	537
6	27	94	7	37 37		3.28	-0.31 -0.31	9.92	673	7		2 94		37	42	3.19	-0.31	9.78	536
6	27 27		10	37 37	42 42	4.17	~0.31 ~0.31	9.92	668	7		2 94		37	42	3.28	-0.31	9.78	534
6	27	94 94	13	31 37	42	4.85	-0.3	9.9	663	7		2 94		37	42	3.44	-0.31	9.8	531
6	27	94	16	37	42	5.61	-0.3	9.9	659	7		2 94		37	42	3.44	-0.31	9.78	527
6	27	94	19	37		5.62	-0.3	9.9	656	7		3 94		37	42	3.39	-0.31	9.79	523
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Appendix D

Gambell Observation Well #2

Mm	Dd	Υу	Яr	Mn	Ss AirT	WaterT	Stage	Conductivity	Мп	Do	ł Yy	Нr	Mn	Ss AirT	WaterT	Stage	Conductivity
7	3	94	4	37	42 3.21	-0.31	9.8	520	7	8	3 94	10	37	42 8.34	~0.31	9.6	476
7	3	94	7	37	42 3.16	-0.31	9.77	518	7	8		13	37	42 9.96	-0.31	9.7	468
7	3	94	10	37	42 3.25	-0.31	9.77	517	7	Š		16	37	42 9.58	-0.31	9.63	454
7	3	94	13	37	42 3.38	-0.31	9.76	516	7	ě		19	37	42 9.83	-0.31	9.68	461
7	3	94	16	37	42 3.7	-0.31	9.76	517	7	8		22	37	42 8-61	-0.31	9.7	457
7	3	94	19	37	42 3.89	-0.31	9.75	513	7	g		1	37	42 7-14	-0.31	9.68	458
7	3	94	22	37	42 4.31	-0.31	9.76	511	7	ġ		4	37	42 6.26	-0.31	9.65	455
7	4	94	1	37	42 4.34	-0.37	9.75	506	7	9	94	7	37	42 6.13	-0.31	9.66	449
7	4	94	4	37	42 4.18	-0.31	9.73	504	7	9	94	10	37	42 7.7	-0.31	9.6	457
7	4	94	7	37	42 4.64	-0.31	9.72	501	7	9	94	13	37	42 10.04	-0.31	9.58	459
7	4	94	10	37	42 5.28	-0.31	9.7	499	7	9	94	16	37	42 8.38	-0.31	9.66	448
7	4	94	13	37	42 6.53	-0.31	9.68	500	7	9	94	19	37	42 7.87	-0.31	9.63	445
7	4	94	16	37	42 6.4	-0.31	9.73	500	7	9	94	22	37	42 7.11	-0.31	9,63	450
7	4	94	19	37	42 5.1	-0.31	9.7	496	7	10		1	37	42 6.52	-0.31	9.62	449
7	4	94	22	37	42 4.73	-0.31	9.69	494	7	10		4	37	42 6.12	-0.31	9.61	447
7	5	94	1	37	42 4.52	-0.31	9.7	495	7	10	94	7	37	42 5.79	-0.31	9.63	446
7	5	94	4	37	42 4.41	-0.31	9.7	496	7	10		10	37	42 5.56	-0.31	9.6	442
7	5	94	7	37	42 4.17	-0.31	9.7	495	7	10		13	37	42 5.49	-0.31	9.61	441
7	5	94	10	37	42 4.43	-0.31	9.67	490	7	10		16	37	42 6.18	-0.31	9.57	457
7	5	94	13	37	42 7.31	-0.31	9.65	511	7	10		19	37	42 7.24	-0.31	9.62	443
7	5	94	16	37	42 9	-0.31	9.66	488	7	10		22	37	42 6.6	-0.31	9.6	437
7	5	94	19	37	42 7.97	-0.31	9.71	484	7	11		1	37	42 5.84	-0.31	9.58	438
7	5	94	55	37	42 6.91	-0.31	9.69	482	7	11		4	37	42 5.21	-0.31	9.59	437
7	6	94	1	37	42 6-15	-0.31	9.69	481	7	11		7	37	42 5.26	-0.31	9.56	435
7	6	94	4	37	42 6.12	-0.31	9.68	482	7	11		10	37	42 6.4	~0.31	9.53	433
7	6	94	7	37	42 6.08	-0.31	9.68	482	7	11		13	37	42 8.89	-0.31	9.5	446
7	6	94	10	37	42 5.41	-0.31	9.69	481	7	11		16	37	42 10.5	-0.31	9.52	429
7	6	94	13	37	42 5.22	-0.31	9.69	479	7	11		19	37	42 10.14	-0.31	9.57	426 427
7~	6	94	16	37	42 5.7	-0.31	9.68	477	7 7	11		22 1	37 37	42 8.82	-0.31	9.58 9.55	428
7	6	94	19	37	42 5.16	~0.31	9.68	478		12		4	37 37	42 6.82 42 5.83	-0.31 -0.31	9.52	426
(	6	94	22	37	42 4.62	-0.31	9.71	475 474	7	12 12		7	37 37	42 5.76	-0.31	9.5	424
(	7 7	94 94	1	37	42 4.3	-0.31	9-68		7	12		10	37 37	42 8.12	-0.31	9.44	438
7	7	94	4	37 37	42 4.43 42 4.56	-0.31 -0.31	9.68 9.68	473 471	7	12		13	37 37	42 10.15	-0.31	9.48	431
7	7	94	7 10	37	42 5.82	-0.31	9.65	470	7	12		16	37	42 11.16	-0.31	9.47	420
7	7	94	13	37	42 7.91	-0.31	9.67	482	7	12		19	37	42 10.73	-0.31	9.49	419
7	7	94	16	37	42 7.37	-0.31	9.69	468	7	12		22	37	42 8.75	-0.31	9.52	423
7	7	94	19	37	42 7.37	-0.31	9.66	467	7	13		1	37	42 7.38	-0.31	9.46	420
7	7	94	22	37	42 7.51	-0.31	9.71	465	7	13		4	37	42 6.73	-0.31	9.46	421
7	á	94	1	37	42 5.83	-0.31	9.69	464	7	13		7	37	42 6.61	-0.31	9.43	417
7	8	94	4	37	42 5.32	-0.31	9.7	462	7	13	-	10	37	42 8.43	-0.31	9.38	420
7	8	94	7	37	42 5.35	-0.31	9.64	461	7		94	13	37	42 11.32	~0.31	9.35	432
,	0	74	,	31	42 7.33	-0.31	7.04	401	,			13	31	75 11176	V-31	, ,	736

Appendix D

Gambell Observation Well #2

Mm	Dd	Yу	Hr	Mn	Ss Aîrĭ	WaterT	Stage	Conductivity	Mm	Dd	Yy	Кr	Mn	Ss AirT	WaterT	Stage	Conductivity
7	13	94	16	37	42 11.88	-0.31	9.41	412	7	18	94	22	37	42 7.45	-0.31	9.26	389
7	13	94	19	37	42 11	-0.31	9.45	415	7	19	94	1	37	42 6.3	-0.31	9.22	390
7	13	94	22	37	42 8.99	-0.31	9.45	418	7	19	94	4	37	42 5.78	-0.31	9.2	390
7	14	94	1	37	42 7.81	-0.31	9.42	414	7	19	94	7	37	42 5.97	-0.31	9.19	392
7	14	94	4	37	42 7.89	-0.31	9.37	413	7	19	94	10	37	42 6.6	-0.31	9.19	386
7	14	94	7	37	42 7.89	-0.31	9.36	412	7	19	94	13	37	42 7.78	-0.31	9.18	387
7	14	94	10	37	42 8.6	-0.31	9.35	411	7	19	94	16	37	42 8.86	-0.31	9.18	386
7	14	94	13	37	42 9.3	-0.31	9.38	415	7	19	94	19	37	42 8.59	-0.31	9.2	386
7	14	94	16	37	42 9.54	-0.31	9.35	414	7	19	94	22	37	42 7.81	-0.31	9.22	384
7	14	94	19	37	42 9.45	-0.31	9.35	430	7	20	94	1	37	42 7.3	-0.31	9.2	383
7	14	94	22	37	42 8.57	-0.31	9.37	410	7	20	94	4	37	42 7.05	-0.31	9.18	385
7	15	94	1	37	42 7.64	-0.31	9.34	409	7	20	94	7	37	42 7.09	-0.31	9.18	385
7	15	94	4	37	42 7.66	-0.31	9.33	406	7	20	94	10	37	42 7.65	-0.31	9.17	382
7	15	94	7	37	42 7.71	-0.31	9.34	407	7	20	94	13	37	42 8,39	-0.31	9.17	397
7	15	94	10	37	42 7.59	-0,31	9.33	408	7	20	94	16	37	42 8.36	-0.31	9.17	390
7	15	94	13	37	42 7.99	-0.31	9.3	415	7	20	94	19	37	42 8.92	-0.31	9.17	384
7	15	94	16	37	42 7.34	-0.31	9.35	416	7	20	94	22	37	42 8.55	-0.31	9.19	378
7	15	94	19	37	42 6.73	-0.31	9.31	408	7	21	94	1	37	42 8.02	-0.31	9.18	382
7	15	94	22	37	42 6.33	-0.31	9.33	404	7	21	94	4	37	42 7.63	-0.31	9.16	381
7	16	94	1	37	42 6.1	-0.31	9.29	403	7	21	94	7	37	42 7.33	-0.31	9.16	381
7	16	94	4	37	42 5-89	-0.31	9.31	400	7	21	94	10	37	42 7.62	-0.31	9.16	380
7	16	94	7	37	42 5.65	-0.31	9.28	397	7	21	94	13	37	42 7.79	-0.31	9.16	381
7	16	94	10	37	42 5.59	-0.31	9.28	394	7	21	94	16	37	42 8.53	-0.31	9.12	378
7	16	94	13	37	42 5.95	-0.31	9,27	395	7	21	94	19	37	42 8.06	-0.31	9.18	381
7	16	94	16	37	42 6.16	-0.31	9,27	389	7	21	94	22	37	42 7.21	-0.31	9.16	377
7	16	94	19	37	42 6.21	-0.31	9.27	388	7	22	94	ŧ	37	42 6.91	-0.31	9.16	378
7	16	94	22	37	42 6.16	-0.31	9.29	389	7	22	94	4	37	42 6.81	-0.31	9.14	380
7	17	94	1	37	42 5.96	-0.31	9.26	388	7	22	94	7	37	42 6.85	-0.31	9.14	379
7	17	94	4	37	42 5.81	-0.31	9.26	389	7	22	94	10	37	42 7.28	-0.31	9.14	378
7	17	94	7	37	42 5.74	-0.31	9.25	390	7	22	94	13	37	42 7.87	-0.31	9.13	378
7	17	94	10	37	42 6.2	-0.31	9.24	390	7	22	94	16	37	42 8.24	-0.31	9.15	379
7	17	94	13	37	42 6.97	-0.31	9.22	389	7	22	94	19	37	42 8.05	-0.31	9.14	378
7	17	94	16	37	42 7.7	-0.31	9.22	388	7	22	94	22	37	42 7.69	-0.31	9.14	377
7	17	94	19	37	42 10.25	-0.31	9.21	388	7	23	94	1	37	42 7.42	-0.31	9.13	377
7	17	94	22	37	42 9.51	-0.31	9.26	388	7	23	94	4	37	42 7.08	-0.31	9.14	378
7	18	94	1	37	42 8.73	-0.31	9.27	391	7	23	94	.7	37	42 6.48	-0.31	9.15	378
7	18	94	4	37	42 8.24	-0.31	9.26	391	7	23	94	10	37	42 5.99	-0.31	9.15	376 377
7	18	94	7	37	42 8-09	-0.31	9.24	390	7	23	94	13	37	42 5.79	-0.31	9.15	377 381
7	18	94	10	37	42 8.73	-0.31	9.19	390	7	23	94	16	37	42 5.88	-0.31	9.16	386
7	18	94	13	37	42 11.17	-0.31	9,18	388	7	23	94	19	37	42 6.27	-0.31	9.14	379
7	18	94	16	37	42 10.8	~0.31	9.26	388	7	23	94 94	22	37 37	42 6.58 42 6.19	-0.31 -0.31	9.15 9.17	379 375
7	18	94	19	37	42 9.35	-0.31	9.28	390	7	24	74	1	31	42 G. 19	-0.31	7.17	3,,

