

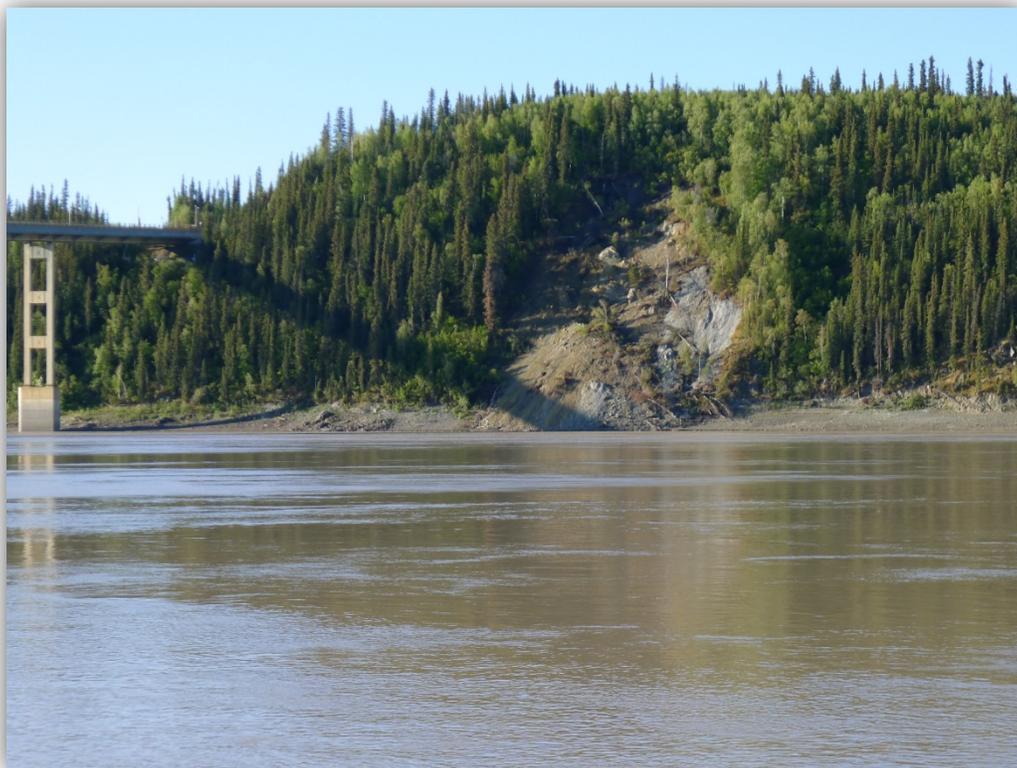
Division of Geological & Geophysical Surveys

PRELIMINARY INTERPRETIVE REPORT 2013-6

**YUKON RIVER BRIDGE LANDSLIDE:
PRELIMINARY GEOLOGIC AND GEOTECHNICAL EVALUATION**

by

Rich D. Koehler, Richard D. Reger, Karri R. Sicard, and Eleanor R. Spangler



Yukon River bridge landslide viewed from the north bank of the Yukon River. Photo by Rich D. Koehler

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YUKON RIVER BRIDGE LANDSLIDE: PRELIMINARY GEOLOGIC AND GEOTECHNICAL EVALUATION

by Rich D. Koehler¹, Richard D. Reger², Karri R. Sicard³, and Eleanor R. Spangler³

Introduction

This report presents the findings of a geologic and geotechnical evaluation of a landslide at the Yukon River bridge, conducted by the State of Alaska, Division of Geological & Geophysical Surveys (DGGs) through a reimbursable services agreement with the State of Alaska Department of Transportation & Public Facilities (ADOT&PF). The E.L. Patton Bridge spans the Yukon River at the Dalton Highway crossing approximately 90 miles northwest of Fairbanks, Alaska (fig. 1). The bridge is a vital link on the transportation corridor between Prudhoe Bay and Fairbanks and supports the trans-Alaska oil pipeline.

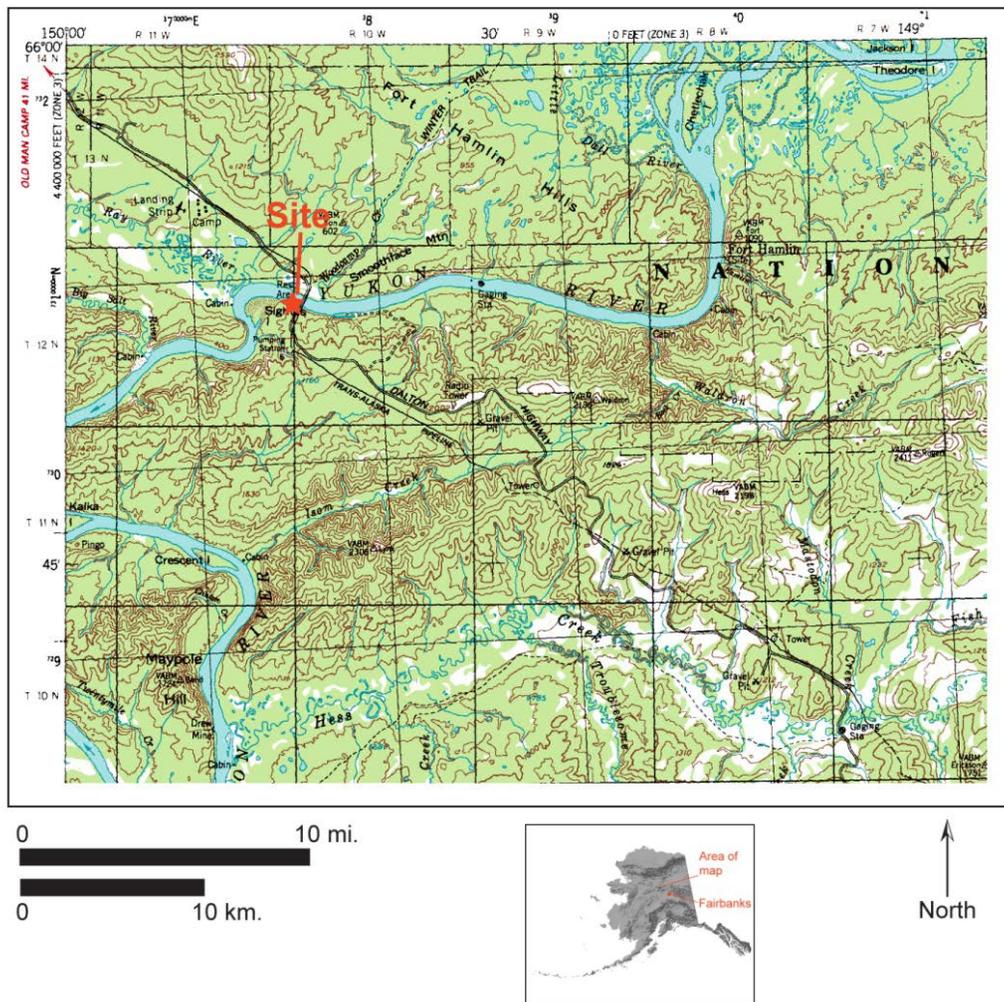


Figure 1. Topographic map of the Yukon River bridge vicinity. Location of landslide shown by red star.

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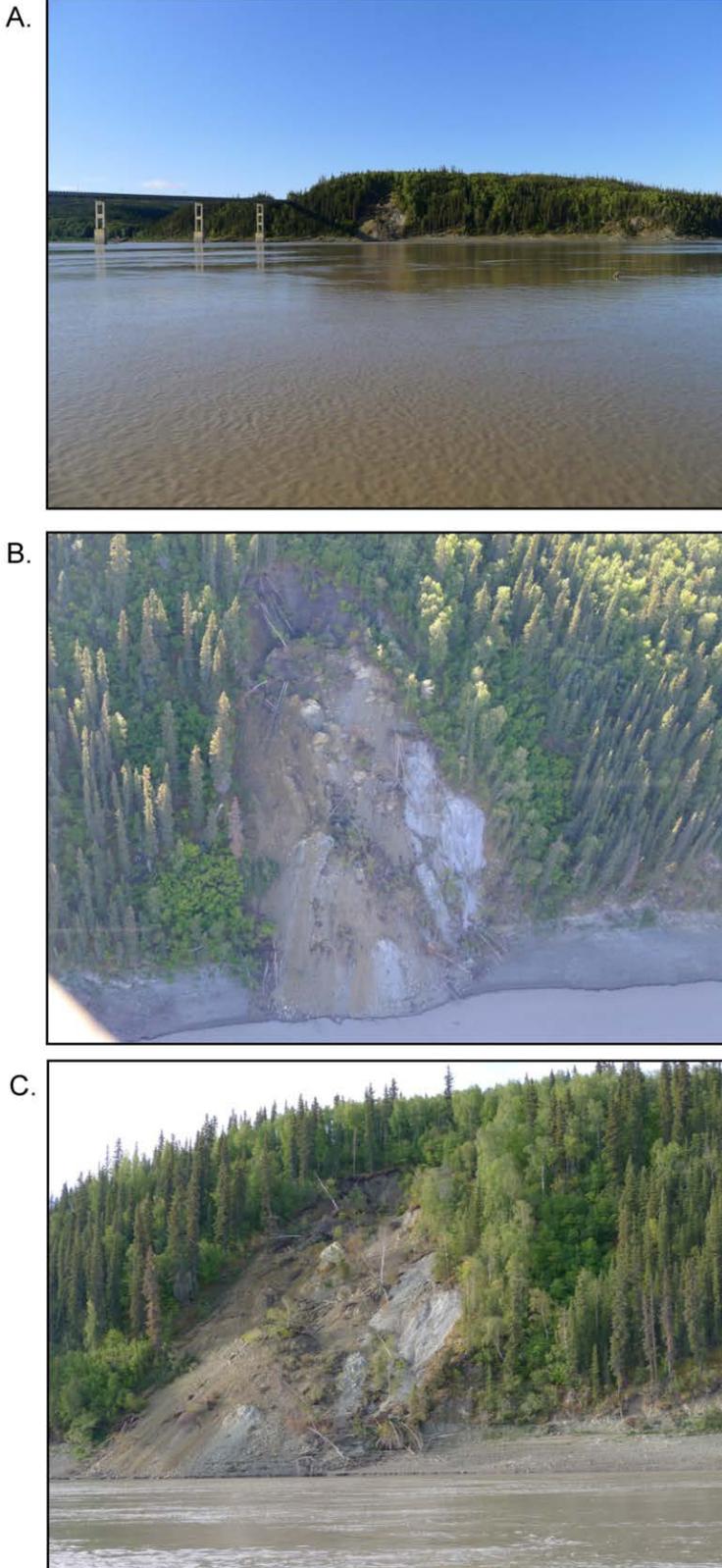


Figure 2. Photographs of the Yukon River landslide. A. View from the north bank of the river. B. Aerial view of slide from helicopter. C. Closer view of slide from the river.

The Yukon River bridge landslide occurred in fall 2012 between approximately 375 and 575 feet west of the bridge (fig. 2). Although there was no damage to the bridge foundation, the landslide’s close proximity to the bridge and concerns over additional failures prompted multiple evaluations, including landslide documentation, drainage assessments, and geotechnical studies, among others. The main purpose of this study is to provide baseline geotechnical and geomorphic observations to supplement concurrent slope-stability analyses being conducted by ADOT&PF, Alyeska Pipeline Service Company, and their consultants.

The following tasks are included in the scope of this evaluation:

- Examination of published geologic reports, LiDAR imagery, and geologic maps;
- Aerial reconnaissance of the bridge vicinity by helicopter on August 25, 2013;
- Ground reconnaissance along the base of the bluff below the bridge and around the landslide between August 26 and 29, 2013;
- Preliminary evaluation of rock strength and discontinuity data;
- Preliminary evaluation of principal stress orientations;
- Preliminary evaluation of slopes and landslide geomorphology;
- Preparation of this report.

Yukon River bridge and landslide

The E.L. Patton Bridge was originally built in 1974–1975 to facilitate construction of the Trans-Alaska Pipeline System (TAPS). Use and maintenance of the bridge and Dalton Highway were officially turned over to the State of Alaska in 1978. The bridge is a girder bridge design measuring 2,295 feet long and 30 feet wide with a timber deck that slopes upward about 200 feet from the north to the south bank of the river. It is supported by five main in-stream piers, and abutments on each bank. It remains the only bridge crossing of the Yukon River in Alaska. The Dalton Highway and the Trans-Alaska Pipeline System rely on the bridge to connect Fairbanks to

the Prudhoe Bay oilfields, ensuring an uninterrupted corridor for the transportation of supplies and personnel. Any compromise to the bridge's integrity could potentially have immediate and severe consequences to the State's economy and environment.

Sometime during late fall 2012, a landslide occurred on the steep bluff above the south shore of the Yukon River between 375 and 575 feet downriver from the E.L. Patton Bridge (fig. 2). The slide originally was reported by Alyeska security on November 30, 2012. Subsequent field inspections conducted by Alyeska and ADOT&PF on December 7, 2012, and January 18, 2013, determined that the slide may have been controlled by highly fractured and altered weak zones in the rock mass (Frank Wuttig, oral commun.). These weak zones were inferred to be related to a potential fault zone encountered during construction of bridge pier 4. Additionally, it was noted that the slide occurred in perennially frozen ground. Given the 2012 slope failure and the occurrence of potentially adverse ground conditions, it was recommended that additional slope monitoring and geotechnical investigations be undertaken. This report contributes to those ongoing investigations.

Regional geology and geomorphology of the Yukon River bridge vicinity

The Yukon River bridge landslide is located along the north-facing bluff of the Yukon River canyon directly west of the E.L. Patton Bridge, approximately 20 miles downstream from the southwestern margin of Yukon Flats (fig. 1). The Yukon River essentially marks the boundary between the Kokrine–Hodzana Highlands, the Rampart Trough, and the Yukon–Tanana Upland physiographic provinces (Wahrhaftig, 1965).

The regional geology of the vicinity of the site is shown in figure 3. Bedrock lithologies near the Yukon River bridge are primarily mapped as Mississippian–Triassic Rampart Group rocks, but minor Tertiary volcanic and sedimentary rocks are present to the southeast (Weber and others, 1992). The Rampart Group consists of a complex assemblage of tectonically deformed mafic igneous and sedimentary rocks. The mafic igneous rocks are intrusive and extrusive and range from aphanitic greenstone to coarse-grained diorite and gabbro, with very rare occurrences of ultramafic rock (Weber and others, 1992). These rocks locally include pillows, amygdules, and interbedded sedimentary rocks. Sedimentary rocks of the Rampart Group, defined by Weber and others (1992), consist of argillite, chert, graywacke, shale, and limestone. Shale units are typically dark gray to black, graphitic, calcareous, and fissile. Argillite and chert units are medium–light gray to greenish gray, locally banded, conglomeratic or brecciated. Graywacke metasandstones are greenish gray, fine to medium grained, and locally micaceous, feldspathic, quartzose, or calcareous. Minor limestone units are bluish gray, fine grained, and laminated. The Rampart Group may correspond to the Tozitna stratigraphic belt in the Livengood area to the south (Dover, 1994; Mertie, 1937; Jones and others, 1984).

In the upland south of the river, tributaries of the Yukon River are incised $\leq 1,700$ feet below ridge crests in rocks of the Rampart Group. Ridge crests are blanketed by 5–50 feet of frozen, locally ice-rich upland loess, and intervening lowlands and stream valleys contain thick, frozen, ice-rich loess and retransported silt (Kreig and Reger, 1982; Shur and others, 2010). These deposits are roughly equivalent to Quaternary loess and colluvium (Qlc) and Quaternary silt (Qsu) mapped by Weber and others (1992) (fig. 3). Through its canyon, the Yukon River winds past 800- to 1,000-foot-high bedrock ridges that were steeply truncated by colossal middle to late Pleistocene outburst floods (Froese and others, 2003; Thorson and Dixon, 1983). At least 160 feet of frozen, fine-grained fluvial and eolian sediments form a surface 200–300 feet above the modern river (Clement, 1999). That surface is modified by thermokarst processes, including formation and expansion of thermokarst pits and gullies, collapse of deep yedoma depressions, and local development of thaw-induced, retrogressive landslides in the river-cut silt bluffs. A pair of late Holocene fluvial terraces with sand and silt cover discontinuously flanks the modern river channel.

The Ray River lowland contains a thick, perennially frozen fill of ice-rich, fine-grained sediments that accumulated during massive late-Pleistocene outburst floods in a major slackwater basin just upriver of a hydraulic dam that formerly existed where the flooding Yukon River abruptly turned south and entered a narrow canyon (Thorson,

1989). Northeast of the Ray River lowland the Fort Hamlin Hills, which are composed of Rampart Group that is weathered to depths ≥ 5 feet, rise to elevations of 1,500 to 3,150 feet. Up to one foot of loess discontinuously covers bedrock and colluvium on upper slopes, and frozen, locally ice-rich loess and retransported silt reach thicknesses of ≥ 100 feet on middle and lower slopes. Perennially frozen alluvial–colluvial fans coalesce at the mouths of stream drainages cut into the southern flank of the Fort Hamlin Hills, forming an ice-rich apron crossed by the TAPS and Dalton Highway routes.

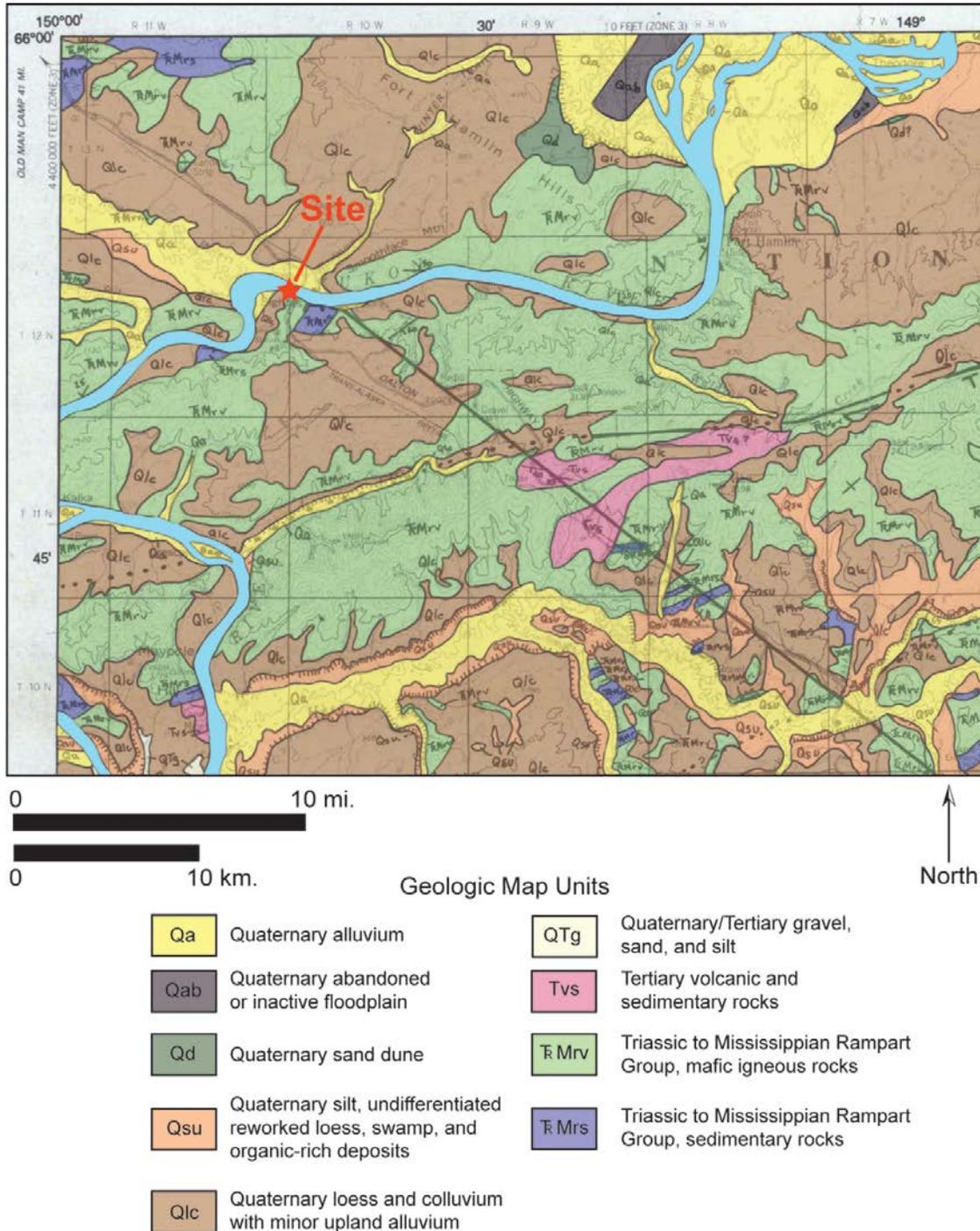


Figure 3. Geologic map of the site vicinity from Weber and others (1992). Geologic units are colored to emphasize unit boundaries. Location of the Yukon River bridge landslide is shown by red star.

Yukon River bridge landslide field review

Methodology

The Yukon River bridge landslide field review was performed August 25–29, 2013, by Rich Koehler, Karri Sicard, and Eleanor Spangler of DGGS and Richard “Dick” Reger of Reger’s Geologic Consulting. A helicopter reconnaissance organized by Frank Wuttig of Alyeska Pipeline Services Company provided an overview of the landslide and general observations of the slope conditions upstream and downstream of the bridge. Robert Joseph of Stevens Village provided boat transportation to access the lower bluff and landslide area and to observe slopes along the south bluff upstream and downstream of the bridge.

Bedrock outcrops along the base of the Yukon River bluff were inspected for the presence of faults, fractures, shears or weathering zones, and/or other features that could provide information from which to infer subsurface conditions of bedrock farther upslope. Quantitative descriptions of rock mass and discontinuity data are based on the methodology of ISRM (1978). Rock mass and discontinuity survey data sheets from the Alaska Field Rock Classification and Structural Mapping Guide (ADOT&PF, 2003) were used to record the field observations. Key rock characteristics that were documented include lithology, color, grain size, field compressive strength, rock mass fabric, block size, and state of weathering. Discontinuity surveys at each outcrop station include information on type of discontinuity, dip, dip direction, persistence, termination, aperture, nature of filling, strength of filling, surface roughness, surface shape, waviness, joint roughness coefficient, and presence of water. Detailed definitions for each of these parameters are provided in ADOT&PF (2003). Discontinuity orientations were measured with a Brunton compass, using standard geologic field techniques.

The slope and landslide evaluation made use of both office and field techniques. Pre- and post-landslide LiDAR data collected by Hubbard and others (2011) and Alyeska Pipeline Service Company, respectively, were used to generate slope profiles and evaluate possible past slope failures. These two data sets were also used to compare the pre- and post-landslide ground surface. The combined LiDAR and field observations were used to quantitatively evaluate possible failure mechanisms for the 2012 landslide.

Results of rock mass and discontinuity evaluation

We evaluated rock strength and discontinuity characteristics along the base of the bluff and riverbank at 13 bedrock field stations distributed between approximately 850 feet east of the Yukon River bridge and approximately 1,150 feet west of the bridge (fig. 4). An additional zone of intensely sheared graywacke between stations 10 and 11 was mostly covered by beach gravels and boulders, and thus not described in the field as a separate station. Observations from this zone are provided in the following discussion. Photographs documenting bedrock features at each outcrop station along the base of the bluff are included in Appendix A. An additional observation station was located at the crest of the landslide. The location of each station and approximate bedrock contacts are shown on a strip map of the transect (fig. 4). GPS coordinates for each station are listed in Table 1. Detailed observations and inventory of rock discontinuity measurements are recorded in the field evaluation sheets in Appendix B.

Bedrock lithologies along the base of the Yukon River bluff consist of diorite, gabbro, graywacke meta-sandstones, greenstone, metabasalt, and chert (fig. 4). Table 2 shows rock-mass information for each bedrock field station. In general, the rock mass is characterized as strong to very strong rock that is fresh to slightly weathered with local zones of moderate weathering. The freshness of the rock is likely a reflection of ice scour and limited exposure to surface conditions (i.e., <15,000 years.). Limited inspection of the roadcut at the south abutment of the bridge indicates that the rock may grade upslope to a more weathered condition (moderately to highly weathered?); however, this outcrop was not studied in detail. The rock character along the base of the bluff is generally blocky (small to medium in scale) with discontinuous zones of very small shattered blocks and closely fractured to crushed zones. The graywacke metasandstone is the only rock type with a discernible fabric, includ-

ing slightly metamorphosed and deformed beds. However, the deformed bedding is irregularly folded and does not have a consistent orientation.

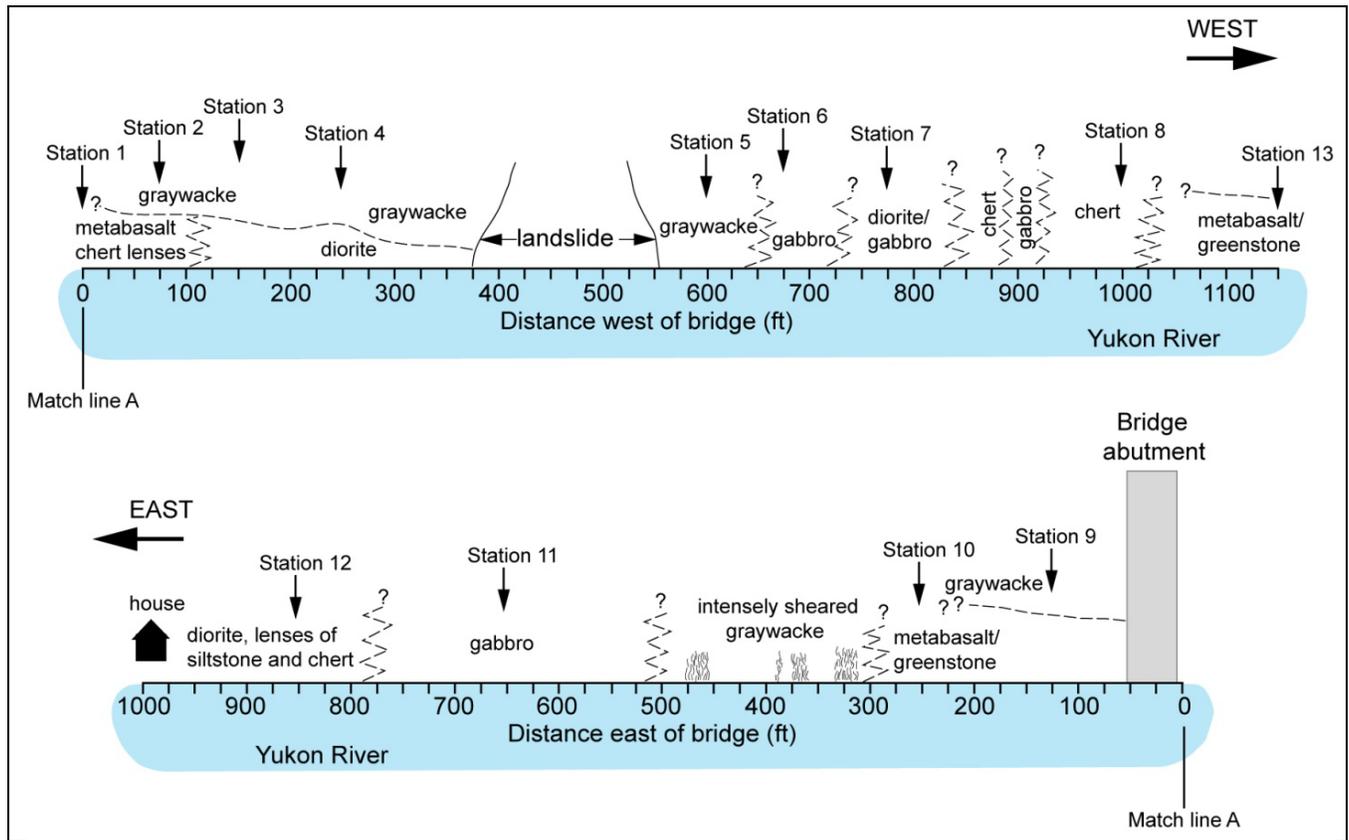


Figure 4. Location of field stations and inferred bedrock contacts along the Yukon River bluff transect. Area west of the bridge is shown at top; area east of the bridge is at bottom.

Table 1. Locations of data stations. GPS data collected in WGS 84.

Station number	GPS point	Latitude	Longitude
1	5	65.87386703	-149.724802
2	6	65.87396703	-149.725185
3	7	65.87400097	-149.725785
4 (a and b)	8	65.874034	-149.725752
5 (a and b)	9	65.87451696	-149.728152
6	10	65.87496699	-149.728452
7	11	65.87491703	-149.729318
8	12	65.87515097	-149.730452
9	13	65.87381699	-149.724118
10	14	65.87370099	-149.723002
11	15	65.87271703	-149.721452
12	16	65.87230104	-149.720385
13	18	65.87573804	-149.732431

Table 2. Rock mass data for individual measurement stations.

Station	Lithology	Color	Grain size	Compressive strength	State of weathering	Fabric	Block size	Number of discontinuity sets
1	Greenstone/ metabasalt	Dark greenish gray to grayish green	Very fine	R5	Fresh	Blocky	Very small	3–4
2	Metabasalt	Dark greenish gray	Fine to very fine	R5	Fresh	Blocky	Medium	>5
3	Diorite	Reddish black to green	Fine	R5	Slight	Blocky	Medium	5
4a	Diorite	Dark reddish gray	Fine	R4	Moderate	Blocky	Small	5
4b	Graywacke metasandstone	Light bluish gray	Very fine	R5	Slight	Blocky to shattered	Small	4
5 (a and b)	Graywacke metasandstone	Dark greenish gray to light green	Fine to very fine	R4–R5	Fresh to slight	Blocky, columnar, shattered	Medium	3
6	Gabbro	Light brownish gray	Fine	R5	Fresh to slight	Blocky	Medium	>4
7	Diorite to gabbro	Dark greenish gray	Fine	R5	Slight	Blocky	Medium	5
8	Chert	Brownish red to greenish blue	Very fine	R4	Slight	Shattered	Very small	3
9	Metabasalt	Dark reddish to yellowish gray	Very fine	R4	Slight	Blocky	Medium	2
10	Basalt/ greenstone	Dark greenish gray	Very fine	R5	Slight	Blocky	Medium	4
Area between 10 and 11	Graywacke metasandstone	Greenish gray to olive green	Fine	R1–R4	Slight	Shattered	Very small	3
11	Gabbro	Dark grayish black	Fine	R5	Moderate	Blocky	Medium	3
12	Diorite	Dark bluish gray	Fine	R5	Slight	Blocky	Small	3
13	Metabasalt/ greenstone	Dark greenish black	Fine	R5	Slight	Blocky	Small	4

Discontinuity data evaluation

Jointing is pervasive throughout the rock mass for all bedrock types and, together with local faults and shear zones, divides the rock into discrete blocks and slabs. Joint dips are predominantly high angle (Appendix B) and may have formed during uplift or unroofing of the Yukon–Tanana Upland. Joint spacing is typically close to moderate in all rock types except chert, which exhibits extremely close to very close spacing possibly related to bedding-parallel shearing, or due to the very fine grain size. Joint surfaces are typically tight and smooth to slightly rough and planar with scattered slickensided shear surfaces. Scattered black oxidation staining and thin fillings of calcite and quartz are present on joint surfaces, however the majority of joints are clean. Aperture widths are commonly tight to very tight, with scattered joints partly open to open and rare very wide openings. Evidence of water flow was not observed on any discontinuity surface.