Appendix D

Gambell Observation Well #2

Мm	Dď	Yy	Hr	Ħ⊓	Ss AirT	WaterT	Stage	Conductivity	Mm	Do	d Yy	Hr	Mn	Ss AirT	WaterT	Stage Co	nductivity
7	24	94	4	37	42 5.78	-0.31	9.17	373	7	29	94	10	37	42 8.04	-0.31	9.01	373
7	24	94	7	37	42 6.08	-0.31	9.13	373	7	29		13	37	42 8.32	-0.31	9.01	381
7	24	94	10	37	42 7.03	-0.31	9.13	377	7	29		16	37	42 8.42	-0.31	9.02	377
7	24	94	13	37	42 8.2	-0.31	9.14	383	7	29		19	37	42 8.12	-0.31	9.04	373
7	24	94	16	37	42 9.75	-0.31	9.15	374	7	29		22	37	42 7.62	-0.31	9.03	374
7	24	94	19	37	42 10.37	-0.31	9,15	369	7	30		1	37	42 7	-0.31	9.03	375
7	24	94	22	37	42 9.67	-0.31	9.18	371	7	30	94	4	37	42 6.62	-0.31	9.01	374
7	25	94	ī	37	42 7.23	-0.31	9.19	372	7	30	94	7	37	42 6.4	-0.31	9.01	373
7	25	94	4	37	42 5.41	-0.31	9.15	372	7	30	94	10	37	42 6.3	-0.31	9.01	374
7	25	94	7	37	42 5.57	-0.32	9.08	365	7	30	94	13	37	42 6.52	-0.31	9	371
7	25	94	10	37	42 6.95	-0.31	9.12	369	7	3(		16	37	42 7.45	-0.31	9.01	372
7	25	94	13	37	42 7.3	-0.31	9.12	391	7	30		19	37	42 7.53	-0.31	9	370
7	25	94	16	37	42 9.06	-0.31	9.08	384	7	30		22	37	42 7.47	-0.31	9.02	369
7	25	94	19	37	42 9.75	-0.31	9.11	372	7	31		1	37	42 7.34	-0.31	9.03	370
7	25	94	22	37	42 8.96	-0.31	9.15	373	7	31		4	37	42 7,25	-0.31	9.03	371
7	26	94	1	37	42 8.18	-0.31	9.15	376	7	31		7	37	42 7.42	-0.31	9.03	370
7	26	94	4	37	42 7.79	-0.31	9.12	375	7	31		10	37	42 7.83	-0.31	9.06	370
7	26	94	7	37	42 7.56	-0.31	9.13	376	7	3′		13	37	42 9.89	-0.31	9.05	373
7	26	94	10	37	42 8.12	-0.31	9.08	375	7	3′		16	37	42 9.75	-0.31	9.13	374
7	26	94	13	37	42 8.83	-0.31	9-1	379	7	31		19	37	42 9-24	-0.31	9.17	374
7	26	94	16	37	42 10.56	-0.31	9-05	380	7	31		22	37	42 8.81	-0.31	9.16	375
7	26	94	19	37	42 10.43	-0.31	9.11	372	8	1	94	1	37	42 8.41	-0.31	9.17	374 376
7	26	94	22	37	42 9.77	-0.31	9.11	373	8	1		4	37	42 8.4	-0.31	9.2	374
7	27	94	1	37	42 8.82	-0.31	9.09	375	8		94	7	37	42 8.42 42 8.6	-0.31 -0.31	9-21 9-23	374 374
7	27	94	4	37	42 8.24	-0.31	9.09	375	8		94	10	37 37	42 8.6 42 8.69	-0.31	9.28	376
7	27	94	.7	37	42 7.79	-0.31	9.07	374	8		1 94 1 94	13	37 37	42 8.86	-0.31 -0.31	9.20	374
7	27	94	10	37	42 7.82	-0.31	9.04	369	8 8			16 19	37	42 8.83	~0.31	9.35	376
7	27	94	13	37	42 8.23	-0.31	9.04	386	8			22	37	42 8.35	~0.31	9.4	378
7	27	94	16	37	42 8.05	-0.31	9.05 9.06	377 370	8	2		1	37	42 7.93	-0.31	9.47	380
7	27	94	19	37 37	42 7.99 42 8.05	-0.31	9.03	367	8	:		4	37	42 7.41	-0.31	9.48	381
7 7	27	94 94	22 1	37	42 8.11	-0.31 -0.31	9.02	367	8	2		7	37	42 7-13	-0.31	9.52	383
7	28 28	94	4	37	42 8.57	-0.31	9.05	367	8	2	_	10	37	42 8.18	-0.31	9.53	381
7	28	94	7	37 37	42 8.49	-0.31	9.03	369	8	2		13	37	42 9.46	-0.31	9.55	386
7	28	94	10	37	42 8.76	-0.31	9.03	371	8	2		16	37	42 10.19	-0.31	9.61	386
7	28	94	13	37	42 9.1	-0.31	9.02	370	8	- 2		19	37	42 10.27	-0.31	9.69	383
7	28	94	16	37	42 9.44	-0.31	9.04	370	8	2		22	37	42 8.58	-0.31	9.71	382
7	28	94	19	37	42 9.11	-0.31	9.05	371	8	3		1	37	42 7.93	-0.31	9.69	381
7	28	94	22	37	42 8.26	-0.31	9.06	372	8	3		4	37	42 7.54	~0.31	9,71	384
7	29	94	1	37	42 7.58	-0.31	9.04	372	8	3		7	37	42 7.47	-0.31	9.71	383
7	29	94	4	37	42 7.41	-0.31	9.04	372	8	3		10	37	42 8.35	-0.31	9.72	382
7	29	94	7	37	42 7.33	-0.31	9.04	373	8		94	13	37	42 9.18	-0.31	9.76	390
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Appendix D

Gambell Observation Well #2

Mm	Dd	Yу	Hr	Mn	Ss AirT	WaterT	Stage	Conductivity	Mm	Dđ	Yy	Ħr	Mn	Ss AirT	₩aterī	Stage	Conductivity
8	3	94	16	37	42 9.93	-0_31	9.77	391	8	8	94	22	37	42 20.91	-44.41	-0.31	-624
8	3	94	19	37	42 9.61	-0.31	9.79	386	8	9		1	37	42 20.75	-47-22	-0.31	-624
8	3	94	22	37	42 8.79	-0.31	9.82	384	8	9		4	37	42 20.7	-48.8	-0.3	~624
8	4	94	1	37	42 8.1	-0.31	9.81	384	8	ģ		7	37	42 20.93	-50.69	-0.27	-624
8	4	94	4	37	42 7.48	-0.31	9.81	386	8	9	94	10	37	42 164.9	-55.81	-0.28	-624
8	4	94	7	37	42 7.06	-0.31	9.84	386	8	9		13	37	42 28.13	-59.6	-0.29	-624
8	4	94	10	37	42 7.35	-0.31	9.81	387	8	9		16	37	42 20.69	-63.43	-0.31	-624
8	4	94	13	37	42 8.34	-0.31	9.79	388	8	9		19	37	42 20.32	-68,41	-0.34	-624
8	4	94	16	37	42 9.46	-0.31	9.71	407	8	9		22	37	42 20.07	-72.85	-0.39	-624
8	4	94	19	37	42 8.73	-51.77	26.33	392	8	10	94	1	37	42 19.46	-78.56	-0.42	-624
8	4	94	22	37	42 7.89	-76.23	26.3	391	8	10		4	37	42 20-01	-84.38	-0.43	-624
8	5	94	1	37	42 7.18	-17.85	26.3	394	8	10		7	37	42 20.76	-88	-0.44	~624
ž	5	94	4	37	42 6.83	-17.98	26.28	397	8	10		10	37	42 19.92	164.94	-0.46	-624
8	5	94	7	37	42 7.34	-31.76	0.5	-110	8	10	94	13	37	42 20.01	164.94	-0.49	-624
8	5	94	10	37	42 15.27	-26.68	83.0	-109	8	10	94	16	37	42 18.64	164.94	-0.52	-623
8	5	94	13	37	42 18.08	-25.19	0.93	-109	8	10	94	19	37	42 17.5	164.94	-0.55	-624
8	5	94	16	37	42 16.67	-26.07	0.88	-108	8	10	94	22	37	42 17.29	164.94	-0.57	-624
8	5	94	19	37	42 18.93	-20.39	1.22	-624	8	11	94	1	37	42 17.13	164.94	-0.58	-624
8	5	94	22	37	42 19.17	-22.88	1.07	-624	8	11	94	4	37	42 17.48	164-94	-0.59	-623
8	6	94	1	37	42 20.12	-24.08	1.16	-624									
8	6	94	4	37	42 20.1	-24.75	1.18	-624									
8	6	94	7	37	42 19.81	-25.42	1.16	-624									
8	6	94	10	37	42 19.7	-25.75	1.12	-624									
8	6	94	13	37	42 20.1	-25.79	1.25	-624									
8	6	94	16	37	42 20.07	-25.98	1.24	-624									
8	6	94	19	37	42 20.09	-26.09	1.25	-624									
8	6	94	22	37	42 20	-26.41	1.22	-625									
8	7	94	1	37	42 19.71	-26.01	1.06	-625									
8	7	94	4	37	42 19.4	-26.64	1.02	-625									
8	7	94	7	37	42 19	-27.06	0.97	-625									
8	7	94	10	37	42 18.74	-27.06	0.96	-625									
8	7	94	13	37	42 18.96	-26.92	0.93	-625									
8	7	94	16	37	42 18.94	~27.3	0.93	-625									
8	7	94	19	37	42 18.92	-28.19	0.82	-625									
8	7	94	22	37	42 18.32	-28.41	0.81	~625									
8	8	94	1	37	42 17.4	-29.22	0.76	-625									
8	8	94	4	37	42 16.58	-30	0.71	-625									
8	8	94	7	37	42 19.6	-28.47	0.69	~625									
8	8	94	10	37	42 20.28	-33.47	-0.01	-625									
8	8	94	13	37	42 20.61	-36.17	-0.17	-625									
8	8	94	16	37	42 20.73	-38.5	-0.26	-625									
8	8	94	19	37	42 20.92	-41.79	-0.3	-624									

Appendix E

Gambell Observation wells Gambell #1, Gambell #2 & the Production well - Daily averages

W3-TEMPC	2.22	3.33	3,33	3.33	5.35	3.33	3,33	3.89	3.89	2,78	3.89	3,33	3,33	3.33	3.33	3.33	3.33	3.33	3.33	3,33	3.33	2.22	2.22	1,67	2.78	2.25	2.78	2.78	7.1	68. F	2.78	3.89	3.33	3.33	3.33	2.78	2.78	2.22	5.53
MELLS	-	_	-		-		-	-	-	_	•		-	-	-	-	-	-	_	-	-		-	- ,	-	-	-		- '	-	_	-	-	-	-	•	-	- 1	•1
W3-ELEV	4.35	4.54	4.81	16.4	4.85	76.9	4.35	4.24	4.16	4.07	4.06	4.09	4.08	3.68	3,58	3.51	3.45	3.43	3.47	3.58	4.20	2.08	5.24	4.83	77.7	70.7	3.85	3.68	5.5	3.35	3.16	3.01	2.93	2.79	5.66	2.51	2.31	2.24	2.20
W3-COND W3-ELEV	150	99	2	2	2	2	120	190	190	190	700	210	210	200	200	180	180	200	8	200	8	220	200	240	¥	¥	¥	≨:	ş	¥	¥	210	200	200	210	200	210	3	<u> </u>
U3-STGE 1	10.06	9.88	9.60	9.50	9.56	77.6	10.06	10.17	10.25	10.34	10.35	10.32	10.33	10,73	10.83	10.90	10.96	10.98	10,94	10.83	10.21	9.33	9.17	9.58	10.17	10.38	10.56	10,7	10.90	11,08	11.25	11.40	11,48	11.63	1.7	11.90	12,10	12.17	12.21
u3-tenpf 1	36.00	38.00	38.00	38.00	38.00	38.00	38.00	39.00	39.00	37.00	39.00	38.00	38.00	38.00	38.00	38.00	38.00	38.00	38.00	38.00	38.00	36.00	36.00	35.00	37.00	36.00	37.00	37.00	40-00	39.00	37.00	39.00	38.00	38.00	38.00	37.00	37.00	38.00	38.00
W3-ATR W3	¥	N A	A	¥	¥	¥	¥	¥	¥Α	NA	ΝĀ	¥	Α¥	Ä	NA	¥	¥.	¥	¥	¥	AM	¥	M	NA NA	A	¥	ş	\$	¥	A	A A	A	AN	¥	¥	Ā	NA NA	¥	¥
		_	_			_	_	_	_	_	_	_	_	_	_		_					_	_	_	_	_	_	_		_	_	_	_	_	_	_			
G2.Elev	NA	Ž	ž	×	ž	2	ž	ž	₹	*	×	ž	ž	¥	ž	ž	Ž	ž	×	ž	ž	ž	≱	Ž	Ž	ž	Ž	ž	ž	ž	ž	Ž	ž	*	Ž	Ì	ž	ž	2
G2-Cond	MA	NA	Ą	NA	¥	A.	¥.	NA NA	¥	NA	MA	¥.	¥	NA NA	¥¥	A A	A A	¥	¥	¥	Ā	¥	AN	¥	MA	N.	≨	¥.	Y.	¥.	¥	MA	NA	¥¥	¥	ž	¥	¥	¥
G2-Stage	¥	NA NA	¥ N	Ą	NA NA	¥	¥.	¥	¥	ΝA	NA	ΝΑ	¥	X	¥	Ā	¥	Ā	¥.	¥	AN	Ą	NA	Ä	AN A	Ν	¥	¥.	KA	A X	¥	A A	HA	NA	AN	¥	¥	NA	¥
	KA	N.	Ā	Ą	¥	¥.	¥.	¥	NA	¥	N.	NA A	NA	NA A	NA A	A N	Ä	Ä	Ä	¥	NA	¥	¥	A.	M	¥	Y.	¥	NA	¥.	KA	¥	N	NA	Ν	¥.	A	ΝA	N A
G2-Air G2-Water	NA	Y.	٧×	NA	ΑN	¥	¥2	¥.	X Y	4	NA	Y.	N A	AN	ĄN	K.	¥,	¥¥	<b>4</b>	ΑN	¥¥	NA NA	KA	Y.	Y.	N A	¥ X	N A	Ą	A A	AN	Ā	NA NA	ΑN	NA	¥	N	ΑN	¥.
G1-Elev	NA A	NA.	A.	¥	Ä	A N	¥Z	N N	¥	NA	NA	NA	Ν	MA	¥4	٧A	X A	¥	AN	A A	¥	N.	¥	AN	٨¥	¥	٧A	¥	ΑN	Ϋ́	Ą	MA	MA	K	¥	ş	¥	HA	¥
G1-Cond	Ā	N	٨	NA	MA	¥2	X	¥,	AN	NA	NA	AN	AN	NA	Ν	M	NA	MA	MA	AN	MA	Α¥	Ϋ́	NA AN	NA	¥	NA NA	¥	NA	Ā	¥.	AN	NA	M	Ν	Ā	¥	¥.	¥
-Stage	KA	X	¥	¥	¥	¥	¥.	¥	Ą	Ν	N	NA	¥	A.	NA	Z.	×	¥	ď	¥	¥	M	N	¥.	Z Z	Υ¥	¥	¥.	¥	¥	¥	¥	NA	NA A	¥	¥	N	N N	¥
Vater G1	NA	¥	¥	¥	¥	NA N	¥2	¥	Ν	¥	NA	NA	MA	N	Ϋ́	NA.	¥	¥	¥	¥	Κ¥	MA	NA	Ν	٨	₩	K.	X A	AN AN	¥	X A	¥	A.	W	¥	¥	¥.	NA	ΑN
G1-Air G1-Water G1-Stage	NA	NA	¥	A N	NA NA	Ą	¥	ΑN	NA	MA	٧¥	W.A	¥.A	NA A	X A	¥	N A	¥	¥	NA	NA	٧A	¥¥	¥¥	N.	¥.	NA NA	Ϋ́	¥	NA	NA	¥4	NA	NA	NA	NA	Y.	٧×	Y.
Time (	NA	¥	¥¥	NA M	¥	¥,	¥	NA A	Α¥	AM	NA W	KA	¥	NA	¥	¥	¥.	¥	٨	KA	NA	NA NA	KA KA	ΚA	¥	NA A	¥	NA	¥	¥	Ā	KA KA	NA A	KA	¥¥	¥¥	NA NA	¥Α	KA K
Date	10/20/92	10/21/92	10/22/92	10/23/92	10/24/92	10/25/92	11/02/92	11/03/92	11/04/92	11/05/92	11/06/92	11/07/92	11/08/92	11/16/92	11/17/92	11/18/92	11/19/92	11/20/92	11/21/92	11/22/92	11/23/92	11/24/92	11/25/92	11/27/92	11/30/92	12/01/92	12/02/92	12/03/92	12/04/92	12/05/92	12/06/92	12/07/92	12/08/92	12/09/92	12/10/92	12/11/92	12/13/92	12/14/92	12/15/92

This is computed daily average data for all wells and is the source data for the graphs, app F.