A wide area of sheared chloritic graywacke metasandstone with zones of more intense shearing and alteration is present between approximately 300 and 475 feet east of the Yukon River bridge (fig. 4). The graywacke between shear zones is strong rock (R4). The shear zones are characterized by very weak (R1), shattered and brecciated rock in a grayish green clay matrix with calcite veins. Shear zones are variably oriented with clusters striking 60°–90°

azimuth and 145° – 170° azimuth with vertical dips. The zones are >18 inches wide, closely spaced, and irregularly curved with calcite present as skins on shattered clasts. Individual shear planes in the zones are tight to open and have orientations similar to the major shear zones.

The 13 bedrock field stations are characterized by an array of joint and fault orientations. Rose diagrams and equal-area stereonet projections of the discontinuity data were plotted using the program Stereonet 8 (Allmendinger and others, 2012). Figures 5 and 6 show rose diagrams of joint orientations for each rock type and field station, respectively. The measurements were reflected across the rose diagrams for visual ease, so that both directions of each plane are visually represented. The bin size is 10 degrees, and the discontinuities are not weighted by length, persistence, spacing, or other factors.



Figure 5. Rose diagrams of rock discontinuity data by rock type. Measurements are reflected across the rose diagrams so that both directions of each plane are represented.

Discontinuity orientations for the different rock types (fig. 5) show clear distinctions. Chert and dioritic rocks have similar fracture patterns with dominant N–S joint sets, and subdominant WNW–ESE and NE–SW fracture sets. These rock types are both fine grained, and the fractures may have broken the rock without being influenced by crystal size or pre-existing weaknesses. Fracture patterns in the gabbroic rocks are characterized by NE–SW and E–W fracture sets. Graywacke metasandstones are characterized by three dominant sets, NW–SE, NE–SW, and WNW–ENE. Pre-existing weaknesses related to bedding in the graywacke metasandstones may have been exploited by the fractures. Greenstones (metabasalts) have fracture patterns that are similar to the dominant WNW–ESE set in the graywacke metasandstones, but also contain NW–SE and NE–SW fracture sets. Shear zones and faults in the greenstones may have influenced the discontinuity orientations. The maxima of the discontinuities are WNW–ESE ($\sim 285^{\circ}$ – 95° azimuth), N–S ($\sim 355^{\circ}$ – 175° azimuth), and NE–SW ($\sim 30^{\circ}$ – 210° azimuth).

Additional patterns are evident in the rose diagrams for individual field stations (fig. 6), however because each station has only about 20 measurements, the patterns may reflect uneven sampling. The rose diagram for the combined dataset of all stations includes 610 discontinuity measurements (fig. 6). This plot generally shows the same major discontinuity sets as seen in the different bedrock type plots but is more scattered, illustrating the diverse complex fracture pattern that characterizes the site.

The strike and dip of the discontinuity surfaces and poles to discontinuity planes were also plotted on equal-area stereonet projections (fig. 7). For the entire data set, no distinct patterns are evident in the composite stereonet projections of the strike and dip measurements (fig. 7A). As with the rose diagrams, grouping stereonets by station and rock type may reveal more robust patterns, however, this is beyond the scope of our study. The plot of the poles to the discontinuity planes shows several distinct clusters in the main populations (fig. 7B). The lines around the clusters are 1 percent area contours. The main plane orientations dip nearly vertical (scattered toward the edges of the net) and are similar to the rose diagrams; the dominant WNW–ENE planes are the cluster of poles plotting slightly E of N, and the dominant N–S planes are the cluster of poles near the E and W edges of the net. The NE–SW planes do not show up as a large cluster of poles, but there are small clusters dipping less vertically ($\sim 75^{\circ}$) in the NW and SE quadrants. The last cluster of poles, approximately 45° E of N near the plot edge, is the near-vertical NW–SE set of discontinuity planes.

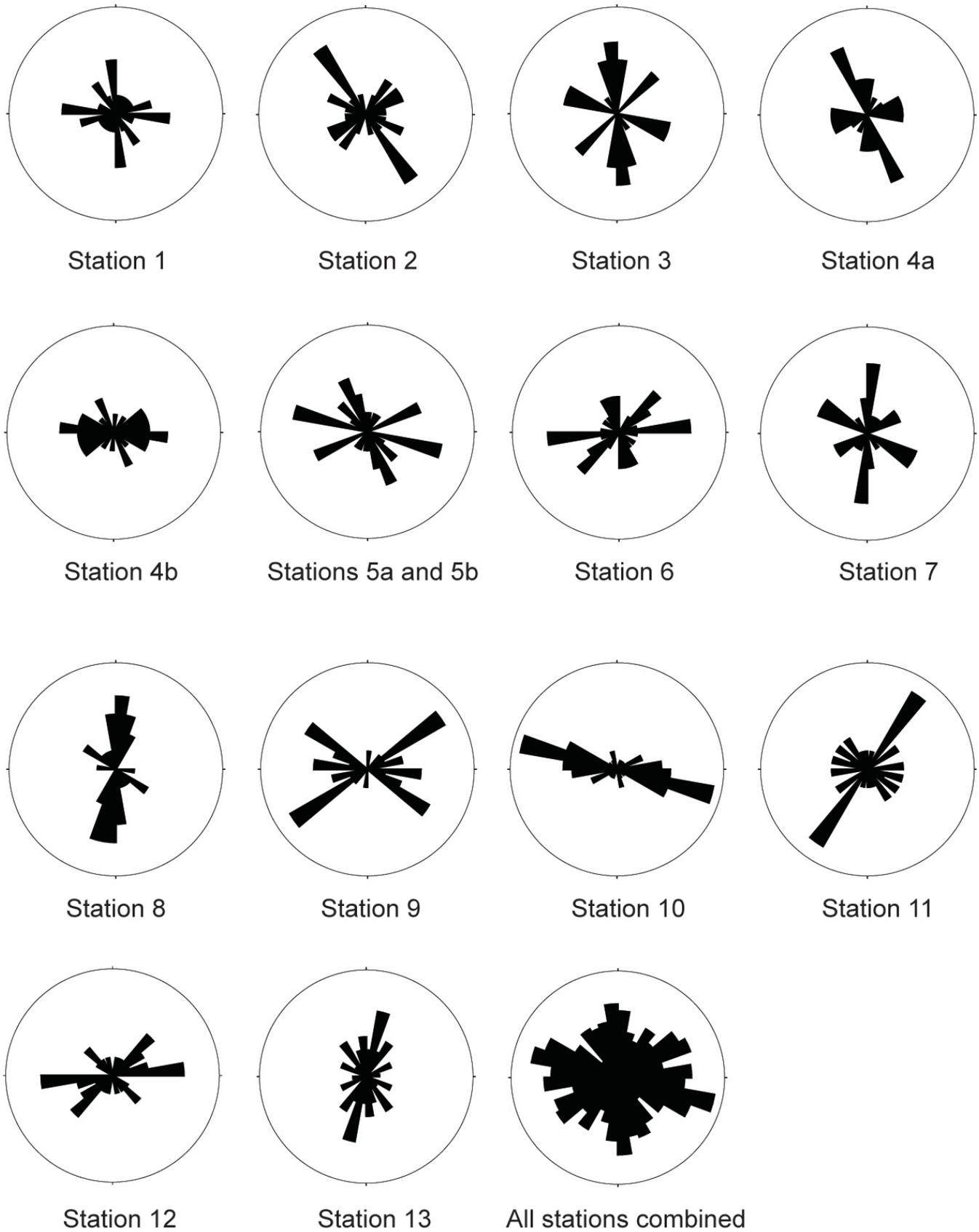


Figure 6. Rose diagrams of rock discontinuity data from each measurement station, and composite plot of the combined dataset (lower right). Measurements are reflected across the rose diagrams so that both directions of each plane are represented.

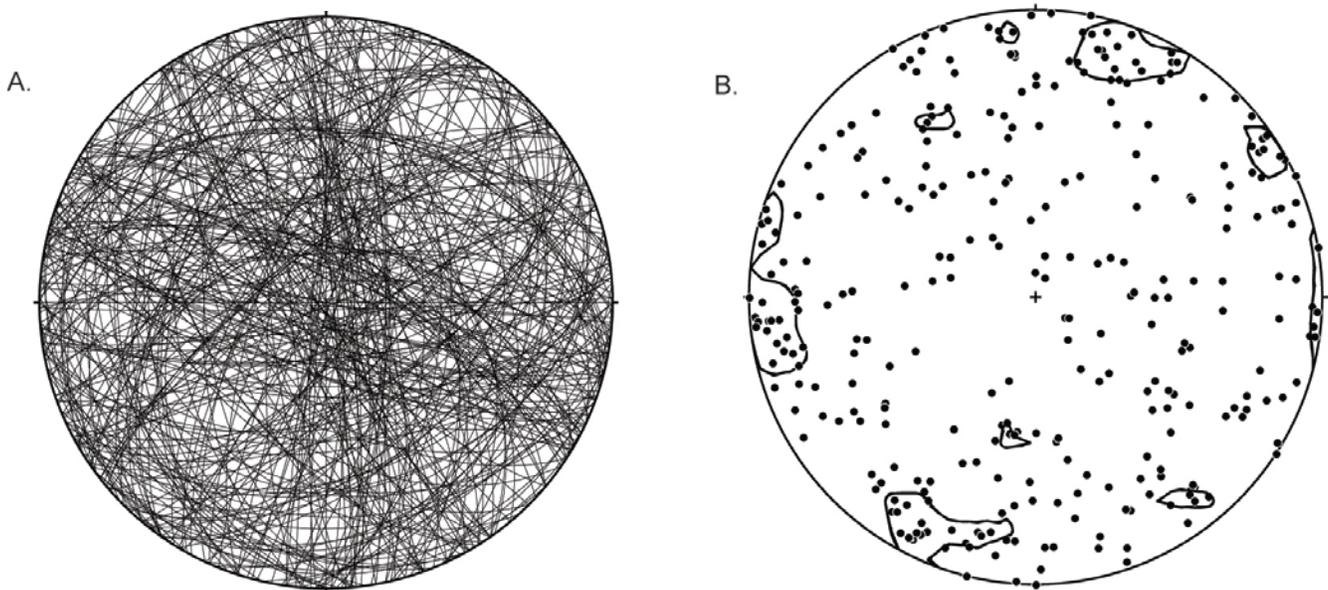


Figure 7. Stereonet projections of rock discontinuity data. A. Equal area stereonet projections for all discontinuity data. B. Poles to the discontinuity planes for all discontinuity data. Lines around clusters are 1 percent area contours.

There are additional ways to analyze the discontinuity data, but these studies should be driven by the goals of future slope stability evaluations and are beyond the scope of this evaluation. For example, discontinuities could be weighted based on important factors such as their length, persistence, spacing, oxide staining, fillings, and other characteristics. The discontinuities could be evaluated spatially, which could reveal patterns related to proximity to shear zones or large faults. Different blocks may exist in areas with different stresses acting on them currently or in the past. Additionally, the fractures proximal to the landslide could be compared to more distal fractures to evaluate whether there are more-dominant fracture sets that could have controlled the bedrock failure in the area of the landslide. A preliminary test of this hypothesis did not yield patterns.

Fault evaluation

Evaluation of fault orientations can provide insight into the state of stress at the time of faulting. Large datasets are needed to determine the current and past stress fields, since stress usually changes through time, and records of these different states of stress are recorded in the rocks. Cross-cutting relations and mineral growth on fault surfaces are extremely useful for evaluating these stresses. Also, conjugate fault sets are much more instructive than independent fault planes in evaluating and determining the state of stress. The pattern of slip on a simple conjugate array of mesoscopic faults is directly related to the state of stress at the time of faulting.

We measured 37 mesoscopic faults in the area around the Yukon River bridge, 33 of which had shear fractures with slicken surfaces. The lack of openings, water flow, gouge, and damage zones on the majority of these faults indicates that they are likely old, and no evidence of recent movement was observed. Some of the shear surfaces showed two different sets of slickenlines with different sets of motion, indicating that the movement had changed. The slip planes of some of these features appeared to be along curvilinear quartz and sometimes epidote veins (plus or minus chlorite), and were sealed or very tight. This suggests that the tensile openings were exploited as slip surfaces. Conversely, the veins could have taken advantage of the fault openings and slickenlines may have been created by continued slip. Either way, the sealed nature of the fractures suggests that this tensile state has passed. Further fault analyses could elucidate the sequence of past structural deformation in the area, however it would not help determine the current state of stress. Thus we did not analyze the faults separately.

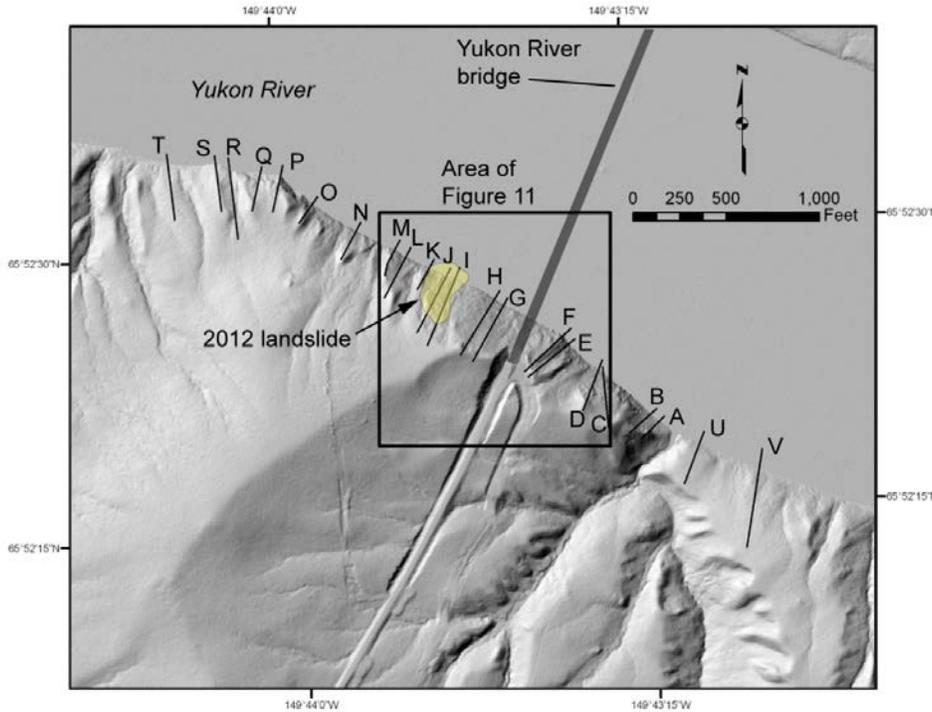


Figure 8. Site vicinity map, showing locations of topographic profiles (thin black lines labeled with letters) and Yukon River landslide (yellow polygon). Black box shows location of detailed views of the site in figure 11.

Figure 9. Topographic profiles A–H and K–V across the southern bluff of the Yukon River in the vicinity of the Yukon River bridge. Figure 8 shows the location of each profile. Profiles I and J across the Yukon River bridge landslide are shown in figure 12.