Appendix E

Gambell Observation wells Gambell #1, Gambell #2 & the Production well - Daily averages

Date	Time	G1-Air	G1-Water	G1-Stage	G1-Cond	G1-Elev	GZ-Air	G2-Water	G2-Stage	G2-Cond	G2-Elev	W3-AIR	W3-TEMPF	W3-STGE	W3-COND	M3-EFEA	WELLS	W3-TEMPC
12/16/92	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	38.00	12.29	170	2.12	3	3.33
12/17/92	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA.	NA	NA	37.00	12-42	200	1.99	3	2.78
12/18/92	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	38.00	12.48	200	1.93	3	3.33
12/19/92	NА	NA	NA	WΑ	NA	NA	NA	NA	NA	NA	NA	NA	38.00	12.63	200	1.79	3	3.33
12/20/92	NA	NА	NA	NA	NA.	NA	NA	NA.	NA	NA	NA	NA	38.00	12.67	200	1.74	3	3.33
12/21/92	AK	NA	NA	NA	NA	NA	NA	NA	₩A	NA	NA	NA	37.00	12.67	190	1.74	3	2.78
12/22/92	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	37.00	12.71	200	1.70	3	2.78
12/27/92	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	38,00	13.00	200	1.41	3	3.33
12/28/92	NA	NA	NA	NA	NA	NA	NA	NA.	NA	NA	NA	NA	38.00	13.00	210	1.41	3	3.33
01/01/93	NA	NA	NA	NA	NA	NA	NA	NA.	NA	NA	NA	NA	36.00	13.33	200	1.08	3	2.22
01/07/93	NA	NA	ΝA	NA	NA	NA	NA	NA	NA	NA	NA	NA	37,00	13.08	210	1.33	3	2.78
01/08/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	38.00	13.13	220	1.29	3	3.33
01/09/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	37.00	13.13	220	1.29	3	2.78
01/10/93	NA	NA	AK	NA	NA	NA	NA.	NA	NA	NA	NA	NA	37.00	13.08	220	1.33	3	2.78
01/11/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	N.A	NA	37.00	13.08	230	1.33	3	2.78
01/12/93	MA	NA	NA	NA	NA.	NA	NA	NA	NA	NA	NA	NA	37.00	13.08	220	1.33	3	2.78
01/16/93	ЖA	NА	NA	NA	NA.	NA	NA	NA	NA	NA	N.A	NA	35.00	13.17	230	1.24	3	1.67
01/17/93	NA	NA	NA	KA	NA	NA	NA	NA.	NA	NA	N.A	NA	35.00	13.25	230	1.16	3	1.67
01/18/93	NA	NA.	NA	NA.	NA	NA	NA	NA	NA	NA	NA	NA	35.00	13.25	230	1.16	3	1.67
01/19/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA.	NA	NA	34.00	13.25	230	1.16	3	1.11
01/20/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	37.00	13.25	220	1.16	3	2.78
01/25/93	NA	NA	NA	NA	NA	NA	NA	NA	NA.	NA.	NA	NA	36.00	13.67	304	0.74	3,4	2.22 1.67
01/26/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	35.00	13.67	308	0.74	3,4	
01/27/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA.	NA	NA	34.00	13.58	200	0.83	3,4	1.11 2.78
01/28/93	NA	NA	NA	NA	NA	NA	NA	NA.	NA	NA	NA	NA	37.00	13.67	216	0.74	3,4	3.33
01/29/93	NA	NA	NA.	NA	NA	NA	NA	NA	NA	NA	NA	NA	38.00	13,67	193	0.74 0.49	3,4	2.78
02/01/93	NA	NA	ЖA	NA	NA	NA	NA	NA	NA	NA.	NA	NA	37.00	13.92	194 199	0.49	3,4 3,4	3.33
02/02/93	NA	NA.	NA	NA	NA	NA	NA.	NA.	NA	NA.	NA.	NA	38.00 38.00	13.92 13.88	277	0.54	3,4	3.33
02/03/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA.	NA		13.92	214	0.49	3,4	3.33
02/04/93	NA	NA	NA.	NA	NA	NA	NA.	NA.	NA	NA	NA NA	NA NA	38.00 37.00	13.92	198	0.49	3,4	2.78
02/05/93	NA	NA	NA	NA	NA	NA 	NA	NA.	NA.	NA	NA	NA NA		13.92	198	1.41	3,4	2.22
02/06/93	NA	NA	NA	NA	NA	NA.	NA.	NA.	NA	NA.	NA	NA NA	36.00 34.00	13.00	204	1.41	3.4	1.11
02/07/93	NA.	NA	NA	NA	NA	NA	NA	NA.	NA.	NA NA	NA.	NA.	37.00	14.08	207	0.33	3,4	2.78
02/08/93	NA	NA	NA	NA.	NA.	NA	NA.	NA	NA.	NA WA	NA NA	NA NA	37.00	13.00	204	1.41	3,4	2.78
02/09/93	NA	NA	NA	NA.	N.A	NA	NA	NA.	NA	NA	NA NA	NA NA	37.00	14.08	214	0.33	3,4	2.78
02/10/93	NA	NA	NA.	NA NA	NA	NA.	NA	NA NA	NA NA	NA NA	NA NA	NA NA	37.00	14.08	304	0.33	3,4	2.78
02/11/93	NA	NA.	NA.	NA	NA.	NA.	NA	NA.	NA	NA.	NA NA	NA.	37.00	14.08	315	0.33	3,4	2.78
02/12/93	NA	NA.	NA.	NA	NA.	NA.	NA NA	NA.	NA NA	NA NA	NA NA	NA NA	37.00	14.08	314	0.33	3,4	2.78
02/13/93	NA	NA	NA.	NA.	NA	NA	NA.	NA NA	AK	NA NA	NA NA	NA NA	37.00	14.08	325	0.33	3.4	2.78
02/14/93	NA	NA	NA	NA.	NA.	NA.	NA.	NA.	NA	NA NA	NA NA		36.00	14.08	332	0.33	3,4	2.73
02/15/93	NA	NA	NA	NA.	NA	NA	NA	NA.	NA	NA.	NA	NA	30.00	14.00	332	0.33	3,4	2.24

Appendix E

Gambell Observation wells Gambell #1, Gambell #2 & the Production well - Daily averages

Date	Time	G1-Air	G1-Water	G1-Stage	G1-Cond	G1-Elev	G2-Air	GZ-Water	G2-Stage	G2-Cond	GZ-Elev	W3-AIR	W3-TEMPF	W3-STGE	W3-COND	W3-ELEV	WELLS	W3-TEMPC
02/16/93	NA	N.A	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	37.00	14.08	330	0.33	3,4	2.78
02/17/93	NA	NA	N:A	NA	NA	NA	NA	NA.	NA	NA	NA	NA	36.00	14.08	320	0.33	3,4	2.22
02/18/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	37.00	14.08	337	0.33	3,4	2.78
02/19/93	NA.	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	36.00	14.08	331	0.33	3,4	2.22
02/20/93	NA	NA	NA	NA	NA	NA.	NA	NA	NA	NA	N.A.	NA	36.00	14.08	338	0.33	3,4	2.22
02/21/93	AK	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	36.00	14.08	335	0.33	3,4	2.22
02/22/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	36.00	14.08	339	0.33	3,4	2.22
02/23/93	NA	NA	NA	NA	NA.	NA	N.A.	NA	NA	NA	NA	NA.	36.00	14.08	340	0.33	3,4	2.22
02/24/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	36.00	14.08	351	0.33	3,4	2.22
02/25/93	NA	NA	NA	NA.	NA	NA.	NA	NA	NA	NA	NA	NA	36.00	14.17	352	0.24	3,4	5.22
02/26/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	36.00	14.17	352	0.24	3,4	5-55
02/27/93	NA	NA	NA.	NA	NA.	NA	NA	NA	N.A	NA.	NA	NA	36.00	14.08	345	0.33	3,4	2.22
02/28/93	NA	NA	NA	NA	NA	NA	NA.	NA	NA.	NA	NA	NA	36.00	14.17	365	0.24	3,4	2.22
03/01/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	36.00	14.25	388	0.16	3,4	2-22
03/02/93	NA.	N.A	NA	NA	NA	NA	NA.	NA	NA	NA	NA	NA	37.00	14.25	348	0.16	3,4	2.78
03/03/93	AK	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	38.00	14.25	367	0.16	3,4	3.33
03/04/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA.	₩A	37.00	14.33	332	0.08	3,4	2.78
03/05/93	NA	NA.	NA	NА	NA	NA	NA	NA	NA	NA	NA	NA	36.00	14.33	334	0.08	3,4	2.22
03/06/93	NA	NА	NA	NA.	NA.	NA	NA	NA	NA	NA	NA	NA	36.00	14.25	325	0.16	3,4	2.22
03/07/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	36.00	14.25	400	0.16	3,4,5	2.22
03/08/93	NA	NA	NA	NA	NA	NA	NA	NA	N.A	NA	NA	NA	37.00	NA	380	NA	3,4,5	2.78
03/09/93	AM	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	36.00	NA	420	₩A	3,4,5	2.22
03/10/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	₩A	NA	37.00	14.33	356	0.08	3,4,5	2.78
03/11/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	36.00	NA	391	AM	3,4,5	2.22
03/12/93	NА	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	37.00	14.33	365	0.08	3,4,5	2.78
03/13/93	NA	NA	NA	NA.	NA	NA	NA	NA	NA	N.A.	NA	NA	37,00	NA	375	NA	3,4,5	2.78
03/14/93	NA	NA	NA	NA	N.A.	NA	NA	NA.	NA	NA.	NA	NA	36.00	NA	380	NA.	3,4,5	2.22
03/15/93	NA	NA	NA.	NA	NA.	NA	NA	NA.	NA	NA	NA	МA	36.00	14.67	393	-0.26	3,4,5	2.22
03/16/93	NA	NA	NA	NA	NA	NA	NA	NA.	NA	NA	NA	NA	36.00	NA.	372	NA.	3,4,5	2.22
03/17/93	NA	NA	NA	NА	NA	NA	NA	NA	NA	N.A	NA	NA	36.00	14.75	367	-0.34	3,4,5	2.22
03/18/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA.	36.00	NA.	364	NA.	3,4,5	2.22
03/19/93	NA	NA	NA	NA	NA	NA	NA	NA.	NA	NA	NA	NA	36.00	14.75	364	-0.34	3,4,5	2.22
03/20/93	КA	AK	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	36.00	N.A	356	NA	3,4,5	2.22
03/21/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	36.00	NA.	321	NA A	3,4,5	2.22
03/22/93	NA	NA	NA	NA	NA	NA	NA	NA	N.A	NA	NA	NA	37.00	14.75	356	-0.34	3,4,5	2.78
03/23/93	ŃΑ	NA	NA.	NA	NA	NA	NA	N.A	NA.	NA	NA	NA	37.00	NA.	372	NA.	3,4,5	2.78
03/24/93	NA	NA	NA.	NA	NA	NA	NA	NA.	NA	NA	NA.	NA	37.00	14.92	388	-0.51	3,4,5	2.78
03/25/93	NA	NA	NA.	NA	NA	NA	NA	NA.	NA	NA	NA	NA	37.00	NA.	446	NA NA	3,4,5	2.78
03/27/93	NA	NA	NA	NA	N.A.	NA	NA	NA.	NA.	NA	NA	NA	37.00	14.92	388	-0.51	3,4,5	2.78
03/29/93	NA	NA	NA	RА	NA	NA	NA	NA	NA	NA	NA	NA	37.00	14.92	355	~0.51	3,4,5	2.78
03/30/93	ЖA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	37,00	NA	374	NA	3,4,5	2.78

Appendix E

Gambell Observation wells Gambell #1, Gambell #2 & the Production well - Daily averages

Date	Time	G1-Air (	G1-Water G1	-Stage	G1-Cond	G1-Elev	G2-Air	G2-Water	G2-Stage	G2-Cond	G2-Elev	W3-AIR	W3-TEMPF	W3-STGE	W3-COND	W3-ELEV	WELLS	W3-TEMPC
03/31/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	37.00	14.92	411	-0.51	3,4,9	2.78
04/01/93	NA	NA	NA	KA	NA	NA	NA	NA	NA	NA	NA	NA	37.00	NA	302	NA	3,4,5	2.78
04/02/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	36.00	14.92	354	-0.51	3,4,5	2.22
04/03/93	NA	NA	NA	NA	NA	NÀ	NA	NA	NA	NA	NA	NA	36.00	NA	434	NA	3,4,5	2.22
04/04/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	36.00	NA	463	NA	3,4,5	2.22
04/05/93	NA.	NA	NA.	NA	N.A	NA	NA	NA	NA	NA	NA	NA	36,00	14,75	426	-0.34	3,4,5	2.22
04/06/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	36.00	NA	416	NA	3,4,5	2.22
04/07/93	NA	NA	NA	NA	NA	NA	NA.	NA	NA	NA	NA	NA	36.00	14.75	421	-0.34	3,4,5	2.22
04/08/93	NA	NA	NA.	NA	NA	NA	NA	NA	NA	NA	NA	NA	36.00	NA	408	NA	3,4,5	2.22
04/09/93	NA	NA	NA	NA	NA	NA	NA	NA.	N/A	NA	NA	NA	36.00	14.83	420	-0.42	3,4,5	2.22
04/10/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	ЖA	NA	36.00	NA	440	NA	3,4,5	2.22
04/11/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	36.00	NA	474	NA	3,4,5	2.22
04/12/93	NА	NA.	NA	NA	NA	NA	NA	NA.	NA	NA	NA	NA	36.00	14.92	483	-0.51	3,4,5	2.22
04/13/93	ŅĄ	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	36.00	NA	456	NA.	3,4,5	2.22
04/14/93	NA	NA	NA	NA	AM	NA	NA	NA	NA	NA.	NA	NA	37.00	14.75	435	-0.34	3,4,5	2.78
04/15/93	NA	NA	NA	NA	NA	NA	NA	NA	NÁ	NA	NA	NA	37.00	. NA	445	NA.	3,4,5	2.78
04/16/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	38.00	15.08	400	-0.67	3,4,5	3.33
04/28/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	35.00	NA	527	NA	3,4	1.67
04/29/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	35.00	NA	493	NA	3,4	1.67
04/30/93	NA	NA	NA	NA	NA	NА	NA	NA	NA	NA	NA	NA	35.00	NA	524	NA	3,4	1.67
05/24/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	36.00	NA	292	NA	4	2.22
05/25/93	NA	NA	NA	NA	NA	NA	₩A	NA	NA.	NA	NA	NA	36.00	NA	296	NA	4	2.22
05/28/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	<b>NA</b>	37.00	NA	283	NA	4	2.78
06/01/93	NA.	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	38.00	NA	ЖA	NA	4	3.33
06/03/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	36.00	NA	NA.	NA	4	2.22
06/05/93	NA	NA	NA	NA	NA	NA	NA	NA.	NA.	NA	NA	NA	36.00	MA	NA.	NA	4	2.22
06/07/93	₩A	NА	NA	NA	NA.	NA.	NA	NA.	NA	NA	NA	NA	36.00	NA	NA	NA .	4	2.22
06/09/93	NA	NA	NA	NA	NA	NA	NA	NA.	NA	NA	NA	NA	36.00	8.67	NA	5.74	4	2.22
06/11/93	NA	NA	RA	NA	NA	NA	NA	NA	NA	NA	NA	NA.	36.00	8.83	NA A	5.58	4	2.22
06/18/93	NA.	NA.	NA	NA	NА	NA	NA	N.A	NA	NA	NA.	NA	36.00	8.75	137	5.66	4	2.22
06/21/93	NA	NA.	NA	NA	NA	NA	NA	NA	NA.	NA	NA	NA.	36.00	NA	136	MA	-4,	2-22
06/22/93	NA	NA	NA	NA	NA.	NA	NA	NA	NA	NA.	NA	NA	36.00	, NA	132	MA	3,4	2.22
06/24/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	36.00	7.75	137	6.66	3,4	2.22
06/25/93	NA	NA	NA	NA	NA	NA	N.A	NA	NA	NA	NA.	NA	NA 22 AA	8.92	NA T/O	5.49	3,4	2.22
06/28/93	NA	NA	NA.	NA	NA	NA	NA	NA	NA	NA	NA	NA.	37.00	8.00	140	6.41	3,4	2.78
06/29/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	37.00	9.08	140	5.33	3,4	2.78
07/02/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	37.00	9.00	143	5.41	3,4	2.78
07/05/93	NA	NA	NA.	NA	NA	NA	NA	NA	NA	NA	NA	NA	37.00	NA	148	NA	3,4	2.78
07/07/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	37.00	NA O 50	151	NA COA	3,4	2.78
07/08/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	N.A.	NA	NA	37.00	9.50	151	4.91	3,4	2.78
07/09/93	NA	NA.	NA	NA	NA	NA	NA	NA	NA	NA.	NA.	NA	37.00	9.58	144	4.83	3,4	2.78