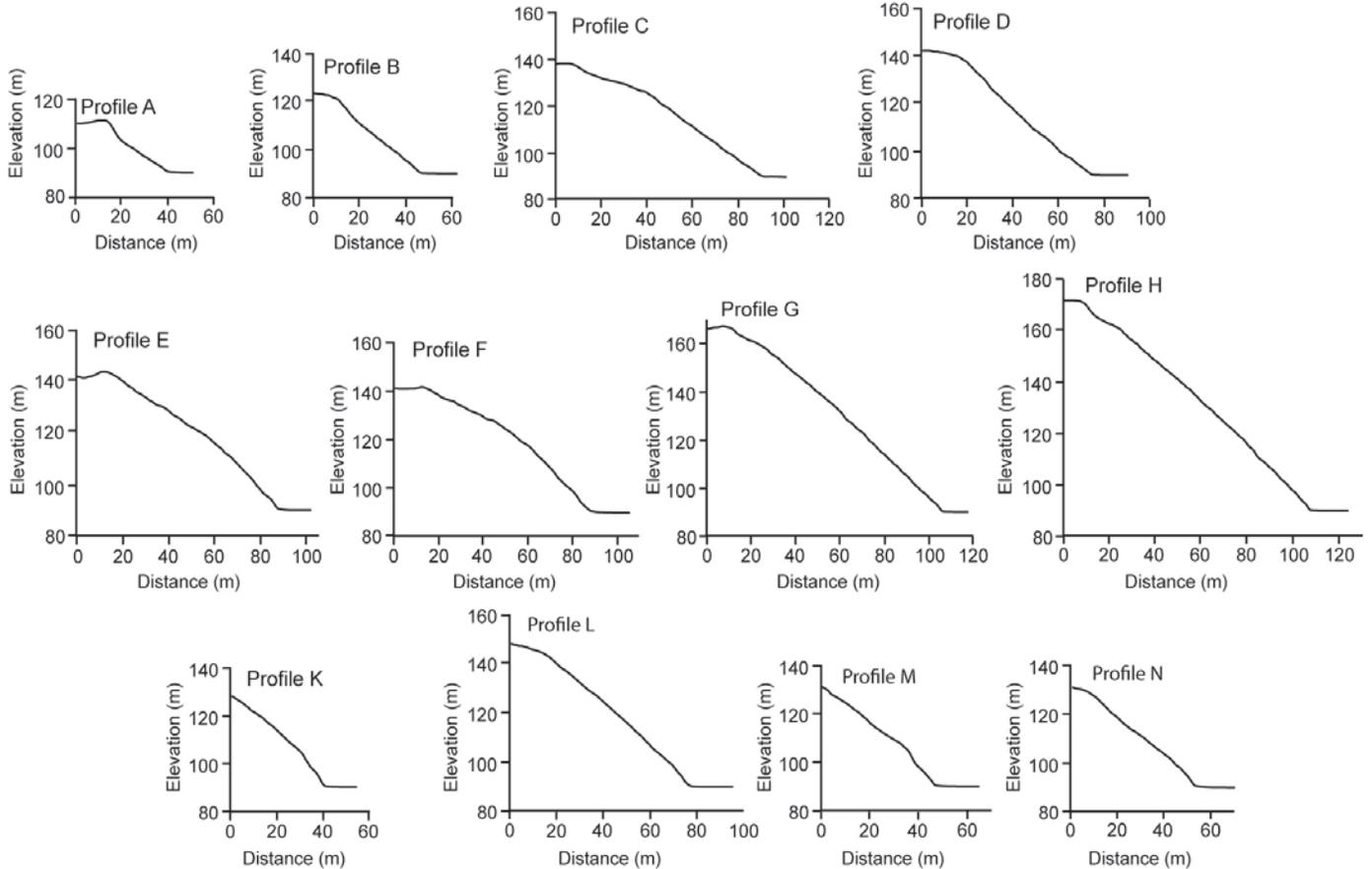


Figure 9, continued

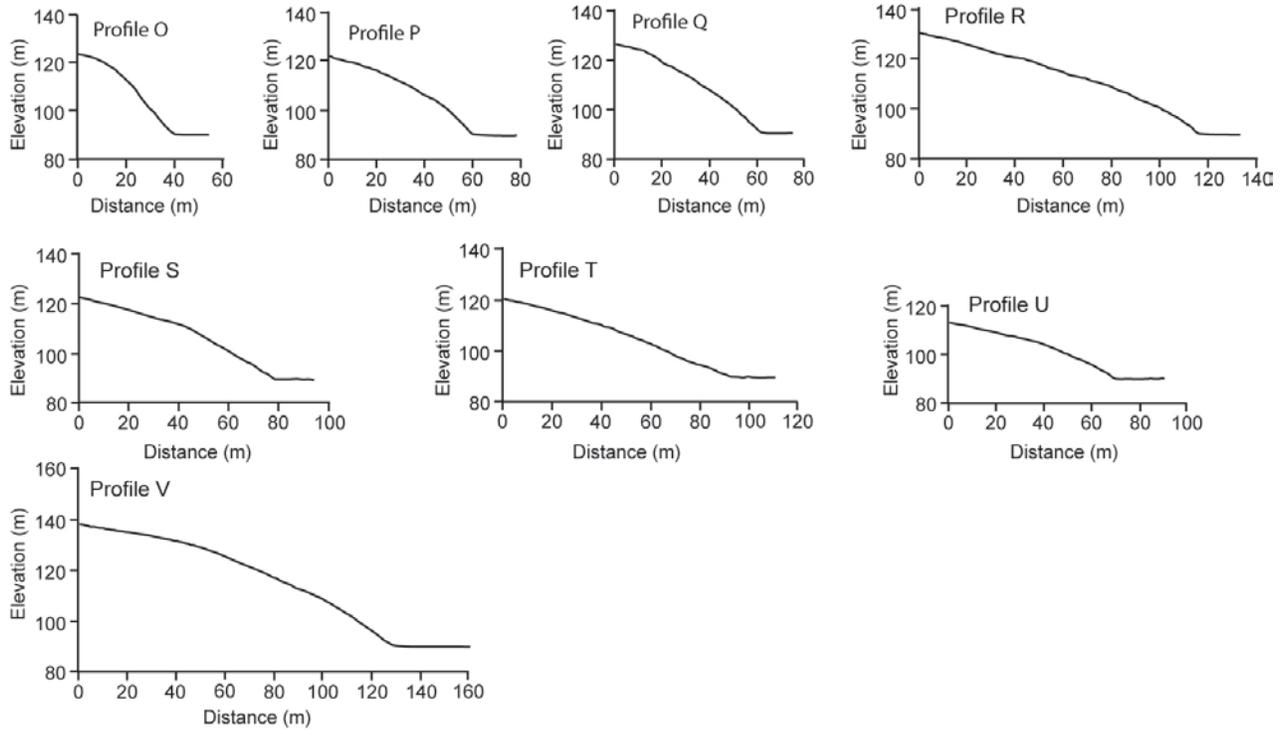
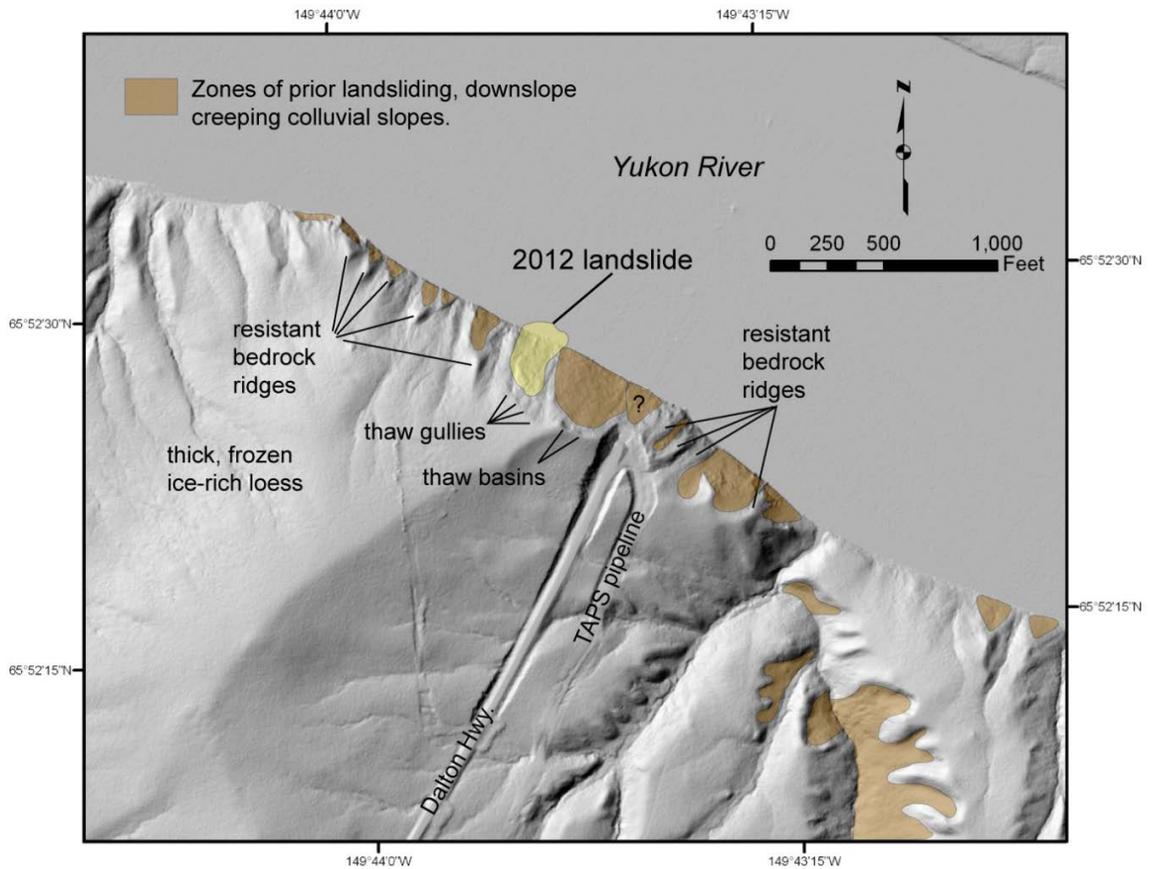


Figure 10. Geomorphic interpretation of the Yukon River bridge area, showing the 2012 landslide and zones of prior slope instability.



Results of slope and landslide geomorphology evaluation

General slope conditions and the location of individual slope profiles are shown in figure 8; profiles are in figure 9. A LiDAR interpretation of the location of prior landsliding and/or other downslope colluvial transport processes is shown on figure 10. For the areas upstream and downstream of the bridge, LiDAR imagery of the bluff shows several vegetated possible landslide slopes separated by steep, narrow bedrock ridges that are relatively stable (fig. 10). Surfaces above the crest of the bluff slopes are mantled by thick, frozen ice-rich loess and characterized by gentle slopes and common thaw gullies and basins. Geomorphic features indicative of active faulting are absent on the surface. In particular, there is no indication of recent along-strike activity of the fault identified in the foundation of bridge pier 4. In the field, helicopter surveys and boat reconnaissance were conducted along the bluff to look for evidence of prior landsliding for approximately 2,000 feet upstream and downstream of the bridge; however, no scarps or obvious debris hollows were observed.

Table 3. Characteristics of LiDAR-derived slope profiles evaluated for evidence of slope instability.

Profile designation	Evaluation scale	Comments
A	1:398	Slope planar @ 35.5°. Slow creep/gelifluction likely.
B	1:521	Slope planar @ 38.5°. Slow creep/gelifluction likely.
C	1:565	Slope planar @ 36.5°. Slow creep/gelifluction likely.
D	1:610	Slope planar @ 38°. Slow creep/gelifluction likely.
E	1:530	Steep gully between bedrock ridges contains slope debris. Possible small failure below 324 ft elevation due to river undercutting.
F	1:549	Steep nose of bedrock ridge. Lower section appears oversteepened by river erosion. Possible slope failure below ~40 ft elevation.
G	1:719	Possible slope failure below ~539 ft elevation.
H	1:698	Possible slope failure below ~543 ft elevation.
I	1:693	2012 landslide below ~507 ft elevation.
J	1:273	2012 landslide below ~477 ft elevation.
K	1:278	Steep nose of bedrock ridge. Possible slope failure at ~325 ft elevation due to undercutting by river.
L	1:522	Uniform slope of 40°. Possible slope failure below ~332 ft elevation due to undercutting by river.
M	1:347	Steep (40°) nose of bedrock ridge. Possible slope failures below ~339 and ~317 ft elevation.
N	1:348	Steep (40°) nose of bedrock ridge. Steepened to 43° below ~325 ft elevation.
O	1:348	Steep (45.5°) nose of bedrock ridge. Top of possible landslide at ~334 ft elevation.
P	1:523	Margin of possible dissected, old landslide below ~372 ft elevation in hollow west of prominent bedrock point.
Q	1:521	Axis of possible dissected, old landslide with top at ~385 ft elevation and surface slope of 28°. Slope steepens to 44° below ~338 ft elevation due to river erosion. Top of possible younger landslide at ~321 ft elevation.
R	1:521	Gully fill between bedrock ridges slopes 17°. Slope steepens to 31.5° at ~337 ft elevation in response to river erosion.
S	1:521	Loess-covered bedrock ridge. Nose slopes consistent 28° below ~361 ft elevation.
T	1:539	Loess-covered bedrock ridge slopes consistently at 20° below ~358 ft elevation.
U	---	Not evaluated.
V	---	Not evaluated.

Profiles derived from LiDAR data demonstrate that vegetated possible landslide surfaces slope between 35° and 42° and the steep, lower crests of resistant bedrock ridges slope approximately 40° to 68°. Table 3 shows the scale at which slopes were evaluated and the slope interpretation for each profile. Between rock exposures on unfailed slopes, 2–3 feet of loess overlie 4–6 feet of pebbly, silty colluvium derived from downslope transport of loess and weathered bedrock. Slopes adjacent to the 2012 landslide display surface evidence of downslope movement,

including numerous bent trees and shrubs, solifluction lobes, and scattered 10- to 20-foot-long, gaping transverse cracks. Profiles A through H and K through Q show oversteepened bases that may be a result of river erosion or past massive floods and/or ice scour (fig. 9). These profiles are located in the zone of possible previous slope movements shown on figure 10. Although some of these slopes may have catastrophically failed in mass wasting events, they may also reflect long-term downslope creep and gelifluction of weathered (residual) bedrock and loess. The absence of large colluvial hollows and debris blocks, as well as the relatively planar morphology of the slope suggests that the latter is the more dominant process of slope modification. Profiles R through V show more subdued profiles and are generally west and east of the zone of possible slope movements. In these areas, the slopes are not faceted and appear relatively stable.

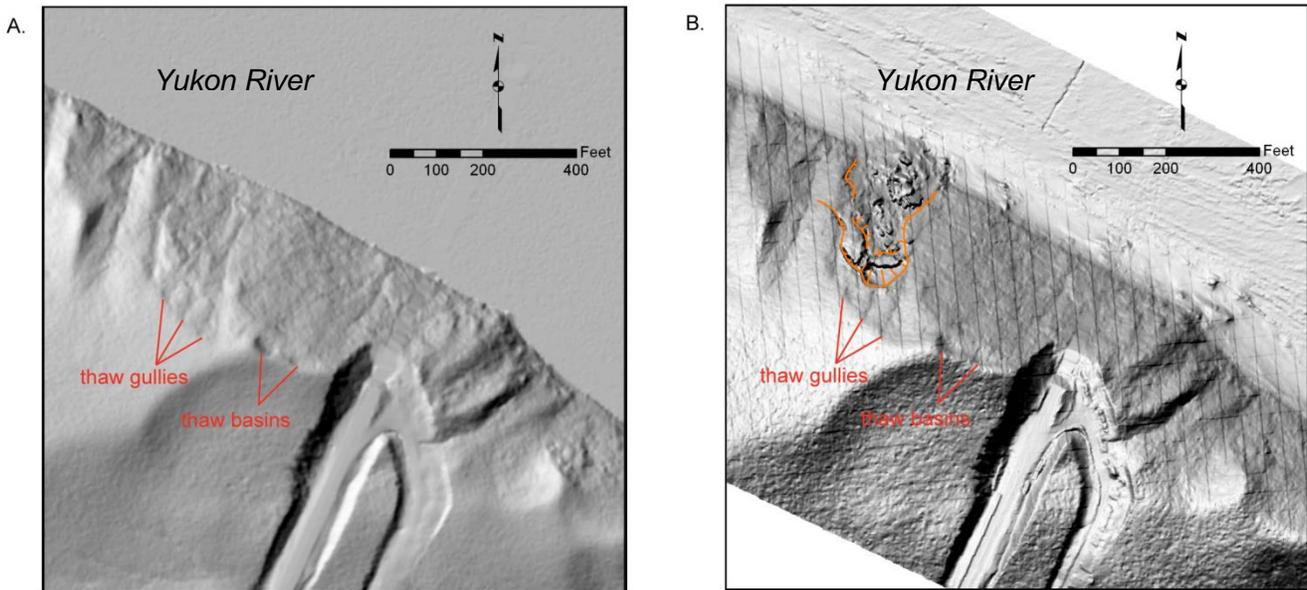


Figure 11. Pre- and post-landslide hillshade images derived from 2010 and 2013 LiDAR data. A. Pre-landslide hillshade. B. Post-landslide hillshade; edges of landslide scarps shown by orange lines.