Appendix E

Gambell Observation wells Gambell #1, Gambell #2 & the Production well - Daily averages

Date	Tîme	G1-Air	G1-Water	G1-Stage	G1-Cond	G1-Elev	G2-Air	G2-Water	GZ-Stage	G2-Cond	G2-Elev	W3-AIR	W3-TEMPF	W3-STGE	W3-COND	W3-ELEV	WELLS	W3-TEMPC
07/12/93	NA	NA.	NA	37.00	9.75	150	4.66	3,4	2.78									
07/14/93	NA.	NA	NA.	NA	37.00	9.83	151	4.58	3,4	2.78								
07/16/93	NA.	NA	NA	NA	NA	NA	NA	NA.	N.A	NA	NA	NA	37.00	9.83	150	4.58	3,4	2.78
07/19/93	NA	37.00	10.00	158	4.41	3,4	2.78											
07/21/93	NA	NA	NA	AK	NA.	NA	NA	NA	NA.	NA.	NA	NA	37.00	10.00	162	4.41	3,4	2.78
07/23/93	NA	NA	NA	NА	NA	39.00	10.29	182	4-12	3,4	3.89							
07/26/93	NA	NA	NA	NA	NA	NA.	NA.	NA	NA	NA	NA	NA	38.00	10.46	169	3.95	3,4	3.33
07/28/93	NA	NA	NA	NA	NA.	NA.	NA.	N.A	NA	NA	NA	NA	36.00	10.63	216	3.79	3,4	2.22
07/30/93	NA	36.00	10.71	202	3.70	3,4	2.22											
08/02/93	NA	36.00	10.88	182	3.54	3,4	2.22											
08/04/93	NA	36.00	10.71	183	3.70	3,4	2.22											
08/06/93	NA	МA	NA	NA	NA	NA	36.00	11.00	182	3.41	3,4	2.22						
08/09/93	NA	NA	NA	NA	NA	WA	AK	NA	NA	NA	NA	NA	36.00	11.08	186	3.33	3,4	2.22
08/11/93	NA	NA	NA	AM	N.A	NA	36.00	11.17	179	3.24	3,4	2.22						
08/13/93	NA.	NA	NA	NA	NA	NA.	NA	NA	NA	NA	NA	NA	36.00	11.25	230	3.16	3,4	2.22
08/16/93	NA.	NA	NA.	AИ	NA	N.A	NA	NA	NA	NA.	NA	NA	37.00	11.13	186	3.29	3,4	2.78
08/18/93	NA.	NA	NA.	АК	NA	NA	NA	NA	NA	NA	NA.	МA	37.00	11.04	194	3.37	3,4	2.78
08/20/93	NA	NA	NA	NA	ŅA	АИ	NA	NA	NA	NA	NA	ЖA	37.00	10.38	186	4-04	3,4	2.78
08/23/93	NA	NA	NA	NA.	NA	38.00	9.83	189	4-58	3.4	3.33							
08/25/93	NA	38.00	10.04	177	4.37	3,4	3.33											
08/27/93	NA	10.13	179	4.29	3,4	NA												
08/30/93	NA	NA.	NA	NA.	NA.	NA	NA	NA	NA	NA	NÁ	NA	NA.	NA	185	NA.	3,4	NA NA
08/31/93	NA	₩A	NA	ΝA	NA	MA	NA	NA	NA	NA	NA	NA	NA (0.00	AM AA	182	NA ( #2	3.4	NA ,
09/08/93	NA	NA	NA	NA	NA	NA.	NA	NA.	NA.	NA	NA	NA	40.00	10.29	195	4.12 3.91	3.4	4.44
09/10/93	NA	NA.	NA	NA	NA	NA.	40.00	10.50	195		3,4							
09/13/93	RA	NA	NA	AA.	NA	NA.	NA	NA.	NÁ	NA.	NA.	NA.	36.00	10.83 10.54	193 189	3.58 3.87	3,4 3,4	2.22 2.22
09/15/93	NА	NA	NA.	NA.	NA	NA.	NA	NA.	NA	NA.	NA.	KA NA	36.00			3.41	3,4	3.33
09/17/93	NA	NA	NA	NA.	NA.	NA.	NA.	NA.	NA	NA.	NA	NA NA	38.00 39.00	11.00	191 186	3.70	3,4	3.89
09/20/93	NA	NA	NA	NA	NA	NA.	NA.	NA.	NA NA	NA HA	NA		40.00	10.46	192	3.95	3,4	4.44
09/22/93	NA.	NA	NA	NA	NA.	NA NA	NA	NA.	NA NA	NA NA	NA NA	NA NA	40.00	10.48	190	4.08	3,4	4.44
09/24/93	NÁ	NA.	NA.	NA	NA	NA NA	NA.	NA.	NA	NA.	NA NA	NA	38.00	10.53	189	3.79	3.4	3.33
09/27/93	NA	NA.	NA.	NA	NA.	NA.	NA	NA.	NA NA	NA NA	KA KA	NA NA	38.00	10.63	188	3.79	3,4	3.33
09/29/93	NA	NA	NA.	NA.	NA.	NA NA	NA MA	NA NA	NA NA	NA	МA	NA.	38.00	9.83	205	4.58	3.4	3.33
10/01/93	NA	MA	NA	NA.	NA NA	36.00	9.75	189	4.66	3,4	2.22							
10/06/93	NA	AN AV	NA.	NA NA		NA NA		NA NA	NA NA	NA NA	NA NA	NA NA	36.00	9.83	186	4.58	3.4	2.22
10/08/93	NA	NA NA	NA	NA NA	36.00	9.96	188	4.45	3,4	2.22								
10/11/93	NA	NA NA	NA NA	AK	NA NA	NA NA	NA NA	NA NA	NA NA	NA NA	NA.	NA NA	36.00	9.92	197	4.49	3,4	2.22
10/13/93	ЖA	NA NA	NA NA	AK AN	NA NA	38.00	9.88	201	4.54	3,4	3.33							
10/15/93	NA.		NA NA	NA NA	NA NA	NA NA	NA NA	NA NA	NA	NA.	NA	NA.	42.00	10.13	195	4.29	3,4	5.56
10/18/93	NA NA	NA.	NA.	39.00	10.17	207	4.24	3,4	3.89									
10/20/93	NA	NA.	NA.	MM	AN.	n/A	n/A	H.P.	mUN.	HA.	NA.	1474	37.00	10.11	EVI	4.54	-,-	2.07

Appendix E

Gambell Observation wells Gambell #1, Gambell #2 & the Production well - Daily averages

Date	Time	G1-Air	G1-Water	G1-Stage	G1~Cond	G1-Elev	G2-Air	G2-Water	G2-Stage	G2-Cond	G2-Elev	W3-AIR	W3-TEMPF	W3-STGE	W3-COND	M3-ELEV	WELLS	W3-TEMPC
10/22/93	NA.	NA	NA	NA	NA	NA	NA	NA	NA	NA	НA	NA	39.00	10.13	200	4.29	3,4	3.89
11/01/93	NA	NA	NA	NA	NA	NA	NA	NA.	N.A	ЖA	NA.	NA	39.00	10,42	198	3.99	3,4	3.89
11/03/93	NA	ДA	NA	NA	NA	NA	NA	NA	NA.	NA	NA.	NA	41.00	10.38	195	4.04	3,4	5.00
11/05/93	NA	NA	NA	NA	NA.	NA	NA	NA.	NA	NA	NA	NA	40.00	10.17	198	4.24	3,4	4-44
11/08/93	NA	NА	NA	NA.	NA	NA	NA	NA	NA	NA	NA	NA	39.00	10.04	193	4.37	3,4	3.89
11/18/93	NA	NA	NA	NA	NA	NA	NA	NA.	N.A	NA	NA	NA	39.00	9.63	192	4.79	3,4	3.89
11/12/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	39.00	8.54	198	5.87	3,4	3.89
11/15/93	NA	NA	NA.	NA	NA	NA	NA	NA	NA	NA	NA	NA	39.00	7.83	215	6.58	3,4	3.89
11/17/93	NA	NA	NA	AK	NA.	N.A.	NA	NA	NA	NA	NA	NA	39.00	8.46	212	5.95	3,4	3.89
11/19/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	39.00	9,17	211	5.24	3,4	3.89
11/24/93	NA	NA	NA	NA	NA.	NA	NA	NA	NA	NA	NA	NA	38.00	10.00	214	4.41	3,4	3.33
11/26/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	39.00	10.04	221	4.37	3,4	3.89
11/29/93	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA.	NA	NA	39.00	10.46	215	3.95	3,4	3.89
12/01/93	NA	NA	NA	NA	N.A.	NA	NA	NÁ	NA	NA.	NA	NA	39.00	10.54	225	3.87	3,4	3.89
12/03/93	NA	NA	NA	NA	NA	NA	NA	NA.	NA	NA	NA	NA	37.00	11.17	227	3.24	3,4	2.78
12/06/93	AA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	N.A	36.00	11.00	230	3.41	3,4	2.22
12/08/93	NA	NA	NA	NA	NA	N.A	NA	NA.	NA	NA	NA	NA	39.00	11.21	233	3.20	3,4	3.89
12/10/93	NA	NA	NA	NA	NA	NA	NA	NA.	NA	NA	NA	NA	39.00	11.54	247	2.87	3,4	3.89
12/13/93	NA	NA	NA.	NA	NA	NA	NA	NA	NA.	NA	NA	NA	37.00	12.00	249	2.41	3,4	2.78
12/15/93	NA	NA	NA	NA.	NA	NА	NA	NA	NA	NA	NA	NA	37.00	12.08	250	2.33	3,4	2.78
12/17/93	NA	NA	₩A	NA	NA.	AK	NA	N.A	N.A	NA.	NA	NA	37.00	12.00	249	2.41	3,4	2.78
12/20/93	NA	NA	NA	NA	₩A	NA	NA	NA	NA	NA	NA	NA	36.00	12.42	243	1.99	3,4	2.22
12/22/93	NA	NA	NА	NA	NA	NA	NA	NA	NA	NA	NA	NA	36.00	12.33	245	2.08	3,4	2.22
01/05/94	24:00	<b>~8.05</b>	0.80	3.64	238.00	1_11	NA	NA	NA	NA.	NA	NA	NA	NA	NA	NA	NA	NA
01/06/94	24:00	-8.85	0.85	3.61	245.00	1.08	-5.95	0.56	6.74	394.25	1.03	NA	NA	NA	NA	NA	NA	NA
01/07/94	24:00	-9.63	0.83	3.58	250.75	1.05	-9.61	0.58	6.73	394.25	1.02	NA	NA	NA	NA	NA	NA	NA
01/08/94	24:00	-12.30	0.82	3.52	274.25	0.99	-13.88	0.57	6.69	396.25	0.98	NA	NA.	NA.	NA	NA.	NA.	₩A
01/09/94	24:00	-12-61	0.81	3.45	270.13	0.92	-14.52	0.55	6.64	400.00	0.93	NA	NA	NA	NA	NA	NA	ЖA
01/10/94	24:00	-12.53	0.80	3.39	264.00	0.86	-14.20	0.54	6.58	401.25	0.87	NA	NA.	NA.	NA	NA.	NA.	₩A
01/11/94	24:00	-14.47	0.79	3.34	262.13	0.81	-16.02	0.53	6.53	402.25	0.82	NA	NA.	NA	NA	NA	NA	NA NA
01/12/94	24:00	-15.90	0.77	3.28	258.50	0.75	-17.41	0.51	6.48	405.00	0.76	NA	NA	NA	NA	NA	NA	NA.
01/13/94	24:00	-15.84	0.76	3.22	258.13	0.69	-17.16	0.50	6-43	404.00	0.72	NA	NA	NA	NA	NA.	NA	RA.
01/14/94	24:00	-15.42	0.74	3.17	260.88	0.64	-16.42	0.49	6.38	400.75	0.67	NA	NA	NA	NA	NA.	NA.	NA.
01/15/94	24:00	-13.32	0,73	3.12	265.88	0.59	-14.46	0.48	6.34	400.88	0.63	NA	NA	NA	KA	NA NA	NA	NA MA
01/16/94	24:00	-14.35	0.72	3.07	264.88	0.54	-15.42	0.47	6.30	401.88	0.59	NA	NA.	NA.	NA	NA NA	NA.	NA NA
01/17/94	24:00	-14.00	0.71	3.03	263.00	0.50	-15.45	0.45	6.25	402.00	0.54	NA	NA TO DO	NA	NA 244	NA O DO	NA.	NA 7 90
01/18/94	24:00	~14.07	0.70	2.97	260.25	0.44	-15.89	0.44	6-20	402.00	0.49	NA.	39.00	14.13	261	0.29	3,4	3.89
01/19/94	24:00	-14.64	0.69	2.91	256.88	0.38	-16.51	0.42	6.15	407.50	0.44	NA	NA ZO DO	NA.	NA 274	NA O D/	, NA	NA 7 80
01/20/94	24:00	-15.23	0.69	2.87	255.25	0.34	-16.89	0.41	6.12	410.25	0.41	NA.	39.00	14.17	271	0.24	3,4	3.89
01/21/94	24:00	-13.74	0.68	2.85	255.13	0.32	-16.07	0.41	6.11	406.50	0.40	NA	NA VO AA	NA 47 OR	NA 274	NA O 72	NA.	NA 7 OO
01/22/94	24:00	-11.84	0.68	2.82	258.13	0.29	-13.79	0.40	6.10	405.13	0.39	NA	39.00	14.08	271	0.33	3,4	3.89

Appendix E

Gambell Observation wells Gambell #1, Gambell #2 & the Production well - Daily averages

Oate	Time	G1-Air	G1-Water	G1-Stage	G1-Cond	G1-Elev	GZ-Air	G2-Water	G2-Stage	G2-Cond	G2-Elev	W3-AIR	W3-TEMPF	W3-STGE	W3-COND	W3-ELEV	WELLS	W3~TEMPC
01/23/94	24:00	-13.33	0.68	2.79	266.25	0.26	-14.10	0.39	6.08	402.75	0.37	NA	NA	NA	NA	NA	NA	ÑА
01/24/94	24:00	-17.57	0.68	2.77	277.13	0.23	-19.40	0.37	6.06	401.63	0.34	NA	39.00	14.00	285	0.41	3,4	3.89
01/25/94	24:00	÷17.64	0.68	2.74	290.13	0.21	-19.99	0.35	6.03	400_13	0.32	NA	NA	NA	NA	NA	NA	NA.
01/26/94	24:00	-18,28	0.69	2.71	302.63	0.18	-20.78	0.33	6.02	400.00	0.31	NA	39.00	13.96	288	0.45	3,4	3.89
01/27/94	24:00	-18.24	0.70	2.70	310.25	0.17	-21.68	0.30	6.02	399.38	0.31	NA	NA	NA	NA	NA	RA.	AM
01/28/94	24:00	-17.83	0.70	2.68	315.00	0.15	-21.50	0.28	6.00	398.25	0.29	NA	39.00	13.88	288	0.54	3,4	3.89
01/29/94	24:00	-14.97	0.70	2.66	319.13	0.13	~18.72	0.26	5.98	397.63	0.27	NA	NA	NA	NA	NA	NA	NА
01/30/94	24:00	-12,24	0.70	2.64	319.88	0.10	-15.80	0.24	5.96	397.13	0.25	NA	NA.	NA	NA	NA	NA	AA .
01/31/94	24:00	-7.47	0.69	2.63	322.75	0.10	-10.69	0.22	5.95	397.50	0.24	NA	39.00	14.50	294	-0.09	3,4	3.89
02/01/94	24:00	-4.49	0.68	2.63	325.75	0.10	-7.74	0.20	5.98	396.38	0.27	NA	NA	NA	NA	NA	NA	NА
02/02/94	24:00	-4.38	0.66	2.65	326.38	0.12	-5.43	0.17	6.02	392.38	0.31	NA	39.00	14.50	295	~0 <b>.09</b>	3,4	3.89
02/03/94	24:00	-4.65	0.64	2.66	328.88	0_13	-4.14	0.14	6.05	387.75	0.34	NA	NA.	NA	NA	NA	_NA	NA
02/04/94	24:00	-4.83	0.62	2.68	331.38	0.15	-4.99	0.12	6.08	382.25	0.37	NA	39.00	14.50	297	-0.09	3,4	3.89
02/05/94	24:00	-4.56	0.60	2.70	332.88	0.17	-4.66	0.09	6.09	382.38	0.38	NA	NA	NA	NA	MA	NA	NA
02/06/94	24:00	-4.45	0.58	2.73	331.00	0.20	-4.50	0.07	6.14	392.25	0.42	NA	NA	NA.	NA	NA	NA	NA.
02/07/94	24:00	-4.59	0.56	2.77	326.75	0.24	-4.07	0.04	6.21	404.75	0.50	NA	39.00	14.42	293	-0.01	3,4	3.89
02/08/94	24:00	-4.80	0.54	2.81	322.13	0.28	-4.34	0.01	6-26	411.00	0.55	NA	NA	AA	NA	NA	_NA	NA
02/09/94	24:00	-6.39	0.51	2.85	317.50	0.32	-5.64	-0.01	6.29	412.63	0.58	NA	39.00	14.33	316	0.08	3,4	3.89
02/10/94	24:00	-11.17	0.49	2.87	311.38	0.34	-10.77	-0.03	6.28	413.50	0.57	NA	NA	NA.	NA ~~~	NA.	NA.	NA -
02/11/94	24:00	-13.07	0.47	2.84	305.63	0.31	-13.46	-0.05	6.23	411.75	0.52	NA	39.00	14.33	328	0.08	3,4	3.89
02/12/94	24:00	-12.58	0.46	2.81	302.88	0.27	-13.45	-0.05	6.17	410.63	0.46	NA	NA	NA	NA	NA	NA.	ÑА
02/13/94	24:00	-11.18	0.45	2.76	303.25	0.23	~11.81	-0.05	6.10	410.88	0.39	NA	NA	NA	NA	NA	NA	ЖA
02/14/94	24:00	-12.68	0.43	2.71	305.50	0.18	-13.64	-0.06	6.03	412.75	0.32	NA.	NA	AA	NA	NA	NA	МA
02/15/94	24:00	-14.34	0.42	2.66	311.13	0.13	-14.54	-0.08	5.97	423.25	0.26	NA	NA.	NA	NA	NA.	NA	NA
02/16/94	24:00	-14.49	0.41	2.62	319.50	0.09	-15.90	-0.09	5.92	434.25	0.21	NA	NA	ХA	NA	NA	NA	AA
02/17/94	24:00	-15.29	0.41	2.58	330.63	0.05	-16.45	-0.09	5.89	435.38	0.18	NA.	NA	NA	NA	NA.	NA	NA 
02/18/94	24:00	-15.33	0.40	2.54	344.25	0.01	-16.39	-0.10	5.86	437.00	0.15	NA.	NA	NA	NA.	NA 	NA.	NA.
02/19/94	24:00	-13.34	0.39	2.52	360.50	-0.01	-13.82	-0.11	5.85	452.88	0.14	NA.	NA	NA	NA	NA.	NA.	AK
02/20/94	24:00	-12.19	0.38	2.50	376.75	-0.03	-12.29	-0.12	5.85	468.75	0.13	NA.	NA.	NA.	NA	NA ***	NA	ЖA
02/21/94	24:00	~12.87	0.37	2.49	389.38	-0.04	-13.34	-0.13	5-84	506.50	0.13	NA	NA	NA	NA.	NA	NA	NA Na
02/22/94	24:00	-12.72	0.36	2.47 2.47	400.25 408.50	-0.06	-13.17	-0.13	5.84 5.82	519.50 563.50	0.13	NA	NA.	NA	NA.	NA	NA	NA UA
02/23/94	24:00 24:00	-11.88 -12.39	0.35 0.34	2.47	415.38	-0.06	-11.93 -13.81	-0.15 -0.16	5.80	585.13	0.11 0.09	NA.	NA NA	NA.	NA NA	NA NA	NA NA	AK Ak
02/24/94		-12.39			421.50	-0.08		_	5.77	623.00		NA.	-	NA NA		NA NA	NA NA	AK
02/25/94	24:00		0.33	2.43		-0.10	-14.83	-0.17			0.06	NA.	NA MA	NA	NA	NA	NA	NA.
02/26/94	24:00	-12.89	0.32	2.40	427.75	-0.13	-14.09 -18.47	-0.17	5.73 5.69	675.25 731.00	0.02	NA NA	NA NA	NA NA	NA MA	NA NA	NA NA	NA NA
02/27/94 02/28/94	24:00 24:00	-16.37 -19.05	0.31 0.30	2.37 2.34	434.25 439.25	-0.16 -0.19	-20.72	-0.18 -0.19	5.66	798.13	-0.02 -0.05	NA NA	NA 39.00	NA 14.79	NA 363	NA -0.38	NA 3,4	NA 3.89
02/28/94	24:00	-19.05	0.30	2.34	443.38	-0.19	-20.72	-0.19	5.63	821.00	-0.03		39.00	14.79	356	-0.34		3,89
03/01/94	******	-19.93	0.29	2.28	443.38	-0.25	-23.50	-0.20	5.59	847.63	-0.08	NA NA		14.75 NA	AN AN	-U.34 NA	3,4 NA	NA 2.09
03/02/94	24:00 24:00	-22.76	0.25	2.24	447.13	-0.29	-23.47	-0.20	5.56	880.13	-0.12	NA NA	NA 39.00	14.83	355	-0.42		3.89
		~21.14	0.26	2.21	447.25	-0.32	~21.87		5.52	918.50	-0.19				NA NA		3,4 NA	3.89 NA
03/04/94	24:00	-21.14	0.20	2.21	441.23	-0.32	~21.0/	-0.21	3.32	410.30	-0.19	NA	NA.	KA	MA.	NA	nA.	MA

Appendix E

Gambell Observation wells Gambell #1, Gambell #2 & the Production well - Daily averages

Date	Time	Gî-Air	G1-Water	G1-Stage	G1~Cond	G1-Elev	G2-Air	G2-Water	G2-Stage	G2-Cond	G2-Elev	W3-AIR	W3-TEMPF	W3-STGE	W3-COND	M3-ETEA	¥ELLS	W3-TEMPC
03/05/94	24:00	-20,17	0.25	2.16	447.63	-0.37	-21.31	-0.21	5.48	941.63	-0.24	NA	NA	NA	NA	NA	NA	NA
03/06/94	24:00	-19.34	0.25	2.13	448.00	-0.40	-20.33	-0.21	5.44	940.50	-0.27	NA	NA	NA	NA	NA	NA	KA
03/07/94	24:00	-18.84	0.24	2.10	450.75	-0.43	-19.76	-0.22	5.41	926.63	-0.30	NA	39.00	15.00	354	-0.59	3,4	3.89
03/08/94	24:00	-18.51	0.23	2.07	454-50	-0.46	-19.33	-0.23	5.39	941.75	-0.32	NA	NA	NA	NA	NA	NA.	NA
03/09/94	24:00	-18.37	0.23	2.04	458.88	-0.49	-19-14	-0.23	5.35	924.63	-0.36	NA	39,00	15.08	359	-0.67	3,4	3.89
03/10/94	24:00	-18.62	0.22	2.00	461.75	-0.53	-19.47	-0.23	5.31	934.63	-0.40	NA	NA	NA	NA	NA	NA	NA
03/11/94	24:00	-18.69	0.21	1.96	465.75	-0.57	-19.29	-0.22	5.27	942.75	-0.44	NA	39.00	15.17	365	-0.76	3,4	3.89
03/12/94	24:00	-19.73	0.21	1.93	467.13	-0.60	-20.59	-0.23	5.24	980.38	-0.47	NA	NA	NA	NA	NA	MA	NA
03/13/94	24:00	-18.97	0.20	1.90	468.75	-0.63	-20.53	-0.23	5.22	965.75	-0.49	NA	NA	NA	NA	NA	NA	NA
03/14/94	24:00	-16.78	0.20	1.88	472.75	-0.65	-18.68	-0.24	5.24	996,25	-0.47	NA	40.00	15.25	372	-0.84	3,4	4.44
03/15/94	24:00	-15.63	0.20	1.89	480.88	-0.65	-17.28	-0.24	5.27	965.13	-0.45	NA	NA	NA	NA	NA	NA	NA
03/16/94	24:00	-14.48	0.19	1.90	493.63	-0.63	-14.53	-0.24	5.29	965.63	-0.42	NA	40.00	15.25	368	-0.84	3,4	4.44
03/17/94	24:00	-14-09	0.19	1.91	512.50	-0.62	-14.31	-0.25	5.32	995.75	-0.39	NA	NA	NA	NA	NA	ŇA	NA
03/18/94	24:00	-14.62	0.18	1.93	541.88	-0.60	-15.12	-0.25	5.35	1018.25	~0.36	NA	40.00	15.25	392	-0.84	3,4	4.44
03/19/94	24:00	-17.03	0.17	1.94	572.63	-0.59	-17-81	-0.26	5-35	1054.13	-0.36	NA	NA	NA	NA.	NA	NA	NA
03/20/94	24:00	-17.40	0.16	1.93	604-13	-0.60	-17.23	-0.27	5.34	1078.00	-0.38	NA	NA	NA	NA	NA	NA	NA
03/21/94	24:00	- 19.81	0.15	1.93	639.38	-0.60	-20.94	-0.28	5.32	1111.13	-0.40	NA	NA	NA	NA	NA	NA	NA
03/22/94	24:00	-25.20	0.14	1.91	672.00	-0.62	-26.62	-0.29	5.29	1131.63	-0.42	NA	39.00	15.25	416	-0.84	3,4	3.89
03/23/94	24:00	-26.16	0.13	1.89	701.13	-0.64	-27.82	-0.28	5.27	1127.50	-0-44	NA	NA	NA	NA	NA	NA	NA
03/24/94	24:00	-25.45	0.12	1.88	731.13	-0.65	-27.42	-0.29	5.26	1136-50	-0.46	NA	NA	NA	NA	МA	NA	NA
03/25/94	24:00	-22.58	0.11	1.87	761.88	-0.66	-25.06	-0.29	5.24	1148.75	-0.47	NA	NA	NA.	NA	NA	NA	NA.
03/26/94	24:00	-19.02	0.31	1.87	800.13	-0.66	-21.60	-0.29		1159.25	-0.48	NA	NA	NA	NA	NA	MA	NA
03/27/94	24:00	-16.87	0.10	1.87	832.63	-0.66	-18.41	-0.29		1180.25	~0.49	NA	NA	NA	NA	NA	NA	AK
03/28/94	24:00	-16.54	0.10	1_86	859.75	-0.67	-17-85	-0.29	5.23	1204.38	-0-48	₩A	NA	NA	NA	NA	₩A	AK
03/29/94	24:00	-15.75	0.09	1_85	886.38	-0.68	-16.64	-0.29	5.21	1228.63	-0.50	NA	NA	NA	NA	NA	NA	NA
03/30/94	24:00	-14.83	0.08	1.84	910.63	-0.69	-15.36	-0.30	5.20	1252.25	-0.51	NA	NA	NA	NA	NA	МA	NA
03/31/94	24:00	-12.84	80.0	1.83	933.63	-0.70	-12.76	-0.30	5.20	1272.25	-0.51	NA	NA	NA	NA	NA	NA	NA
04/01/94	24:00	-11.99	0.07	1.85	955.88	-0.68	-10.28	-0.30	5.22	1293.25	-0.49	NA	NA	NA	NA	NA	NA	NA
04/02/94	24:00	-10.69	0.07	1.86	978.25	-0.67	-9.24	-0.30	5.25	1316.88	-0.46	NA	NA	NA	NA	NA	NA	NA
04/03/94	24:00	-9.78	0.06	1.86	1002.38	-0.67	-6.00	-0.30	5.25	1342.75	-0.46	NA	NA	NA	NA	NA	NA	NA
04/04/94	24:00	-8-29	0.05	1.87	1027.50	-0.66	-3.90	-0.30	5.27	1364.38	-0.45	NA	NA	NA	NA	NA	NA	NA
04/05/94	24:00	-7.43	0.04	1.89	1050.50	-0.64	-6.42	-0.30	5.29	1386.25	-0.42	NA	NA	NA	NA	NA	NA	NA
04/06/94	24:00	-7.82	0.04	1.91	1074.38	-0_62	-7.91	-0.30	5.30	1405_00	-0.42	NA	NA	NA	NA	NA	NA	NA
04/07/94	24:00	-9.36	0.03	1.91	1100.63	-0.62	-9.04	-0.31	5.29	1422.63	~0.42	NA	NA	NA	NA	NA	NA	NA
04/08/94	24:00	-10.56	0.02	1.92	1130.38	-0.61	-9.95	-0.31	5.30	1440.75	-0.41	NA	NA	NA	NA	NA.	NA	ЖA
04/09/94	24:00	-10.90	0.01	1.92		-0.61	-10.92	-0.31	5.29	1454.25	-0.42	NA	KA	NA	NA	NA	NA	₩A
04/10/94	24:00	-10.87	0.01	1.90	1165.63	-0.63	-11.03	-0.31	5.25	1466.75	-0.46	NA	NA	NA	NA	NA	NA	NA
04/11/94	24:00	-10.52	0.00	1.87	1174.38	-0-66	-11.03	-0.31	5.20	1475.00	~0.51	NA	NA	NA	NA	NA	NA	NA
04/12/94	24:00	-11.29	0.00	1.84	1187.13	-0.69	-11.89	-0.31	5.15	1481.25	-0.56	NA.	NA	NA	NA	NA	NA.	NA NA
04/13/94	24:00	-11.82	-0.01	1.80	1198.00	-0.73	-12.28	-0.31	5.11	1485.25	-0.60	NA	NA	NA	NA	NA	NA.	NA
04/14/94	24:00	-11.93	-0.01	1.77	1205.38	-0.76	-12.3 <b>1</b>	-0.31	5.09	1489.00	-0.62	NA	NÁ	NA	NA	NA	MA	NA