A comparison of the pre- and post-landslide surface and profiles across the landslide are shown in figures 11 and 12, respectively. Photographs of key features on the landslide are shown in Figure 13. In the pre-landslide hillshade image, hummocky topography along the slope indicates the possible presence of previous slope instability. Thaw gullies at the crest of the slope may have contributed to previous slope movements. The 2012 landslide occurred along the downstream end of the thaw gullies. Based on the distribution of headscarps (orange lines on fig. 11B), the 2012 landslide initiated on the east and propagated to the west. Blocks of debris in the mid-slope region and a large debris cone at the base of the slope are clearly visible on the LiDAR. Based on the LiDAR data, the main slide mass, including the area of the debris cone, is approximately 90–100 feet wide and approximately 220 feet long, however the bulk of the debris was sourced from an approximately 90 × 100-foot translational slide block in frozen loess at the top of the slope (fig. 13B). In addition to the frozen loess, a large slab of highly weathered gabbro also failed. Also present are two additional blocks of rock and colluvium that did not catastrophically fail down the slope. An approximately 50 × 50-foot block on the western side of the headscarp separated from the slope across a large fracture. This block is underlain by fairly competent, fractured graywacke metasandstone and was likely made unstable after the main slide eroded the downslope side of the block, removing lateral support and causing slip to occur along fracture planes. Midway along the western margin of the slide a second block, measuring approximately 50 × 100 feet, separated approximately three feet from the adjacent in-place slope (fig. 13D). This block may be susceptible to future sliding.

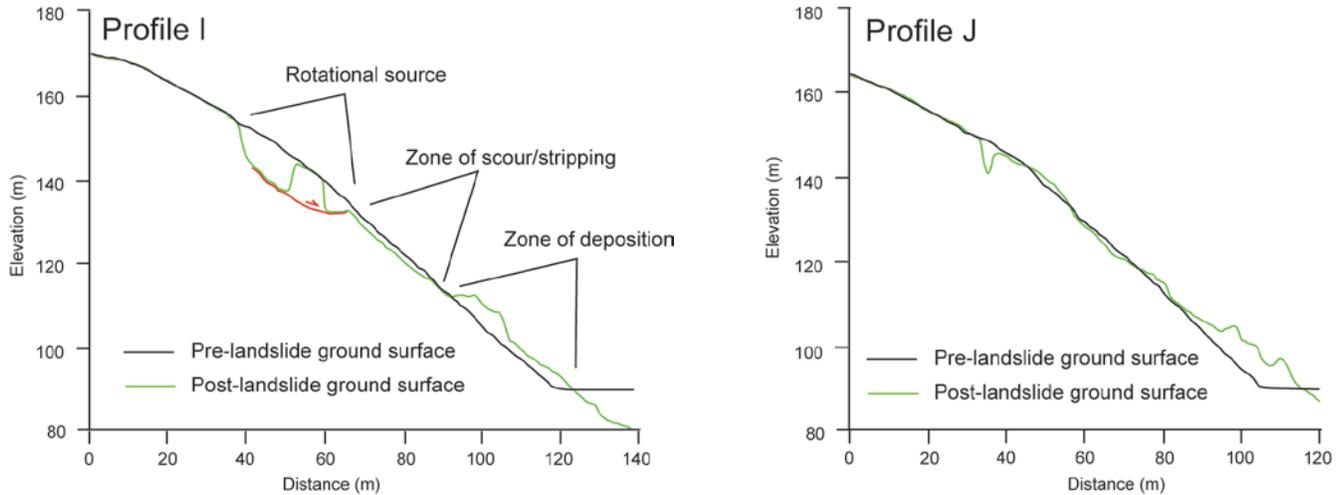


Figure 12. Topographic profiles I and J across the Yukon River bridge landslide showing the pre- and post-landslide ground surface. Pre-landslide ground surface derived from LiDAR data collected by DGGS (Hubbard and others, 2011). Post-landslide ground surface derived from LiDAR data collected by Alyeska Pipeline Service Company in April 2013. Inferred slide plane indicated in orange on Profile I.

Topographic profiles I and J were generated from the pre- and post-landslide LiDAR data across the eastern and western sides of the body of the 2012 landslide. They demonstrate that the crown of the slide is approximately 236 feet above low-water level (fig. 12). The profiles show that the landslide occurred on a slope of approximately 40° and that the post-landslide slope is around $35\text{--}37^\circ$, which was confirmed by direct measurements in the field. Profile I, down the main body of the landslide, shows three distinct zones including an upper block failure, a mid-slope zone of scour and stripping, and a lower zone of slide debris deposition (fig. 12A). Flood deposits on the lower part of the debris cone indicate that break-up floods in spring 2013 did not remove an appreciable amount of slide debris. Profile J, measured on the slope directly west of the main slide body, shows a large tension fracture and only subtle translation of the slope mass (fig. 12B).

Three 20- to 30-foot-wide former thaw gullies are present on the slope across the top of the landslide, but their rounded cross profiles indicate that they are filled with loess and retransported loess and are no longer active. Along the upper marginal scarps and headwall of the failure, the loess displays closely-spaced planar structures that generally parallel the ground surface. In Interior Alaska, such planes develop in loess during the annual freezing of the ground by the formation of very thin, clear, parallel to subparallel, segregated ice lenses (French, 2007). Parallel shear planes also develop parallel to the slope during slow downslope creep of the loess, and downslope creep likely produced the parallel shear planes in the underlying frozen colluvium. A 5-inch-wide wedge of clear ice was visible for approximately 5 feet across the freshly exposed headwall of the landslide, demonstrating that the permafrost table was approximately 2 feet deep at the end of August 2013. The ice wedge formed when precipitation or meltwater entered and froze in an open transverse crack on the perennially frozen slope. No other visible ice was observed in the permafrost there, and no evidence of meltwater from thawing permafrost was observed in or around the landslide.

Field observations indicate that the large landslide blocks of frozen loess, colluvium, and highly weathered bedrock were not rotated during downslope motion but slid on the underlying, more competent bedrock on a shallow, planar, translational slide plane. Northwest-trending transverse open cracks and their ice fillings likely had a significant impact on the locations and sizes of the block failures. Additionally, long-term creep and gelifluction on the slope may have contributed to progressively greater tension that eventually exceeded the tensile strength in the frozen blanket of loess and colluvium. Deeper slide planes may also have developed along

intersecting fracture planes in the highly weathered gabbro, which is altered to seamy clay. After initial failure, the displaced blocks collapsed and cascaded down the steep slope as a debris slide, stripping 2–3 feet of colluvium off the underlying bedrock in the mid-slope region, and depositing a large debris cone over the lower 90 feet or so of the slope. The debris cone is characterized by angular chert, gabbro, and graywacke metasandstone fragments, averaging 4–18 inches in diameter. Several large debris blocks with trees in growth position were deposited on the slope (fig. 13C). The zone of stripping and talus deposition is shown in figure 13A. Although a more detailed site investigation is necessary to more accurately define the slide plane and mechanism of failure, the field observations are consistent with a block glide transitioning downslope to a debris slide (Varnes, 1958).

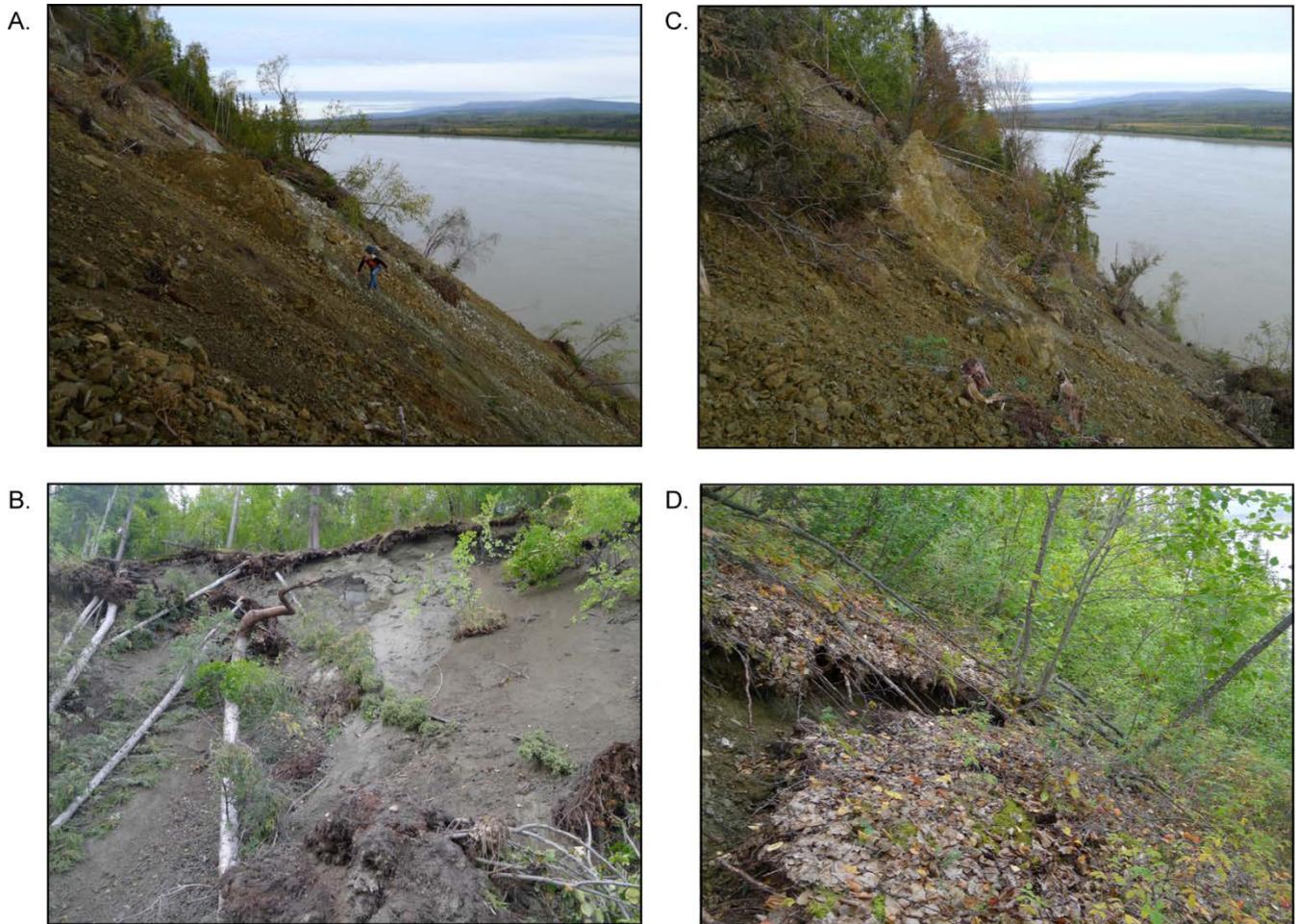


Figure 13. Photographs of the Yukon River landslide. A. Upper part of debris cone. Light gray color in upper left is exposed graywacke bedrock. B. Intact block of weathered gabbro bedrock on the surface. C. Frozen silt exposed in the headscarp. D. Separation scarp extending west of the middle part of the slide.

Conclusions and Recommendations

The 2012 landslide occurred adjacent to the Yukon River bridge, but the bridge foundation did not sustain any damage. The slide initiated in frozen loess and retransported loess, but also involved the underlying highly weathered, weak bedrock (gabbro and graywacke metasandstone). The high density of fractures, joints, shear zones, and minor faults in the rock mass likely contributed to instability, and active faulting was not a factor. Tension in the overlying loess related to transverse cracks and ice fillings and the influence of surface hydrology may also have contributed to the slope failure. The relative roles of these potential causative factors are not completely understood. Based on the surface geomorphology, we conclude that the slide is most consistent with a block glide failure transitioning downslope to a debris slide.

The bedrock and discontinuity survey determined that the bedrock along the base of the bluff is primarily composed of metabasalt (greenstone), diorite, gabbro, graywacke metasandstone, and chert with minor limestone, all of which is fresh and strong. The rocks are closely jointed, with dominant joint sets oriented WNW–ESE, NE–SW, N–S, E–W, NW–SE. These joint patterns likely extend throughout the rock mass, which includes zones that are highly altered and intensely weathered upslope. Our assessment of slopes in the vicinity of the bridge indicates that slopes are $>40^\circ$ and are mantled by fairly thin colluvium. The crest of the slope is buried by thick frozen loess. The interaction of gelifluction and ice and soil processes with the intensely fractured rock provides favorable driving forces for slope failure.

Several arcuate, open fractures are present south of the main headscarp of the 2012 landslide, indicating that additional smaller landslide blocks are poised for future downslope displacements. The slightly separated slope along the western margin of the landslide is prone to future failure, assuming continued loss of lateral support and steepening of the base of the slope by Yukon River erosion. Thaw basins at the top of the slope between the landslide and the Yukon River bridge, as well as the presence of gelifluction and active creep features, indicate the possibility of similar slope failures occurring in that area in the future. Although the potential exists for future slope failures, the lack of any significant landslide scars along the bluff upstream and downstream of the bridge indicates that large-scale failures are a rare occurrence. The 2012 landslide is the first landslide of this type and scale at least since the construction of the Yukon River bridge in 1974–75 and probably for at least 20 years previously.

Our geologic and geomorphic evaluation has determined that the fractured bedrock and steep slopes in the bridge vicinity are prone to slope failure. Given the significant landslide hazard adjacent to the Yukon River bridge and Trans-Alaska Pipeline System, and the potential impact of damage to the bridge to the state's economy, it is recommended that a monitoring and instrumentation program be initiated on the slope adjacent to the bridge to better understand the landslide risk. The instrumentation program should include the installation of piezometers, extensometers, and tiltmeters. Detailed hydrologic studies aimed at characterizing drainage patterns, and a geotechnical study focused on characterizing subsurface conditions and an estimate of "Factor of Safety" are also recommended, particularly in the critical area between the 2012 landslide and the Yukon River bridge.

Closure and Limitations

This report was prepared to convey to the public the general characteristics of the rock mass, characteristics of rock discontinuities, and the geomorphic expression of the 2012 landslide in the vicinity of the Yukon River bridge. The observations and conclusions contained in this report are based on site conditions on the dates of the field evaluations discussed herein and are the opinions of the authors. The information contained in this report should be considered preliminary and should not be used to determine areas of potential future slope instabilities. A significant amount of additional exploration and slope stability analysis are required to fully understand the landslide hazard in the area of the bridge, as well as the potential for reactivation and/or expansion of the 2012 landslide into adjacent slopes.

Acknowledgments

The authors appreciate the coordination among Steve McGroarty, Jeff Currey, Kevin Maxwell, and Garrett Speeter of (ADOT&PF) and Frank Wuttig of Alyeska Pipeline Services Company at pre-project briefing and planning meetings as well as during our field evaluation. Alyeska graciously provided helicopter support for our initial reconnaissance. Robert Joseph of Stevens Village expertly guided our boat-based river surveys. Eric Hatleberg of DNR's State Pipeline Coordinator's Office provided valuable feedback regarding our work during a field review. We thank De Anne Stevens of DGGS for an insightful review of the report.

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Appendix A

Photographs of bedrock at rock discontinuity measurement stations

A1. Station 1 joint sets, beneath the Yukon River bridge.





A2. Station 2 joint sets, 75 feet west of the Yukon River bridge.



A3. Station 3 joint sets, 150 feet west of the Yukon River bridge.





A4. Station 4a joint sets, 250 feet west of the Yukon River bridge and directly east of landslide.

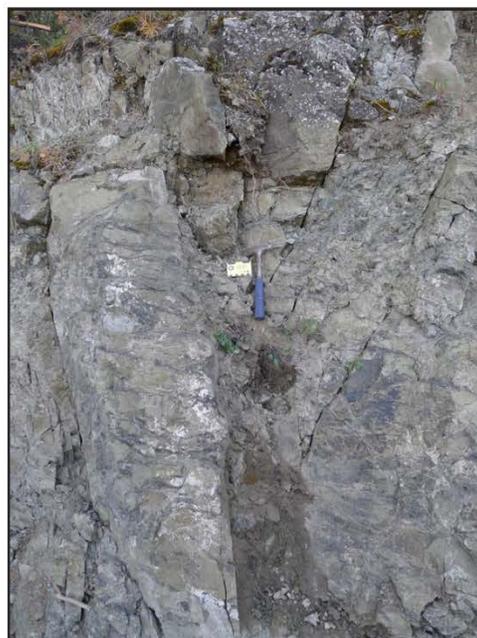
A5. Station 4b joint sets, 250 feet west of the Yukon River bridge and east of the landslide.





A6. Station 5a joint sets, 600 feet west of the Yukon River bridge and west of the landslide.





A7. Station 5b joint sets, 600 feet west of the Yukon River bridge and west of the landslide.



A8. Station 6 joint sets, 650 feet west of the Yukon River bridge and west of the landslide.



A9. Station 7 joint sets, between 770 and 800 feet west of the Yukon River bridge and west of the landslide.



A10. Station 8 joint sets, 1,000 feet west of the Yukon River bridge and west of the landslide.

A11. Station 9 joint sets, between 100 and 150 feet east of the Yukon River bridge.





A12. Station 10 joint sets, between 200 and 250 feet east of the Yukon River bridge.

A13. Station 11 joint sets, between 625 and 675 feet east of the Yukon River bridge.





A14. Station 12 joint sets, between 850 and 900 feet east of the Yukon River bridge.



A15. Station 13 joint sets, approximately 1,150 feet west of the Yukon River bridge (prominent outcrop that extends into the river).





A16. Area between Stations 10 and 11, joint sets in sheared graywacke, approximately 300 to 475 feet east of the Yukon River bridge.



Appendix B

Field evaluation sheets



State of Alaska DOT & PF
Design & Engineering Services
Statewide Materials

ROCK MASS DESCRIPTION DATA SHEET

Project Name: Yukon River bridge landslide

Field Party: D66S

Date: 8/26/13

Weather: Sunny, bluebird, windy, cold.

Project No: _____

GENERAL INFORMATION

Location: Yukon River bridge Station/Hole No. Station 1

Locality: South bank Yukon River No. of Sheets of Discontinuity Data: _____

Type: 1 Slope Length: _____ Sketch: yes

Natural Exposure: _____ Slope Height: ~16ft @ 40° Photograph: yes

3. Trench Excavation: _____ Core Size: _____

4. Adk: _____

5. Tunnel: _____

6. Drill Hole: _____

REMARKS (exposure type/age, stability condition, design issues etc.):
Y → west
abutment (South)
- high water

ROCK MATERIAL INFORMATION

Color: 2 6 8 9 6 Grain Size: 5 locally 4

1. Light
2. Dark
3. Yellowish
4. Brownish
5. Olive
6. Greenish
7. Bluish
8. White
9. Grey
10. Black

1. Pink
2. Red
3. Yellow
4. Brownish
5. Olive
6. Greenish
7. Bluish
8. White
9. Grey
10. Black

1. Very coarse - boulders (>12 in)
2. Coarse - cobbles (3-12 in)
3. Medium - gravel (0.2-3 in)
4. Fine - sand (0.003-0.2 in)
5. Very fine - silt/clay (<0.003 in)

Compressive Strength: RS PSI
4
4-7
7-15
15-35
35-70
>70

Method to Determine Compressive Strength: 2
1. Measured
2. Assessed

Rock Type: Greystone metz basalt

Qualifying terms to describe rock:
locally contains chert inclusions
8-10% veins
highly fractured, multiple joint orientations.

S1 Very soft clay
S2 Soft clay
S3 Firm clay
S4 Stiff clay
S5 Very stiff clay
S6 Hard clay
R0 Extremely weak rock
R1 Very weak rock
R2 Weak rock
R3 Medium strong rock
R4 Strong rock
R5 Very strong rock
R6 Extremely strong rock

35-150
150-725
725-3,500
3,500-7,000
7,000-15,000
15,000-36,000
>36,000

(Moldable by fingers, but retains fabric)
(Hammer craters surface, sides pushed up)
(Hammer creates smooth dent)
(Hammer creates rough pit)
(Hammer rebounds)

ROCK MASS INFORMATION

Fabric: 1 Block Size: 5 State of Weathering: 1 ICC Scored

1. Blocky
2. Tabular
3. Columnar
4. Shattered

1. Fresh
2. Slight
3. Moderate
4. High
5. Complete
6. Residual Soil

1. Very large (>216ft³ or 6ft cube)
2. Large (8-216ft³ or 2-6ft cube)
3. Medium (0.3-7ft³ or 0.67-2ft cube)
4. Small (12in³-0.3ft³ or 2.3in to 0.67ft cube)
5. Very small (<12 in³ or 2.3in cube)

Failure Mode: N.A. No. of Major Discontinuity Sets: 3-4
e.g. Toppling, Wedging

LINE SURVEYS TO DETERMINE DISCONTINUITY SPACING (OR DRILL HOLE ORIENTATION)

Line	Plunge of line / Hole	Trend of line / Hole	Length of line (m)	No. of Fractures	Spacing	Remarks / True Spacing
Line 1						
Line 2						
Line 3						

Discontinuity spacing:
1. Extremely close (<1 in)
2. Very close (1-2.5 in)
3. Close (2.5 - 8 in)
4. Moderate (8 in - 2ft)
5. Wide (2-5 ft)
6. Very wide (6-20 ft)
7. Extremely wide (>20 ft)

State of Alaska DOT & PF
Design & Engineering Services
Statewide Materials

DISCONTINUITY SURVEY DATA SHEET

Project Name: Yukon River bridge landslide
Project No.:

Date: 8/26/13
Field Party:
Weather:

Waypoint 5
N 65° 52.432'
W 149° 043.986'

GENERAL INFORMATION																	
Location:		0 ft. under bridge		Station /		Discontinuity Data Sheet No.:		/		of							
NATURE AND ORIENTATION OF DISCONTINUITY																	
Station or Depth	Type	Dip	Dip Direction	Persistence	Termination	Aperture/Width	Nature of Filling	Strength of Filling	Surface Roughness	Surface Shape	Waveiness Wavelength	Waveiness Amplitude	JRC	Water Flow	Strike	Remarks	Spacing
0 ft.	2	63°	5°	2	0	1	1	N.A.	2	2	<1ft.	<0.5in	10	NA	strike 95°		spacing close
	2	84°	180°	2	2	1	1	N.A.	2	3	N.A.	NA	10	NA	strike 70° straight		spacing close
	2	26°	180°	2	0	2	1	N.A.	3	2	6in	<0.5in	15	NA	strike 096		spacing
	2	81°	210°	3	0	2-5	1	N.A.	3	1	3ft	3in	8-10	NA	strike 300		very close to close
	2	86°	270°	2	1	1-2	1	N.A.	2	2	1-2ft	2in	8-10	NA	188 strike		mod. spacing
	2	72°	298°	2	0	5	open	N.A.	2-3	1	3ft	1in	4-6	NA	208°		close spacing
	2	69°	235°	3	0	3	open	N.A.	2	1	10ft	<1in	4-6	NA	145°		close spacing
	2	84°	326°	2	1	0	open	N.A.	2	1	0	0	2-4	NA	236°		infill with gravel close
	2	42°	130°	3	0	2	caliche	NA	2	2	24"	3in	8-10	NA	270°		spacing wide
	2	90°	var-tilt	3	0	5	caliche	NA	2	1	1-2ft	2in	12-14	NA	270°		spacing moderate
	2	88	90(E)	2	1	1	1	NA	3	2	18"	3"	14	0	014		3
	2	83	90(E)	2	2	2	1	NA	3	2	6"	0.5"	14	0	355		4
	2	87	90(E)	2	2	1	1	NA	2	1	18"	3"	18	0	254		4
	2	54	0(N)	2	2	1	1	NA	3	3	18"	1"	15	0	297		2
	2	96	45(N/E)	2	0	1	1	NA	3	2	18"	1"	13	0	065		3
	7	62	135(SE)	3	1	5	8 quartz	RS	3	2	12"	0.5"	9	0	174		3
	7	46	270(W)	1	2	7	8 quartz	RS	3	2	8"	0.7"	8	0	158		2
	5	27	270(W)	3	2	5	6 caliche	R2	1	2	8"	0.7"	8	0	101		4
	2	90	0(N)	2	2	1	1	NA	3	1	8"	1"	14	0	147		1
	2	54	270(W)	3	0	1	1	NA	3	2	8"	1"	14	0	147		1

Sand, Spangler field party
Kochler, Roger field party

WATER FLOW (Filled)
 0. Discontinuity very light and dry, water flow doesn't appear possible
 1. Discontinuity dry, no evidence of water flow
 2. Discontinuity is damp, but no free water present
 3. Discontinuity shows seepage, occasional drops of water, no continuous flow
 4. Discontinuity shows seepage, occasional drops of water, no continuous flow
 5. Continuous flow of water (Estimate lith and describe pressure i.e. low medium high)
 6. Filing materials heavily consolidated and dry, significant flow unlikely due to very low permeability
 7. Filing materials damp, no free water present
 8. Filing material wet, occasional drops of water
 9. Filing materials show signs of wetness, continuous flow of water (Estimate lith)
 10. Filing materials locally washed out; considerable water flow along outwash channels (Estimate lith and describe pressure)

COMPRESSIVE STRENGTH OF INFILLING
 PSI
 <4
 4-7
 7-15
 15-35
 35-70
 >70
 R0 Extremely weak rock
 R1 Very weak rock
 R2 Weak rock
 R3 Medium strong rock
 R4 Strong rock
 R5 Very strong rock
 R6 Extremely strong rock

NATURE OF FILLING
 1. Clean
 2. Surface staining
 3. Non-cohesive
 4. Inactive clay or clay matrix
 5. Swelling clay or clay matrix
 6. Cemented
 7. Chert, talc or gypsum
 8. Other - specify

APERTURE WIDTH
 1. Very tight (<0.04 in)
 2. Tight (0.04-0.1 in)
 3. Partly Open (0.1-0.2 in)
 4. Open (0.2-1 in)
 5. Moderately Wide (1-4 in)
 6. Wide (>4in)
 7. Very wide (4-4 in)
 8. Extremely wide (4 in - 3 ft)
 9. Cavemous (> 3 ft)

SURFACE ROUGHNESS
 1. Slickensided
 2. Smooth
 3. Rough

TERMINATION
 0. Neither end visible
 1. One end visible
 2. Both ends visible



State of Alaska DOT & PF
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Statewide Materials

ROCK MASS DESCRIPTION DATA SHEET

Project Name: Yukon River Bridge

Date: 8/26/13

Field Party: _____

Project No: _____

Weather: _____

waypoint 6
N 65° 52.438'
W 149° 43.511'

REMARKS (exposure type/age, stability condition, design issues etc.)
outcrops contain systematic and non-systematic (curved) joints

GENERAL INFORMATION

Location: Station 2 Station/Hole No. 2

Locality Type: 1 Slope Length: _____ No. of Sheets of Discontinuity Data: _____

Slope Height: _____ Sketch: _____

Core Size: _____ Photograph: yes

1. Natural Exposure
2. Construction Excavation
3. Trial Pit
4. Trench
5. Adit
6. Tunnel
7. Drill Hole

ROCK MATERIAL INFORMATION

Color: 2 6 9 Grain Size: 4-5 Compressive Strength: 85 PSI

Rock Type: meta basalt high porosity of chlorite
metagabbro-sandstone

Method to Determine Compressive Strength: 2

1. Measured
2. Assessed

Qualifying terms to describe rock:
Surface weathers to light brown reddish brown light grey green and red
loose thin bedded chert

1. Pink
2. Reddish
3. Yellow
4. Brownish
5. Olive
6. Greenish
7. Blue
8. Greyish
9. Grey
10. Black

1. Very coarse - boulders (>12 in)
2. Coarse - cobbles (3-12 in)
3. Medium - gravel (0.2-3 in)
4. Fine - sand (0.005-0.2 in)
5. Very fine - silt/clay (<0.003 in)

S1 Very soft clay
S2 Soft clay
S3 Firm clay
S4 Stiff clay
S5 Very stiff clay
S6 Hard clay
R0 Extremely weak rock
R1 Very weak rock
R2 Weak rock
R3 Medium strong rock
R4 Strong rock
R5 Very strong rock
R6 Extremely strong rock

35-150
150-725
725-3,500
3,500-7,000
7,000-15,000
15,000-36,000
>36,000

(Moldable by fingers, but retains fabric)
(Hammer craters surface, scales pushed up)
(Hammer creates smooth dent)
(Hammer creates rough pit)
(Hammer rebounds)

ROCK MASS INFORMATION

Fabric: 1 Block Size: 3 State of Weathering: 1

1. Blocky
2. Tabular
3. Columnar
4. Shattered

1. Very large (>216ft³ or 6ft cube)
2. Large (8-216ft³ or 2-6ft cube)
3. Medium (0.5-7ft³ or 0.67-2ft cube)
4. Small (12in³-0.3ft³ or 2.3in to 0.67ft cube)
5. Very small (<12 in³ or 2.3in cube)

1. Fresh
2. Slight
3. Moderate
4. High
5. Complete
6. Residual Soil

Failure Mode: 75
e.g. Toppled, Wedges

No. of Major Discontinuity Sets: 75

LINE SURVEYS TO DETERMINE DISCONTINUITY SPACING (OR DRILL HOLE ORIENTATION)

Line	Range of line / hole	Trend of line / hole	Length of line (m)	No. of Fragments	Spacing	Remarks / True Spacing
Line 1						
Line 2						
Line 3						

Discontinuity spacing:
1. Extremely close (<1 in)
2. Very close (1-2.5 in)
3. Close (2.5 - 8 in)
4. Moderate (8 in - 2 ft)
5. Wide (2-6 ft)
6. Very wide (6-20 ft)
7. Extremely wide (>20 ft)

State of Alaska DOT & PF
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Statewide Materials

DISCONTINUITY SURVEY DATA SHEET

Project Name: Yukon River bridge landslide
Project No.:

Date: 8/26/13

Field Party: Rich Koehler, Dick Reger
Weather:

GENERAL INFORMATION

Discontinuity Data Sheet No.: of

Station/Hole No.: Station 2

Location: Station 2

NATURE AND ORIENTATION OF DISCONTINUITY

Station or Depth	Type	Dip	Dip Direction	Persistence	Termination	Aperture/Width	Nature of Filling	Strength of Filling	Surface Roughness	Surface Shape	Waviness Wavelength	Waviness Amplitude	JRC	Water Flow	Strike	Remarks
S1, 2	2	88°	230°	4	1	4	1st	NA	2	1-2	2 ft.	< 0.5 in.	4-6	NA	140°	close
	2	62°	155°	2	1	< 5	1	NA	2	1	none	none	2-4	NA	65°	close
	3	37°	160°	3	1	2	8 stone	NA	3	2	1 ft.	2 in.	12-14	NA	110°	close
	2	65°	325°	3	0	2	1	NA	2	1	> 3 ft.	< 1 in.	2-4	NA	235°	close
	2	80°	318°	1	2	7	1	NA	2	1	none	none	2-4	NA	35°	close
	2	84°	165°	1	2	4-5	none	NA	2	2	6 in.	< 1/4 in.	6-8	NA	65°	close
	2	77°	114°	2	1	2	1	NA	2	1	1 ft.	< 1/4 in.	4-6	NA	204°	close
	2	86°	25°	2	1	2	1	NA	2	2	2 ft.	< 1/4 in.	2-4	NA	115°	close
	2	85°	15°	7	1	2	1	NA	2	2	2 ft.	< 1/4 in.	2-4	NA	165°	close
	5	60°	70°	3	0	3	7	R1	3	2	2 ft.	< 1/4 in.	8-10	NA	180°	close
	2, 9, 11	85°	355°	3	1	3	1	NA	2	1	none	none	2-4	NA	80°	very close
	2, 4, 7, 10	75°	140°	3	1	5	1	NA	2	1	none	none	2-4	NA	230°	very close
	2, 9, 11	66°	220°	3	1	5	1	NA	2	1	none	none	2-4	NA	310°	very close
	2	72°	237°	3	1	5	1	NA	2	1	none	none	2-4	NA	117°	close to v. close
	2	86°	235°	3	1	4-5	1	NA	2	1	none	none	2-4	NA	145°	close to v. close
	2	88°	235°	3	1	4-5	1	NA	2	1	none	none	2-4	NA	145°	close to v. close
	2	81°	340°	3	1	2-3	1	NA	2	1	3 ft.	< 0.5 in.	4-6	NA	250°	close
	2	90°	vertical	3	1	2-3	1	NA	2	1	3 ft.	< 0.5 in.	4-6	NA	213°	close

5 in. to 16 ft. wide
local slickensides plunge 45° to 225°
st. considered chlorite & calcite plunge 65° to 55°
very close joints parallel to bedding?
very close joint parallel to bedding? chert
joint parallel to bedding? terminate to east at shear zone.