Appendix E

Gambell Observation wells Gambell #1, Gambell #2 & the Production well - Daily averages

из-темрс	44	2	A A	N.	MA	Z A		ď :	A .	A A	¥ Z	Ϋ́	MA	ΝA	NA	۸A	۸A	¥	Ą	KA KA	43	¥¥	KA	NA NA	NA	A.	NA	A A	X X	ď.	¥	¥.	¥	A :	AN AN	AM.	KA	X Y	Y.	<b>₹</b>	¥	¥.	4	
WELLS	VIA.	Š	AN	MA	M	¥ 7	£ :	¥	¥.	K)	A	¥	¥	¥	₩	X.	MA	¥	Ā	¥	¥	¥	NA	M	KA	¥¥	¥	MA	¥.	¥	X X	≨ :	¥	≨ :	¥	¥	¥	¥	¥	¥	¥	¥	¥	
3-ELEV	*11	ď	MA	NA	44	2 4	<u> </u>	Z :	Y Y	¥	ď.	¥	KA	AM	XX	¥	¥	¥	¥	¥	≨	¥	¥	¥	¥	Y Y	A.	X A	KA	<b>X</b>	¥	<b>X</b>	₹	¥	Y Y	¥	¥	¥	¥	¥	¥	<b>4</b>	¥	
43-COND 43-ELEV	413	¥.	¥	NA.	MA	2 4	<b>5</b>	¥ :	¥	¥	¥	MA	AN	A A	A	N.	N A	¥	Ą	Ą	¥	¥	A.	¥	NA.	¥¥	¥	NA A	¥.	X.	¥	Z	¥	Y.	¥	¥	¥	¥	¥	¥	¥	<b>X</b>	¥	
	***	¥	Ā	MM	VN	£ 5	£ :	¥.	KA KA	MA.	Y Y	¥	A A	¥	¥	NA	¥	¥	¥	¥	¥	٧¥	NA	MA.	NA	NA NA	A	NA	¥	¥	¥	¥	¥	¥	¥	¥	¥	¥	¥	¥	¥	¥	¥	
TEMPF W	*	4	¥.	MA		2 2	Z :	Z.	<b>4</b>	Ā	¥,	¥	Y Y	¥	NA	MA	MA.	X A	Ā	¥	¥	Ā	¥	A	¥	¥	¥	A	A	NA NA	Z Z	<b>X</b>	¥	K K	¥	¥	¥	¥	¥	¥	¥	¥	¥	
W3-AIR W3-TEMPF W3-STGE	•	¥.	NA NA	44	5	X 5	¥ ;	ď	Z Z	¥.	¥¥	NA A	A N	NA	NA	NA	NA NA	Ā	NA	Y.	NA N	V.	NA NA	HA	NA	¥	NA	٧×	NA	NA	¥.	4	A A	X A	WA	NA	NA	N N	N	Ą	NA NA	NA N	¥	
G2-Elev W		20.0-	-0.63	-0 K1		65.0	-0.39	-0.60	~0.62	-0. \$	-0.66	-0.66	-0.66	-0.66	-0.67	-0.69	-0.70	-0-68	-0.63	-0.57	-0.52	-0.50	-0.47	-0.43	-0.41	07.0-	-0.42	-0-41	-0.38	-0.39	-0.39	-0.38	-0.33	-0.28	٠٥.23	-0.20	-0.12	0.09	0.40	69.0	7.0	0.71	99.0	
G2-Cond		1495.65	1506.13	1515 00	20-71-1	1517-00	1565.50	1524.75	1526.38	1527.50	1530.88	1532.75	1536.25	1539.00	1543.00	1545.25	1546.63	1549.00	1552.00	1549.50	1540.73	1538.00	1536.25	1533.75	1529.88	1528.13	1530.13	1524.63	1513.50	1505.63	1497.13	1489.13	1465.88	1442.00	1428,38	1402.25	1402.00	1529.13	1483.50	1520.88	1516.75	1527.88	1620.00	
i2-Stage		2,08	5.09	2 10	2 5	2.16	2.16	5.11	5.09	5.07	5.05	5.05	5.05	5.05	5.04	5,02	5.01	5.03	5.08	5.14	5.19	5.22	5.54	5.28	5.31	5.31	5.29	5.30	5.33	5.32	5.32	5.33	5.38	5-43	5.48	5.51	5.59	5.80	6.11	6.40	6.45	6.42	6.37	
G2-Air G2-Water G2-Stage		-0.31	-0.31	75 0	1	70-34	-0.32	-0.32	-0.32	-0.31	-0.31	-0.31	-0.32	~0.31	-0.31	-0.31	-0.31	-0.32	-0.32	-0.32	-0.32	-0.32	-0.32	-0.32	-0.32	-0.32	-0.32	-0.32	-0.32	-0.32	-0.32	-0-32	-0.32	-0.33	-0.33	-0,33	-0.33	-0.33	-0.31	-0.31	-0.31	-0.31	-0.31	
GZ-Air G	,	-13.55	-15.13	15 44	5	14.02	75.61	-12.50	-11.60	-11.21	-11.01	-10.35	62.6-	×9.02	-7.91	-7.36	.5.99	-6.11	-6.18	-5.94	-5.10	-3.93	-3.36	-3.00	-3.12	-2,85	-2.61	-2.90	-2.72	-2.28	-1.92	-1.27	-0.48	-0.36	-0.76	-0.57	-0.07	0.05	0.15	0.09	-0.24	-0.45	-0.47	
G1-Elev		-0.7	-0.78	200	100	0,70	0,0	-0.77	-0,78	08'0,	-0.81	-0.82	-0.82	-0.82	-0.82	-0.84	-0.85	-0.85	-0.82	-0.78	-0.74	-0.71	-0.69	~0.66	-0.62	-0.59	-0.60	09-0-	-0.58	-0.59	-0.60	·0.58	-0.56	-0.52	-0.46	-0.42	-0.34	-0.09	0.29	9.6	0.73	0.69	9.0	
G1-Cond		1218,63	1234 38	125/ 25	274-67	1272.00	1288.00	1300.50	1310.75	1320.13	1328, 13	1336.00	1345.88	1358.25	1369.38	1378.75	1388.13	1401.88	1421.38	1446.75	1471,63	1494.25	1510.25	1525.13	1540.13	1549.88	1556.63	1562.75	1569.38	1577.25	1583.88	1592.13	1601.88	1607.88	1613.63	1613.38	1617.13	1588.25	1577.50	1576.75	1568.00	1564.25	1567.88	
1-Stage	ì	1.76	<u>τ</u> Κ		1 :	::	1.1	1.76	<b>ر</b> ال	1.74	22.1	1.71	1.71	1-71	1.7	1.69	1.68	1.68	1.71	7.7	1.79	1.82	1.84	1.87	1.91	1.94	1.93	1.93	1.95	1.94	1.93	1.95	1.97	2.01	2.07	2.11	2.19	5.44	2.82	3.19	3.26	3.25	3.17	
G1-Air G1-Water G1-Stage	,	-0.01	-0.01		20.05	20.0-	-0.02	-0.03	~0.03	-0.03	-0.04	-0.04	.0.0¢	-0-04	-0.04	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	·0-05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	~0.05	-0.06	-0.06	-0,06	-0.06	-0.06	-0.05	-0.05	-0.05	-0.05	-0.05	50°0,	-0.06	
61-Air G		-12.89	-13 70	* * / *	* +	23.50	-12.86	-12.04	-11.42	-11.12	-10.94	-10.29	-9.80	-9.13	-8.20	-7,71	-6.35	-6-42	-6.48	-6.31	-5.66	-4.29	-3.59	-3.30	-3.52	-3.24	-2.89	-3.08	-2.92	-2.40	-1.97	-1.30	-0.79	-0.67	-1.12	-0.79	-0.35	-0.21	-0.05	-0.18	-0.51	-0.57	77.0-	
Time	;	24:00	00.76	2 6	00:50	24:00	24:00	24:00	54:00	24:00	24:00	24:00	24:00	24:00	24:00	24:00	24:00	24:00	24:00	24:00	24:00	24:00	24:00	24:00	24:00	24:00	24:00	54:00	24:00	54:00	24:00	54:00	24:00	24:00	24:00	24:00	24:00	24:00	24:00	24:00	24:00	24:00	24:00	
Date		04/15/94	16/16/06	0,747,0	54/11/50	36/BL/50	04/19/94	04/50/64	04/21/64	04/22/94	04/23/94	04/54/94	04/52/64	76/97/70	04/27/94	04/28/94	04/29/94	04/30/94	05/01/94	05/02/94	05/03/94	05/04/94	05/05/94	05/06/94	05/07/94	05/08/94	05/09/94	05/10/94	05/11/94	05/12/94	05/13/94	05/14/94	05/15/94	05/16/94	05/17/94	05/18/94	05/19/94	05/20/94	05/21/94	05/22/94	76/52/50	76/72/50	05/25/94	

Appendix E

Gambell Observation wells Gambell #1, Gambell #2 & the Production well - Daily averages