WATER FLOW (Open)
1. Discontinuity very light and dry, water flow doesn't appear possible
2. Discontinuity dry, no evidence of water flow
3. Discontinuity dry, shows evidence of water flow e.g. rust staining
4. Discontinuity is damp, but no free water present
5. Discontinuity shows seepage, occasional drops of water, no continuous flow.
6. Continuous flow of water (Estimate flow and describe pressure i.e. low medium high)

WATER FLOW (Filled)
6. Filling materials heavily consolidated and dry, significant flow unlikely due to very low permeability
7. Filling materials damp, no free water present
8. Filling materials wet, occasional drops of water
9. Filling materials show signs of outwash, continuous flow of water (Estimate flow)
10. Filling materials locally washed out; considerable water flow along outwash channels (Estimate flow and describe pressure)

COMPRESSIVE STRENGTH OF INFILLING
PSI
4
4-7
7-15
15-35
35-70
>70
R1 Extremely weak rock
R2 Very weak rock
R3 Weak rock
R4 Medium strong rock
R5 Strong rock
R6 Very strong rock
R7 Extremely strong rock

NATURE OF FILLING
1. Clean
2. Subcohesive
3. Non-cohesive
4. Inactive clay or clay matrix
5. Swelling clay or clay matrix
6. Cemented
7. Chlorite, talc or gypsum
8. Other - specify

APERTURE WIDTH
1. Very tight (<0.04 in)
2. Tight (0.04-0.1 in)
3. Partly Open (0.1-0.2 in)
4. Open (0.2-1 in)
5. Moderately Wide (1-4 in)
6. Wide (>4 in)
7. Very wide (4-4 in)
8. Extremely wide (4 in - 3 ft)
9. Cavaneous (>3 ft)

PERSISTENCE
1. Very Low (<3 ft)
2. Low (3-10 ft)
3. Medium (10-30 ft)
4. High (30-60 ft)
5. Very High (>60 ft)

SURFACE ROUGHNESS
1. Stair-stepped
2. Smooth
3. Rough

SURFACE SHAPE
1. Planar
2. Undulating
3. Stepped

JRC (Joint Roughness)
0. Stair-stepped, planar
5. Stair-stepped, undulating
15. Smooth, undulating
20. Rough, stepped

ROCK MASS DESCRIPTION DATA SHEET

Project Name: Yukon Crossing

Project No: _____

Date: 8/26/2013

Field Party: Kami AElie

Weather: SUNNY 60°F windy

GPS: VOLT # 7
N 65° 52.440'
W 149° 43.547'

GENERAL INFORMATION

Location: 150' W of bridge Station/Hole No. #3

Locality Type: 1 Slope Length: 20' No. of Sheets of Discontinuity Data: 1

Slope Height: 15' Sketch: N/A

Core Size: X Photograph: _____

1. Natural Exposure
2. Construction Excavation
3. Trial Pit
4. Trench
5. Adit
6. Tunnel
7. Drill Hole

REMARKS (exposure type/age, stability condition, design issues etc.)
In fact: outcrop on river bank with boulders scattered on surface. Competent rock but jointed. Outcrops below mean highwater line - and vegetation.

ROCK MATERIAL INFORMATION

Color: 2 6 16 6 Grain Size: 4 Compressive Strength: RS Method to Determine Compressive Strength: 2 Rock Type: Dioritic

1. Light
2. Dark
3. Yellowish
4. Brownish
5. Olive
6. Greenish
7. Bluish
8. Greyish
9. Grey
10. Black

1. Very coarse - boulders (>12 in)
2. Coarse - cobbles (3-12 in)
3. Medium - gravel (0.2-3 in)
4. Fine - sand (0.003-0.2 in)
5. Very fine - silt/clay (<0.003 in)

PSI
4-4
4-7
7-15
15-35
35-70
>70
35-150
150-725
725-3,500
3,500-7,000
7,000-15,000
15,000-36,000
>36,000

S1 Very soft clay
S2 Soft clay
S3 Firm clay
S4 Stiff clay
S5 Very stiff clay
S6 Hard clay
S7 Extremely weak rock
R1 Very weak rock
R2 Weak rock
R3 Medium strong rock
R4 Strong rock
R5 Very strong rock
R6 Extremely strong rock

Qualifying terms to describe rock:
Anorthoclase, hyaloclastitic
granular
bluish red oxidation
thin rails: quartz, feldspar
black amphibole
-locally more fractured
-locally coarser grained
-quartz veins.

(Measurable by fingers, but retains fabric)
(Hammer creates surface, sides pushed up)
(Hammer creates smooth dent)
(Hammer creates rough pit)
(Hammer rebounds)

ROCK MASS INFORMATION

Fabric: 1 Block Size: 3 State of Weathering: 2 No. of Major Discontinuity Sets: 5

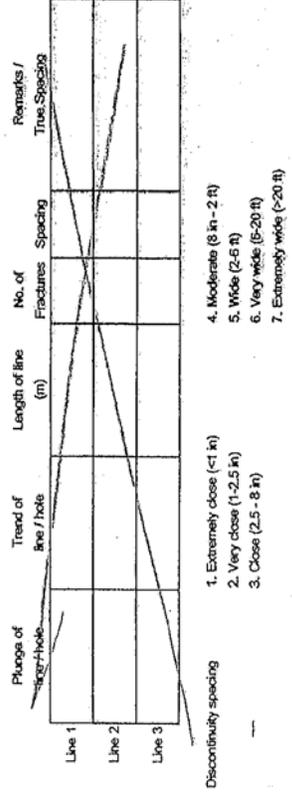
1. Blocky
2. Tabular
3. Columnar
4. Stattered

1. Very large (>216ft³ or 6ft cube)
2. Large (8-216ft³ or 2-6ft cube)
3. Medium (0.3-7ft³ or 0.67-2ft cube)
4. Small (12ft³ or 0.3ft³ or 2.3ft to 0.67ft cube)
5. Very small (<12 in³ or 2.3ft cube)

1. Fresh
2. Slight
3. Moderate
4. High
5. Complete
6. Residual Soil

Failure Mode: Jointed
e.g. Toppling, Wedges

LINE SURVEYS TO DETERMINE DISCONTINUITY SPACING (OR DRILL HOLE ORIENTATION)



DISCONTINUITY SURVEY DATA SHEET

State of Alaska DOT & PF
Design & Engineering Services
Statewide Materials

Date: 8/26/13
Field Party: Kamin & Blire
Weather: sunny ~ 60°F

Project Name: Yukon Crossing
Project No:

GENERAL INFORMATION

Location: 150' - 170'

Station/Hole No.: 3

Discontinuity Data Sheet No.: of

NATURE AND ORIENTATION OF DISCONTINUITY

Station or Depth	Type	Dip	Direction	Persistence	Termination	Aperture/Width	Nature of Filling	Strength of Filling	Surface Roughness	Surface Shape	Waviness Wavelength	Waviness Amplitude	JRC	Water Flow	Remarks
1	2	81	90 (E)	3	0	1	1	—	3	2	8"	.3"	17	0	350° 4
2	2	83	180 (S)	3	1	1	1	—	3	1	—	—	5	0	100° 4
3	2	34	270 (W)	2	1	1	1	—	3	3	—	—	14	0	180° 3
4	2	84	90 (E)	2	1	1	1	—	3	3	—	—	8	0	353° 3
5	2	81	315 (NW)	1	1	1	1	—	3	1	—	—	7	0	229° 3
6	2	78	180 (S)	2	1	1	1	—	3	1	—	—	7	0	113° 3
7	2	82	0 (N)	2	1	1	1	—	3	1	—	—	7	0	290° 4
8	2	81	180 (S)	2	1	1	1	—	3	3	—	—	7	0	108° 4
9	2	79	0 (N)	2	1	1	1	—	3	3	—	—	7	0	295° 4
10	2	84	90 (E)	2	0	1	1	—	3	2	6"	.3"	8	0	346° 3
11	2	79	90 (E)	2	0	1	1	—	3	2	6"	.3"	8	0	348° 3
12	2	86	255 (W)	2	0	1	1	—	3	2	6"	.3"	8	0	138° 3
13	2	51	270 (W)	2	0	1	1	—	3	2	6"	.3"	8	0	148° 3
14	2	78	135 (SE)	2	0	1	1	—	3	2	8"	.5"	12	0	040° 3
15	2	77	135 (SE)	2	1	1	1	—	3	2	8"	.5"	12	0	043° 3
16	2	27	270 (W)	1	1	1	1	—	3	2	8"	.5"	12	0	179° 3
17	2	38	270 (W)	1	1	1	1	—	3	1	—	—	8	0	180° 3
18	2	28	270 (W)	2	0	1	1	—	3	2	8"	.5"	10	0	177° 3
19	2	73	0 (N)	2	0	1	1	—	3	1	—	—	8	0	284° 4
20	2	74	45 (NE)	2	0	1	1	—	3	2	10"	.5"	13	0	347° 4

WATER FLOW (Open)
 0. Discontinuity very tight and dry, water flow doesn't appear possible
 1. Discontinuity dry, no evidence of water flow
 2. Discontinuity dry, shows evidence of water flow e.g. rust staining
 3. Discontinuity is damp, but no free water present
 4. Discontinuity shows seepage, occasional drops of water, no continuous flow.
 5. Continuous flow of water (Estimate l/min and describe pressure i.e. low medium high)
WATER FLOW (Filled)
 6. Filling materials heavily consolidated and dry; significant flow unlikely due to very low permeability
 7. Filling materials damp, no free water present
 8. Filling material wet, occasional drops of water
 9. Filling materials show signs of outwash, continuous flow of water (Estimate l/min)
 10. Filling materials locally washed out; considerable water flow along outwash channels (Estimate l/min and describe pressure)

COMPRESSION STRENGTH OF INFILLING
 PSI
 <4
 4-7
 7-15
 15-35
 35-70
 >70
 S1 Very soft clay
 S2 Soft clay
 S3 Firm clay
 S4 Stiff clay
 S5 Very stiff clay
 S6 Hard clay
 R0 Extremely weak rock
 R1 Very weak rock
 R2 Weak rock
 R3 Medium strong rock
 R4 Strong rock
 R5 Very strong rock
 R6 Extremely strong rock

NATURE OF FILLING
 1. Clean
 2. Surface staining
 3. Non-cohesive
 4. Irregular clay or clay matrix
 5. Swelling clay or clay matrix
 6. Cemented
 7. Chlorite, talc or gypsum
 8. Other - specify

APERTURE WIDTH
 1. Very tight (<.004 in)
 2. Tight (.004-.01 in)
 3. Partly Open (.01-.02 in)
 4. Open (.02-.1 in)
 5. Moderately Wide (.1-1 in)
 6. Wide (>1in)
 7. Very wide (1-4 in)
 8. Extremely wide (4 in - 3 ft)
 9. Cavernous (> 3ft)

PERSISTENCE
 1. Very Low (<3 ft)
 2. Low (3-10 ft)
 3. Medium (10-30 ft)
 4. High (30-60 ft)
 5. Very High (>60 ft)

SURFACE SHAPE
 1. Planar
 2. Undulating
 3. Stepped

SURFACE ROUGHNESS
 1. Slickensided
 2. Smooth
 3. Rough

JRC (Joint Roughness)
 0 Slickensided, planar
 5
 10 Smooth, undulating
 15
 20 Rough, stepped

TERMINATION
 0. Neither end visible
 1. One end visible
 2. Both ends visible

Sheet 1 of 2

Date: 8/27/2013
 Field Party: Karri + Ellie

ROCK MASS DESCRIPTION DATA SHEET
 Project Name: Yukon River bridge landslide

State of Alaska DOT & PF
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Weather: _____

Project No: _____

Station/Hole No. #4a

Locality 250' West

Location 250' West

No. of Sheets of Discontinuity Data 2

Slope Length _____

Slope Height _____

Core Size _____

Sketch _____

Photograph _____

REMARKS (exposure type/age, stability condition, design issues etc.)
outcrop extends 25' to the E of the 250' Station and 15' to the W of the Station
Outcrop examined is rock type that makes up lower 3/4 of slope.

ROCK MATERIAL INFORMATION

Color 2 2 9

Grain Size 4

Compressive Strength R4 PSI

Method to Determine Compressive Strength 2

Rock Type Dioritic

Qualifying terms to describe rock:
 - Fracture C - hypocrateritic, granitic, quartzite, felspar.
 - Quartz veins prevalent
 - Carved to sharp binary offset veins.
 - Outcrop very fractured.
 - Many slickensides.

1. Very soft clay
 2. Soft clay
 3. Firm clay
 4. Stiff clay
 5. Very stiff clay
 6. Hard clay
 7. Extremely weak rock
 8. Very weak rock
 9. Weak rock
 10. Medium strong rock
 11. Strong rock
 12. Very strong rock
 13. Extremely strong rock

ROCK MASS INFORMATION

Fabric 1

Block Size 3

State of Weathering 3

No. of Major Discontinuity Sets 5

Failure Mode Jointed
 e.g. Toppling, Wedges

LINE SURVEYS TO DETERMINE DISCONTINUITY SPACING (OR DRILL HOLE ORIENTATION)

Line	Plunge of line / hole	Trend of line / hole	Length of line (m)	No. of Fractures	Spacing	Remarks / True Spacing
Line 1						
Line 2						
Line 3						

Discontinuity spacing

- Extremely close (<1 ft)
- Very close (1-2.5 ft)
- Close (2.5 - 8 ft)
- Moderate (8 in - 2 ft)
- Wide (2-6 ft)
- Very wide (6-20 ft)
- Extremely wide (>20 ft)

Sample taken # 13yc04a

State of Alaska DOT & PF Design & Engineering Services Statewide Materials

DISCONTINUITY SURVEY DATA SHEET

Date: 8/27/2013 Field Party: Kari Sicard + Ellie Spangler Weather: Soish, sunny, high cloud.