LS-TEMPC	NA NA	A	4	2	ζ <b>Α</b>	4	Z 2	<b>X X</b>	<b>E</b> 5	¥ :	Y.	A.A	WA	Ϋ́Α	M.A	43	¥.	Z A	Y Y	ď.	AN	NA	ΥA	¥¥	KA.	NA.	XX.	V I	K :	¥ :	Y.	Y.	X :	4	¥.	Z Z	¥ Z	ď.	¥	A.A.	NA.	¥¥	
WELLS	¥.	MA	V N	2 2	( q	NA NA	4	<b>E E</b>	¥ ;	Z :	AN	¥	¥	X Y	¥	AM AM	A X	AN	¥	¥	NA	NA	NA	¥	MA	¥	¥	¥ :	¥:	¥	× :	¥ i	Y :	¥	¥	M	¥	¥	¥	¥	AN	¥	
3-ELEV	MA	MM	44	2 4	۲ ع د ع	<b>* * *</b>	2 3	£ 5	X ·	KA:	X	¥.	¥	Ä	₹	Y Y	¥	Y.	¥	NA	Ä	¥.	NA	X A	¥	¥	¥	¥	<b>Z</b>	≨ :	\$	¥	¥:	¥	NA.	¥	¥	¥	<b>4</b> 2	XX	Z.	¥	
N GNOO-S	MA	MA	4	2 2	<b>5</b> 5	£ 5	2 2	<u> </u>	Z ;	4	¥.	¥	¥	Y Y	¥ ¥	NA NA	X	Ą	A A	NA	¥	H	ΑN	N A	¥	¥	Z Z	ž	¥	¥	Y.	¥	Y.	¥.	¥	¥	¥	¥	¥	¥	4	¥	
/3~STGE 4	N	A N	4 7	¥ ¥	£ 3	2	2 3	5	¥ :	¥	NA N	A	N	A A	N	ď	¥	¥Ν	¥¥	¥¥	NA	¥.	MA	NA	A.	¥	A	¥	¥ i	¥	Y.	¥.	AN	¥	¥	NA	¥	¥	K Z	¥.	AN	¥.	
-TEMPF 1	M	47	<b>X X X</b>	<u> </u>	( q	( <	< <	2 3	¥ ;	ď	¥	A	¥	X X	¥ 2	¥	٧×	NA NA	ΑÃ	AM	Ā	N A	¥.	¥	Ą	¥	¥	¥	¥	¥	¥	¥.	Y.	¥	A A	¥	¥	¥ ¥	¥	¥	¥	¥	
U3-AIR U3-TEMPF U3-STGE U3-COND U3-ELEV	AN	4	2 2	C 4	ĭ <	5 5	£ 2	<b>E</b> :	Y :	NA	ΝA	NA	٧¥	AN.	NA NA	Y Y	AN AN	NA	NA NA	ΝA	Y.	NA	NA	KA K	×	NA NA	K K	X X	Y X	¥	NA.	Y.	MA	A	M	ΥA	X.	¥	¥	NA NA	¥	NA NA	
G2-Elev	0, 69	7,7	2 0		, +			2 .	27.	1.56	1.78	1.97	2.28	2.65	5. 8.	3.26	3.67	4.02	4.33	4.53	69.4	4.76	78.9	4-93	4.86	4.72	4.60	25.4	4.37	4.37	4.40	4.37	4.30	4.21	4-14	4.12	4.09	4-07	4.07	7.06	4-00	3.98	
G2-Cond	22. 7591	1710 KZ	170		5 K	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	36 7361	77.17.	27.67	1726.88	1728.88	1757.00	1765.38	1764.63	1734.50	1706.50	1662.88	1640.88	1634.25	1634.50	1619.00	1600,13	1578,00	1533.38	1436.00	1290.50	1144.38	1024.75	931.13	864.25	807.50	753.63	709.38	666.63	632.00	604,13	581.50	553.75	535.50	516.88	200.00	492.63	
G2~Stage	9 70	57 7	7	2 2	0.70	8 8	8 9	6-0	8 1	1.27	4.49	7.68	7.%	8,36	8.70	8.97	9.38	9.73	10.04	10.24	10.40	10.47	10.57	10.64	10.57	10.43	10.31	10.18	10.08	10.08	10.11	10.08	10-01	9.92	9.85	9.83	9.80	9.78	9.78	9.77	9.71	69.6	
2-Air G2-Water G2-Stage	-D 31	7	5 6	20.0	0.56	7.0	7.0.0	5.0	-0.31	-0.32	-0.32	-0-31	-0-31	-0.31	-0.31	-0.31	~0.30	-0.29	-0.29	-0.30	-0.30	-0.29	-0-29	-0.29	-0.29	-0-30	-0.30	-0.30	-0.30	-0.30	-0.30	-0.30	0.30	-0.30	-0.30	-0,31	-0.31	-0.31	-0.31	-0.31	-0,31	-0.31	
G2-Air	-0 04	0.16	200	, ,	0.69	4.0	2.0	4.0	15.0	0.67	0.53	0.76	1.52	2.22	1.24	5.29	4.52	5.32	5.63	4.28	5.56	7.30	8.62	6.37	3.59	2.7 <del>.</del>	2.8	2.51	2.17	1.93	2.92	3.43	2.73	4.13	5.73	4.17	3.78	3.20	3.23	3.54	5.15	6.09	
G1-Elev	74 0	, K	200		<u> </u>		07.1	<b>†</b> :	1.46	X X	NA	NA	NA	¥¥	MA	Ą	N	AN AN	ď	N	NA	NA	¥	NA	N	KA	KA	A A	<b>X</b>	¥ Z	X X	NA	¥	¥	NA	¥	A A	¥2	NA	A.A	KA KA	NA NA	
G1-Cond	1562 50	1541 00	1530 47	1367.03	27.17.	26.75	33.6	930.00	948.55	NA NA	M	XA	X	¥	<b>X</b>	¥	NA NA	Ā	AN	AN	KA	MA	¥.	¥	Ä	¥	Ā	¥	NA NA	AN AN	A.	AN	¥	٨¥	MA	K	¥	¥	¥.	¥	A	N N	
1-Stage	3 20	27. 24	2.50	7 6	2.6	70.7	7.07	20.0	3.5	<b>X</b>	ĄN	NA	W	¥.	MA	Z A	NA	AN	NA	NA	¥	AN	¥	Ä	¥	NA NA	¥	NA	XX	X X	NA	NA	NA NA	NA	٨	¥	Ν	¥	Y.	¥	¥	KA	
G1-Air G1-Water G1-Stage	70	3 2	0 0	0.00	70.0	0.0	0.00	00-0-	-0.08	¥	A A	¥.	۸	ΑN	42	۸×	¥	KA KA	N.	AN.	NA.	N A	Ν	Ŋ	¥	X X	NA	NA	A'A	A A	ΚA	NA	ď	¥ V	٧	¥.	¥	٧	Y.	¥2	¥2	M	
61-Air 6	01 00	2	0.00	2.0	0.00	, C. C.	0,0	0.57	0.03	NA	NA	MA	NA	AN	KA	MA	A.	Ą	NA	NA	MA	NA	NA	NA	¥¥	¥N	МA	AN	¥	AN	NA	N	NA	M	ΑN	¥	NA NA	ď.	NA NA	NA NA	M	¥	
1 ग्रिल	2700	20.5	24.00	24:00	24:00	00:42	200	00: 57	24:00	24:00	24:00	24:00	24:00	54:00	54:00	24:D0	24:00	24:00	24:00	24:00	24:00	24:00	24:00	24:00	54:00	24:00	24:00	24:00	24:00	54:00	24:00	24:00	24:00	54:00	24:00	24:00	24:00	54:00	24:00	24:00	24:00	24:00	
Date	05 /26 /0/	07/20/20	10, 90, 30	76/66/50	76/67/50	46/06/60	10/3/20	00/01/24	06/05/94	06/03/94	06/04/94	06/05/94	76/90/90	76/20/90	06/08/94	76/60/90	06/10/94	06/11/94	06/12/94	06/13/94	06/14/94	06/15/94	06/16/94	06/17/94	06/18/94	06/19/94	06/20/64	06/21/94	06/22/94	06/23/94	06/24/94	06/25/94	06/26/94	06/27/94	06/28/94	06/29/94	06/30/94	07/01/94	07/02/94	07/03/94	76/70/20	76/50/20	

Appendix E

Gambell Observation wells Gambell #1, Gambell #2 & the Production well - Daily averages

Date	Time	G1-Air G	1-Water G	ì1-Stage	G1-Cond	G1-Elev	G2-Air	G2-Water	G2-Stage	G2-Cond	G2-Elev	W3-AIR	W3-TEMPF	W3-STGE	W3-COND	W3-ELEV	WELLS	W3+TEMPC
07/06/94	24:00	NA	NA	NA	NA	NA	5.56	-0.31	9.69	479.38	3.98	NA	NA	NA	NA	NA	NA	NA
07/07/94	24:00	NA	NA	NA	NA	NA	6.25	-0.31	9.68	471.25	3.97	NA	NA	NA	NA	NA.	ЖA	ЖA
07/08/94	24:00	NA	NA	NA	NA	NA	7.85	-0.31	9.67	462.88	3.96	NA	NA	NA	NA	NA	АИ	NA
07/09/94	24:00	NA	NA	NA	NA	ЖA	7.58	-0.31	9-64	452.63	3.93	NA	NA	NA	NA	NA	NA	NA
07/10/94	24:00	NA	NA	NA	NA	NA	6.19	-0.31	9-61	445.25	3.90	NA	NA	NA	NA	ЖA	ХA	NA
07/11/94	24:00	NA	NA	NA	NA	NA	7.63	-0.31	9-55	433.88	3.84	NA	N.A.	NA	NA	NA	NA	NA
07/12/94	24:00	NA	NA	NA	NA	NA	8.42	-0.31	9.50	426.13	3.79	NA	NA	MA	NA	NA	ЖA	NA.
07/13/94	24:00	NA	NA	NA	NA	NA	9.04	-0.31	9.42	419.38	3.71	NA	NA	NA	NA	NA	NA	NA
07/14/94	24:00	NA	NA	NA	NA	NA	8.63	-0.31	9.37	412.38	3.66	NA	NA	NA	NA	NA	NA	NA
07/15/94	24:00	МA	NA	NA	NA	NÁ	7.37	-0.31	9.33	409.13	3-62	NA	NA	NA	NA	NA	NA	NА
07/16/94	24:00	NA	NA	NA	NA	NA	5.96	-0.31	9.28	394.38	3.57	NA	NA	NA	NA	NA	NA	NА
07/17/94	24:00	NA	NA	NA.	NA	NA	7.27	-0.31	9.24	388.75	3.53	NA	NA	NA	NA	NA	NA	NA
07/18/94	24:00	NA.	ŅΑ	NA	NA	NA	9.07	-0.31	9.24	389.63	3.53	NA	NA	NA	NA	NA	NA	NA
07/19/94	24:00	NA	AK	NA	NA	NA	7.21	-0,31	9-20	387-63	3.49	NΑ	NA	NA	NA	NA	NA	NA
07/20/94	24:00	NA	NA	NA	NA	NA.	7.91	-0.31	9.18	385.50	3.47	NA	NA	NÁ	NA	NA	NA	NA
07/21/94	24:00	NA	NA	NA	NA	NA	7.77	-0.31	9.16	380.13	3.45	NA	NA	NA	NA	NA	NA	NA
07/22/94	24:00	NA	NA	ЖA	NA	NA	7.46	-0.31	9.14	378.38	3.43	NA	NA	NA	NA	NA	ЖA	NA
07/23/94	24:00	NA	NA	NA	NA	NA	6.44	-0.31	9.15	379.00	3.44	NA	NA	NA	NA	NA	NA	NA
07/24/94	24:00	NA	NA	NA	NA	NA	7.88	-0.31	9.15	374.38	3.44	NA	NA	NA	NA	NA	NA	NA.
07/25/94	24:00	NA	NA	NA	NA	NA	7.53	-0.31	9.13	374.75	3.42	NA.	N.A	NA	NA	NA	NA	NA
07/26/94	24:00	NA	NA	N.A.	NA	NA	8.91	-0.31	9.11	375.75	3.40	NA	NA	NA	NA	ЖA	NA	NА
07/27/94	24:00	NA	NA.	NA	NA.	NA	8.12	-0.31	9.06	374.13	3.35	NA	NA	NA	NA	NA	NA	NA
07/28/94	24:00	NA	NA	NA	NA	NA	8.73	-0.31	9.04	369.63	3.33	NA	NA	NA	NA	NA	NA	NA
07/29/94	24:00	NA	NA	NA	NA	NA	7.86	-0.31	9.03	374.38	3.32	NA.	NA	NA	NA	NA	NA	NA
07/30/94	24:00	₩A	NA	NA	NA.	NA	6.91	-0.31	9.01	372.25	3.30	NA	NA	NA	NA	NA	NA	NA
07/31/94	24:00	₩A	NA	NA	NA	NA	8.44	-0.31	9.08	372.13	3.37	NA	NA	NA	NA	NA	NA	NA
08/01/94	24:00	NA	NA	NA	NA	NA.	8.57	-0.31	9.27	375.25	3.56	NA.	NA	NA	NA	NA	NA	NA
08/02/94	24:00	NA.	NA	NA	NA	NA	8.64	-0.31	9.57	382.75	3-86	NA	NA	NA	NA	NA	NA	NA
08/03/94	24:00	NA	NA	NA	NA	NA	8.60	-0.31	9.75	385.13	4.04	NA	NA	NA	NA	NA	NA	NA
08/04/94	24:00	NA	NA	NA	NA	NA.	8.05	-0.32	9.80	390.13	4.09	KA	NA	NÁ	НA	NA	NA.	NA
08/05/94	24:00	NA	NA	NA	NΑ	NA.	13.68	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
08/06/94	24:00	NA	NA	RA	NA	NA	20.00	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	КA
08/07/94	24:00	NA	NA	NA	NA	NA	19.00	NA	NA	NA	NA.	WA	NA	NA	NA	NA	NA	NA
08/08/94	24:00	NA	NA	NA.	NA	NA.	19.63	NA	NA	NA	NA.	NA.	NA	NA	NA	NA	NA	ÑΑ
08/09/94	24:00	NA	NA	NA	NA	NA	39.57	NA	NA	NA	NA.	NA	NA	NA	NA	NA	NA	NA
08/10/94	24:00	NA	NA	NA	NA	NA	19,20	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	ЖA
08/11/94	24:00	NA.	NA	NA	NA	NA	17.31	NA	NA	NA	AK	NA	NA	NA	NA	NA	RA	RA

#### **DISCUSSION OF GRAPHS**

These graphs were created in order to present the data in more informative ways than simple tabulation. This was especially important in showing the relationships between the parameters monitored during the study period. All graphs were derived from appendix E, the daily averaged data for each of the three wells. The other appendices are briefly cited.

The series of graphs were divided into three sections: the first (A) being the combined graphs for each of the three wells for each of the four environmental conditions monitored, the second (B) being another series of graphs, by individual well, comparing each of the environmental conditions, one against another, and the third (C) being a graph of the mean aquifer elevation, for the three wells, compared to rates of pumping at the production well. A discussion of each graph follows.

## A) Series of combined graphs.

Graph 1 - Water Conductivity. The production wells, being fairly remote (2500 ft) from the source of increased conductivity (assumed to be mainly sodium chloride from sea water), had a low range of encountered conductivity values (180 - 560 umhos/cm) as compared to those at the observation wells (Gambell #1 230 - 1624 umhos/cm, Gambell #2 392 - 1828 umhos/cm). Gambell #2, 1700 ft from saltwater, had the highest values and the greatest range in values. This is shown in the graph where the small range of the production wells show on the left and the high ranges of the observation wells shows on the right. There is only a short period of overlapping data for the three wells. Initially, the observation wells had similar, if somewhat higher, conductivities than at the production well, but the conductivity rose rapidly in the observation wells and only slowly in the production wells. If the production well curve for 1994 was similar to that of 1993, by late May it's conductivity would drop off, preceding the drop observed at the monitoring wells. Timing of events at Gambell #2 lead Gambell # 1 by 3 to 4 weeks due to its closer proximity to the saltwater, and its graph also showed a greater rate of change than Gambell #1's graph. The graph curves from the three wells mirrored each other both in timing, except for small delays due to location, and in the shape of the curves, though the dynamic ranges were different (higher peaks and lower troughs). The graph curve from Gambell #2 shows several pairs of small peaks, which may have been caused by the action of seasonal/tidal events in the nearby ocean. They either do not show on the graphs of the other wells or are much reduced. The unexpected rise of conductivity at Gambell #1 to values higher than that at Gambell #2 in mid May '94 is not simply explained. A dilution affect, possibly surface snow melt, may have caused the Gambell #2 well to temporarily drop from its steady rise in observed conductivity, or some feature of the system may have allowed water with higher conductivity to bypass the lower well, Gambell #2, and yet still have affected the upper well. This affect was not observed at the production well.

Graph 2 - Water Surface Elevations Relative to Mean Low Low Water (MLLW) The production well had a higher initial static water elevation than the monitoring wells at the start of the monitoring period on January 5, 1994. This caused concern that there could have been an error in the survey and installation of the recording devices and that the water levels might actually have been closer than indicated in the graph. Further scrutiny of the data showed this was not the case, since the production well water elevation rapidly dropped down to near and even below the water elevations of the monitoring wells, shortly after January 23, 1994. The differences were caused by pumping from the production well. On June 17, 1994, after a period of recovery, the elevation in the monitoring wells rose to a level only slightly below the maximum observed at the production well on June 24, 1993.

The smoothing effect of the 24 period moving average on the production well graph lowered the graphed values to 5.2 ft instead of 6.66 ft as recorded in the dataset, app E on June 24, 1993. The high porosity of the gravel and the lower pumping rate at those times allowed this comparison. Because of the high porosity, the differences between the water elevations at each well was small when compared to the total change in water elevation observed within the aquifer. The graph also showed a cyclic periodicity to the drawdowns and recoveries, although the decline in the second period was more rapid and resulted in a longer low water surface elevation period than that of the first period. Lack of production well data for the end of this period prevented confirmation of any distorted periodicity.

The water elevations in the production well dropped steadily down as the season progressed: to the zero level (MLLW) in late March 1993 and late February '94, and then below the zero level to the extreme lows encountered in late March and early April (data from the production well ceased before the minimum was reached in 1994). The observation wells dropped to still lower elevations in late April and early May 1994, with Gambell #1 lower than Gambell #2, indicating that the production well should drop similarly. This was not directly verifiable because of only a small overlap in the period of data collection between the monitoring wells and the production well, complete 1994 data not having been presented for inclusion in the report. Changes in water elevation were mirrored in both observation wells, with Gambell #2 less effected than Gambell #1, and both less affected than the production wells. This was true for both increases and decreases in water elevation, with the production wells having the greatest dynamic range in water elevation and Gambell #2, the least. Prior years data indicated that the production well should recover to a higher elevation than the observation wells.

Graph 3 - Air Temperature. This figure was included to show the very similar atmospheric temperatures experienced by sensors located at each observation well. While most of the two graphs overlap, Gambell #2 showed a greater dynamic range than Gambell #1. The overall patterns were very consistent. No air temperature was available from the pumphouse. Lows occurred in late March and highs in late August, at which time data collection ceased.

Graph 4 - Water Temperature. The water temperature in the production well was relatively high, and it fluctuated between 2.3°C and 4.2°C through the year. This may have been due to standing time in the heated pumphouse, because it is unlikely for the groundwater at that location to reach so high a temperature. The observation wells started out at just below 0.8°C and declined to below 0.0°C with Gambell #2, reaching to -0.32°C, being about 0.25°C colder than Gambell #1. This may have been related to the distance from the point of recharge, the main thermal input into the system, and also to the close proximity of the underlaying permafrost. No evidence of thermal recovery was apparent when data gathering ceased. The pressure transducer indicated freezing at the bottom of the well when the temperature at Gambell #2 dropped from -0.31°C to -0.32°C on August 4, 1994.

# B) Individual Well Graphs, with combined parameters.

Graphs 5, 8 & 11 Water Conductivity and Water Surface Elevation. These graphs showed an almost inverse relationship between water elevation and conductivity at each of the observation wells and at the production well. The "inverse" relationship held for the production well, Gambell #1 and most of Gambell #2. During May and early June at Gambell #2, an anomaly occurred when the conductivity rose at a rate similar to the rise in water elevation, after having started to decline as expected. After reaching a new high, the conductivity levels then declined again, having been delayed by about a month

as compared to Gambell #1 and the production well. At the end of this graph there was an indication that the inverse relationship was being restored and conductivity had regained it's initial values. This anomaly may be related to the unexpected rise in conductivity at Gambell #1 to levels higher than at Gambell #2, during the preceding two weeks, as discussed above for Figure 7. Gambell #2 had the greatest dynamic range in both graphs and the production well the least.

Graphs 6, 9 & 12 - Water Conductivity and Water Temperature. These graphs show that initially the conductivity rose as the temperature dropped but as the temperature leveled out at the low for the remainder of the period, the conductivity rapidly rose, reached a maximum and then dropped down to its initial values with almost no change in temperature. This is shown in Figure 15, at Gambell #2, and, by extrapolation of the graphs, also at Gambell #1 where the relevant data was lost and the pumphouse where it was not recorded. This extrapolation is justified by the repetitive pattern shown at the pumphouse. The graphs indicate that the conductivity and temperature were not directly related and that the initial inverse relation was just circumstantial - this is especially evident in the graph for Gambell #2. The graph for the production well does not yield any useful temperature information since the water temperature is questionable, probably having been heated.

Graphs 7, 10 & 13 - Water Temperature and Water Surface Elevation. These graphs show a steady, almost linear relationship between declining temperature and declining water elevation and then an abrupt break in the relationship as water elevation rapidly rose while temperatures remained more or less constant at their seasonal lows. Unfortunately, monitoring ceased before the temperature recovery took place. This recovery must take place between late August, which showed constant low temperatures, and late December, where the decline in temperatures had already begun again, if the temperature environment was cyclical as expected. Thermal degradation, that is intrusion of permafrost into the aquifer, could have distorted this cycle. Recovery in temperature is expected to be slow and uniform due to the thermal inertia of the gravels and the infiltration of "warmer" water from the sources being not much warmer since it was mostly snow melt or runoff from groundwater springs. Once again, the data from the pumphouse were almost meaningless due to the questionable water temperatures.

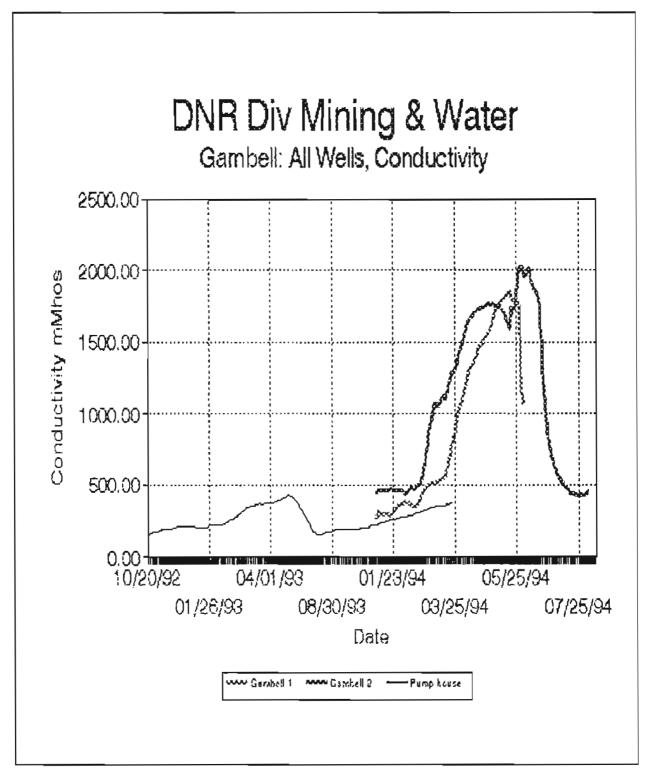
### C) Mean Aquifer Water Surface Elevation and Pumping Rate.

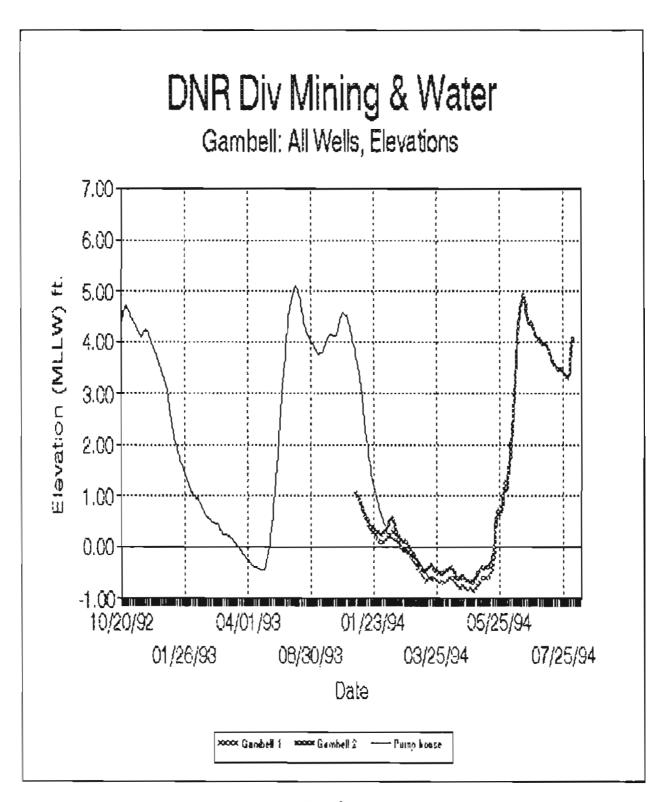
Graph 14 - Mean Aquifer Water Surface Elevation and Pumping Rate. This graph shows that the mean pumping rate varied seasonally, with the highest rates of pumping occurring in the late winter and early spring, coinciding with the lowest water elevation levels in the aquifer. Mean aquifer levels were used since the porosity of the gravels reduced the differences between the wells to negligible amounts as compared to the total dynamic range in water elevation within the aquifer itself, as confirmed by the short period of overlapping water elevation data, as shown in Graph 2.

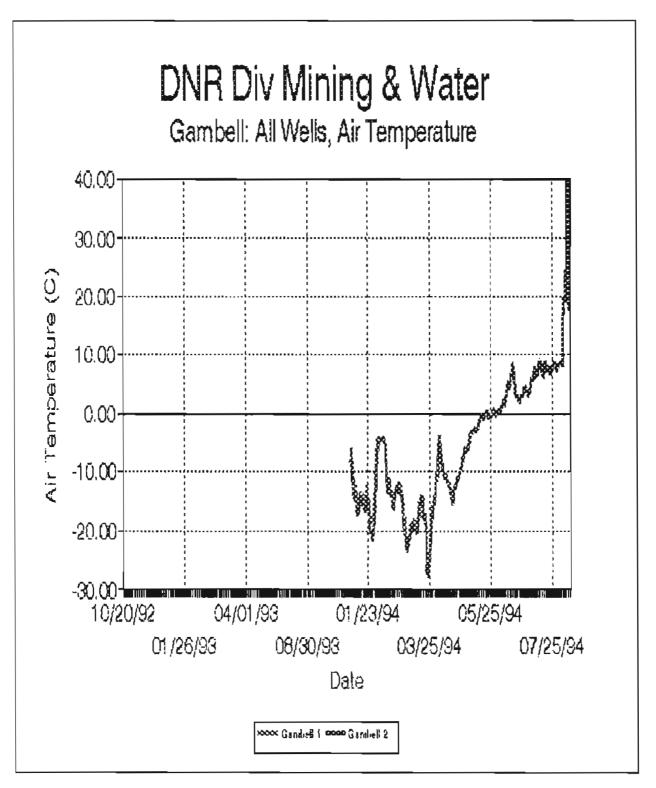
Water elevation of the aquifer varied almost independently of the rate of pumping, even though it appears to have an inverse relationship in the graph. It was more a function of recharge from the sources and discharge into the ocean than management of the rates of pumping. This is shown in the period from 08/30/93 to 01/23/94, where the stage fell rapidly, despite the rate of pumping having been relatively low. This non-relationship only held when aquifer elevations were relatively high; where they were low, excess pumping caused the levels to drop below the otherwise equilibrium condition. The equilibrium condition was approached when recharge from the sources reached minimum levels in late winter, and appears to have matched the reduced outflow into the ocean. At that time the minimal

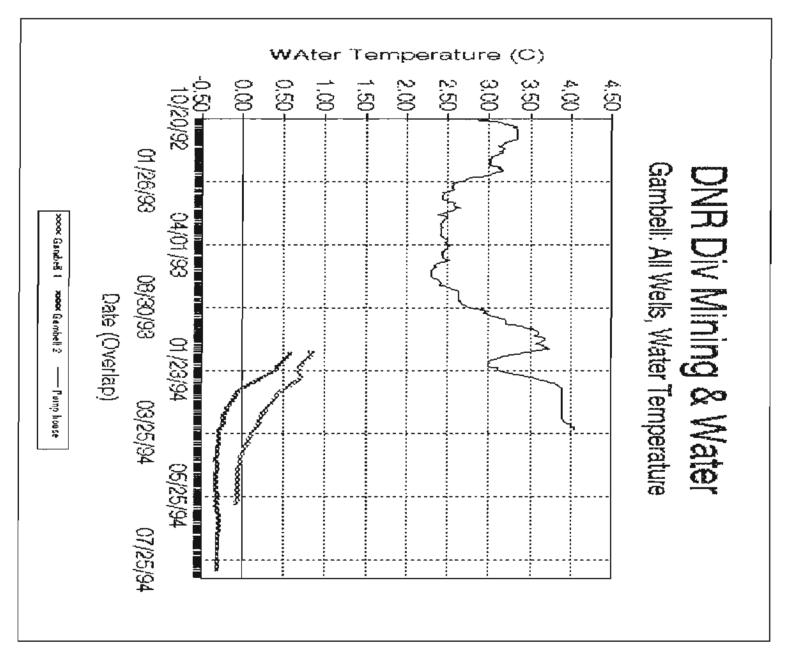
recharge would have allowed a density gradient to be established between the saltwater and fresh water interface. At equilibrium, the greater density of saltwater would have caused the elevation of fresh water in the aquifer to be somewhat higher than MLLW. A reduction of fresh water surface elevation in the aquifer a this time would be balanced by the influx of saltwater, resulting in the restoration of the equilibrium water elevation to some extent, but with an intrusion of saltwater into the body of the aquifer.

The graph suggests that the aquifer can easily take a rate of pumping of about 14 gallons per minute (gpm), while a rate of 16 to 17 gpm is barely sustainable during periods of low water elevation (notice the two short low gradient parts of the water elevation curve that occurred in late February of both 1993 and 1994). It appears that rates exceeding 17 gpm caused the mean water elevation to dip below MLLW elevation and hence allowed saline penetration into the aquifer. Low pumping rates at this time would be expected to allow the equilibrium level to be established and maintained. Any reduction of water elevation to below this level (by pumping) would cause a reversal of flow direction within the aquifer. Higher pumping rates are feasible during the period from early June through late December when water elevation within the aguifer is also high (3-5 ft above MLLW), but that lower levels of pumping should be observed through the remainder of the year (late December through early June). This is especially true when the water elevation drops to near 0.33 ft above MLLW. Low water elevation pumping rates should probably not exceed 16 gpm (23,000 gallons per day), while high water elevation pumping rates could easily exceed 18 gpm (26,000 gallons per day) with 21 gpm (30,000 gallons per day) appearing quite sustainable. This was evidenced by the fact that the graph tended to level off even during the high pumping rates encountered during February 1994, a low water elevation period. If this pumping had taken place during high water, the effect would have been minimal.









Graph 73