GENERAL INFORMATION

Location: 250 W08 of bridge Station/Hole No.: 44a

Discontinuity Data Sheet No.: 1 of 2

NATURE AND ORIENTATION OF DISCONTINUITY

Table with columns: Station or Depth, Type, Dip, Direction, Persistence, Termination, Aperture/Width, Nature of Filling, Strength of Filling, Surface Roughness, Surface Shape, Waveiness, Waviness, Amplitude, JRC, Water Flow, Remarks. Includes handwritten notes like 'Parallel to gr veins' and 'Bluish oxide staining'.

Classification and descriptive text sections including: APERTURE WIDTH, PERSISTENCE, NATURE OF FILLING, COMPRESSIVE STRENGTH OF INFILLING, WATER FLOW (Open), and WATER FLOW (Filled). Includes various codes and scales for classification.

Sheet 2 of 2

WP # 8
N 05° 52.442'
W 119° 43.545'



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ROCK MASS DESCRIPTION DATA SHEET

Date: 8/27/2013

Project Name: Yukon Crossing

Field Party: Karri Sicard + Ellie Spangler

Project No:

Weather: Sunny and 50° - thin high clouds.

GENERAL INFORMATION

Location: 250' west of bridge
Station/Hole No.: #4b
Locality Type: 1
Slope Length: No. of Sheets of Discontinuity Data: 2
Slope Height: Sketch:
Core Size: Photograph:
1. Natural Exposure
2. Construction Excavation
3. Trial Pit
4. Trench
5. ADK
6. Tunnel
7. Drill Hole

REMARKS (exposure type/age, stability condition, design issues etc.)
Outcrop extends 25' to the E of the 250' station and ~15' feet west of the 250' station.
Outcrop examined is rock type that makes up upper 1/4 of slope.

ROCK MATERIAL INFORMATION

Color: 1 7 9
Grain Size: 5
Compressive Strength: R5
Method to Determine Compressive Strength: 2
Rock Type: Gneiss
Qualifying terms to describe rock:
• Grain size is very fine to fine.
• Layers of alternating granitic and color.
• Locally deformed bedding.
• Rock has been heated, some water damage.
• Siliceous, some Feldspar, quartz, plagioclase.
• Extensively veined, identified by quartz.
• Few oxidized surfaces, otherwise fresh.
• Mainly fractured.

ES:
S1 Very soft clay
S2 Soft clay
S3 Firm clay
S4 Stiff clay
S5 Very stiff clay
S6 Hard clay
S7 Extremely weak rock
R1 Very weak rock
R2 Weak rock
R3 Medium strong rock
R4 Strong rock
R5 Very strong rock
R6 Extremely strong rock

ROCK MASS INFORMATION

Fabric: 1+04
Block Size: 4
State of Weathering: 2
No. of Major Discontinuity Sets: 4
Failure Mode: Jointed
e.g. Topping, Wedges

LINE SURVEYS TO DETERMINE DISCONTINUITY SPACING (OR DRILL HOLE ORIENTATION)

Line #	Plunge of line / hole	Trend of line / hole	Length of line (m)	No. of Fractures	Spacing	Remarks / True Spacing
Line 1						
Line 2						
Line 3						

Discontinuity spacing:
1. Extremely close (<1 in)
2. Very close (1-2.5 in)
3. Close (2.5 - 8 in)
4. Moderate (8 in - 2 ft)
5. Wide (2-6 ft)
6. Very wide (6-20 ft)
7. Extremely wide (>20 ft)

Sample taken # 13yc04b

Date: 8/27/2013
Field Party: Kari Sicaud / Ellic Spongler
Weather:

DISCONTINUITY SURVEY DATA SHEET
Project Name: Yukon Crossing
Project No.:

State of Alaska DOT & PF
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Statewide Materials



Station/Note No.: #416 Discontinuity Data Sheet No.: 2 of 2

Location: 230' W28° E of 5r-4

NATURE AND ORIENTATION OF DISCONTINUITY

Station or Depth	Type	Dip	Dip Direction	Persistence	Termination	Aperture/Width	Nature of Filling	Strength of Filling	Surface Roughness	Surface Shape	Waviness Wavelength	Waviness Amplitude	JRC	Water Flow	Remarks	SPILLAGE
1	2	74	0 (N)	1	1	1	2	1	3	3	12"	1.5"	3	0	256	3
2	2	76	0 (N)	2	1	1	1	1	2	3	12"	1.5"	3	0	232	2
3	2	79	0 (N)	2	0	1	1	1	2	3	12"	1.5"	3	0	232	2
4	2	75	0 (N)	2	0	1	1	1	2	3	12"	1.5"	3	0	255	3
5	2	68	0 (N)	1	1	1	1	1	2	3	12"	1.5"	3	0	240	3
6	2	75	0 (N)	2	0	1	1	1	2	3	12"	1.5"	3	0	240	3
7	2	75	0 (N)	2	0	1	1	1	2	3	12"	1.5"	3	0	240	3
8	2	62	0 (N)	2	0	1	1	1	2	3	12"	1.5"	3	0	240	3
9	2	72	150 (S)	2	0	1	1	1	2	3	12"	1.5"	3	0	240	3
10	2	69	160 (S)	2	0	1	1	1	2	3	12"	1.5"	3	0	240	3
11	2	80	160 (S)	2	0	1	1	1	2	3	12"	1.5"	3	0	240	3
12	2	80	160 (S)	2	0	1	1	1	2	3	12"	1.5"	3	0	240	3
13	2	77	160 (S)	2	0	1	1	1	2	3	12"	1.5"	3	0	240	3
14	2	77	160 (S)	2	0	1	1	1	2	3	12"	1.5"	3	0	240	3
15	2	69	160 (S)	2	0	1	1	1	2	3	12"	1.5"	3	0	240	3
16	2	69	160 (S)	2	0	1	1	1	2	3	12"	1.5"	3	0	240	3
17	5	69	285 (SW)	2	0	1	1	1	2	3	12"	1.5"	3	0	240	3
18	5	88	205 (SW)	2	0	1	1	1	2	3	12"	1.5"	3	0	240	3
19	2	87	250 (W)	2	1	1	1	1	2	3	12"	1.5"	3	0	240	3
20	5	45	155 (SE)	2	0	1	1	1	2	3	12"	1.5"	3	0	240	3

APERTURE WIDTH: 1. Very tight (<0.04 in), 2. Tight (0.04-0.1 in), 3. Partly Open (0.1-0.2 in), 4. Open (0.2-1 in), 5. Moderately Wide (1-4 in), 6. Wide (4-8 in), 7. Very wide (4-4 in), 8. Extremely wide (4 in - 3 ft), 9. Cavernous (> 3 ft)

PERSISTENCE: 1. Very Low (<5 ft), 2. Low (5-10 ft), 3. Medium (10-30 ft), 4. High (30-60 ft), 5. Very High (>60 ft)

TERMINATION: 0. Neither end visible, 1. One end visible, 2. Both ends visible

SURFACE ROUGHNESS: 1. Stratifoliated, 2. Smooth, 3. Rough

SURFACE SHAPE: 1. Planar, 2. Irregular, 3. Stepped

JRC (Local Roughness): 0. Stratifoliated, Planar, 5. Irregular, 10. Smooth, uplapping, 15. Rough, stepped

COMPRESSIVE STRENGTH OF INFILLING: S1 Very soft clay, S2 Soft clay, S3 Firm clay, S4 Stiff clay, S5 Very stiff clay, S6 Hard clay, R0 Extremely weak rock, R1 Very weak rock, R2 Weak rock, R3 Medium strong rock, R4 Strong rock, R5 Very strong rock, R6 Extremely strong rock

PSI: 35-150, 150-725, 725-5,000, 3,500-7,000, 7,000-15,000, 15,000-35,000, >35,000

WATER FLOW (Open): 0. Discontinuity very tight and dry, water flow doesn't appear possible, 1. Discontinuity dry, no evidence of water flow, 2. Discontinuity shows evidence of water flow e.g. rust staining, 3. Discontinuity is damp, but no free water present, 4. Discontinuity shows seepage, occasional drops of water, no continuous flow, 5. Continuous flow of water (Estimate flow and describe pressure in low medium high), WATER FLOW (Fined): 6. Filling materials heavily consolidated and dry; significant flow unlikely due to very low permeability, 7. Filling materials damp, no free water present, 8. Filling material wet, occasional drops of water, 9. Filling materials show signs of outwash, continuous flow of water (Estimate flow), 10. Filling materials locally washed out; considerable water flow along outwash channels (Estimate flow and describe pressure)

REMARKS: These joints are offset by the above group. Individual thin joints are more recent. High angle movement. These joints were made up by the contractor in the horizontal plane. Average sense of shear acute to 81, 82 steps. For betterment 1 step - 81



State of Alaska DOT & PF
Design & Engineering Services
Statewide Materials

ROCK MASS DESCRIPTION DATA SHEET

Date: 8/27/13
Field Party: Rich Koehler, Elise Spangler, Dirk Reger, Keri Siccard
Weather: high clouds, ±50° no wind

Project Name: Yukon River bridge
Project No:

GENERAL INFORMATION

Location: Station 5A 600ft. SW of bridge
 Locality Type: 1
 Slope Length:
 Slope Height:
 Core Size:
 Natural Exposure:
 Construction Excavation:
 Trial Pit:
 Trench:
 Adit:
 Tunnel:
 Drill Hole:
 No. of Sheets of Discontinuity Data: SA
 Sketch: NO
 Photograph: YES

Remarks (exposure type/age, stability condition, design issues etc.):
 Station 5B --- high water line
 Station 5A gray waste

ROCK MATERIAL INFORMATION

Color: 2 6 9
 Grain Size: 5
 Compressive Strength: AS
 Method to Determine Compressive Strength: 2
 Rock Type: meta greywacke
 Qualifying terms to describe rock: weathers to purplish grey

1. Measured
 2. Assessed

ESL
 S1 Very soft clay 4-4
 S2 Soft clay 4-7
 S3 Firm clay 7-15
 S4 Stiff clay 15-35
 S5 Very stiff clay 35-70
 S6 Hard clay >70
 R0 Extremely weak rock 35-150
 R1 Very weak rock 150-725
 R2 Weak rock 725-3,500
 R3 Medium strong rock 3,500-7,000
 R4 Strong rock 7,000-15,000
 R5 Very strong rock 15,000-36,000
 R6 Extremely strong rock >36,000

(Moldable by fingers, but retains fabric)
 (Hammer creates surface, sides pushed up)
 (Hammer creates smooth face)
 (Hammer creates rough pit)
 (Hammer rebounds)

ROCK MASS INFORMATION

Fabric: 1
 Block Size: 3
 State of Weathering: 1
 No. of Major Discontinuity Sets: 3
 Failure Mode:
 e.g. Topping, Wedges

LINE SURVEYS TO DETERMINE DISCONTINUITY SPACING (OR DRILL HOLE ORIENTATION)

Line	Plunge of line / hole	Trend of line / hole	Length of line (m)	No. of Fractures / Spacing	Remarks / True Spacing
Line 1					
Line 2					
Line 3					

Discontinuity spacing:
 1. Extremely close (<1 in)
 2. Very close (1-2.5 in)
 3. Close (2.5 - 8 in)
 4. Moderate (8 in - 2 ft)
 5. Wide (2-6 ft)
 6. Very wide (6-20 ft)
 7. Extremely wide (>20 ft)

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DISCONTINUITY SURVEY DATA SHEET

Date: 8/27/13
Field Party: Rich Koehler / Dick Regar
Weather:

Project Name: Yukon River Bridge Landslide
Project No.:

Location: Skatka, SA
Station/Hole No.: SA
Discontinuity Data Sheet No.: of

NATURE AND ORIENTATION OF DISCONTINUITY

Station or Depth	Type	Dip	Direction	Persistence	Termination	Aperture/Width	Nature of Filling	Strength of Filling	Surface Roughness	Surface Shape	Waviness Wavelength	Waviness Amplitude	JRC	Water Flow	Strike	Remarks
SA	2	55°	85°	3	0	2	1 some g	RO	2	1	none	none	4-6	NA	175°	Moderate discontinuous calcarenaceous clay
	2	63°	65°	3	0	2	1 some g	RO	2	1	none	none	4-6	NA	155°	Moderate
	2	67°	60°	3	0	2	1	PA	2	1	none	none	4-6	NA	150°	Moderate
	2	72°	10°	3	0	1	1	NA	2	1	none	none	2-4	NA	100°	very close
	2	78°	15°	3	0	1	1	NA	2	1	none	none	2-4	NA	105°	very close
	2	76°	16°	3	0	1	1	NA	2	1	none	none	2-4	NA	106°	very close
	2	62°	330°	3	0	2	1	NA	2-3	2	1.5 ft	1 in.	8-10	NA	60°	Moderate
	2	78°	150°	3	0	2	1	NA	2-3	2	1.5 ft	1 in.	8-10	NA	62°	Moderate
	2	90°	ver-tical	3	0	2	1	NA	2-3	2	1.5 ft	1 in.	8-10	NA	60°	Moderate

TYPE	PERSISTENCE	APERTURE/WIDTH	NATURE OF FILLING	COMPRESSIVE STRENGTH OF INFILLING	WATER FLOW (Open)
0. Fault Zone	1. Very Low (<3 ft)	1. Very tight (<.004 in)	1. Clean	PSI	0. Discontinuity very light and dry, water flow doesn't appear possible
1. Fault	2. Low (3-10 ft)	2. Tight (.004-.01 in)	2. Surface staining	<4	1. Discontinuity dry, no evidence of water flow
2. Joint	3. Medium (10-30 ft)	3. Partly Open (.01-.02 in)	3. Non-cohesive	4-7	2. Discontinuity dry, shows evidence of water flow e.g. rust staining
3. Cleavage	4. High (30-60 ft)	4. Open (.02-.1 in)	4. Inactive clay or clay matrix	7-15	3. Discontinuity is damp, but no free water present
4. Schistosity	5. Very High (>60 ft)	5. Moderately Wide (.1-.4 in)	5. Swelling clay or clay matrix	15-35	4. Discontinuity shows seepage, occasional drops of water, no continuous flow.
5. Shear	6. Very wide (.4 - 4 in)	6. Wide (>.4 in)	6. Cemented	35-70	5. Continuous flow of water (Estimate lith and describe pressure i.e. low medium high)
6. Flare	7. Extremely wide (4 in - 3 ft)	7. Very wide (4 - 4 in)	7. Chlorite, talc or gypsum	>70	6. Filling materials heavily consolidated and dry; significant flow unlikely due to very low permeability
7. Tension Crack	8. Cavernous (> 3 ft)	8. Cavernous (> 3 ft)	8. Other - specify	35-150	7. Filling materials damp, no free water present
8. Fracture			9. Calcarenous	725-3,500	8. Filling material wet, occasional drops of water
9. Bedding				3,000-7,000	9. Filling materials show signs of cohesiveness, continuous flow of water (Estimate lith and describe pressure)
				7,000-15,000	10. Filling materials locally washed out; considerable water flow along outwash channels (Estimate lith and describe pressure)
				15,000-36,000	
				>36,000	

ROCK MASS DESCRIPTION DATA SHEET

Project Name: Yukon River Bridge

Date: 8/27/13

Field Party: DGS

Project No:

Weather:

GENERAL INFORMATION

Location: station SB
 Locality: 600 ft. west of bridge
 Type: 1
 Slope Length: 600 ft.
 Slope Height: 600 ft.
 Core Size: 6
 No. of Sheets of Discontinuity Data: SB
 Sketch: yes
 Photograph: yes

REMARKS (exposure type/age, stability condition, design issues etc.)

Station SB light green graywacke
Station SA dark graywacke
high water mark
shear zones to broken up for accurate orientation generally N-S. multiple other shear fabrics in rock

ROCK MATERIAL INFORMATION

Color: 1 X 6
 Grain Size: 4
 Compressive Strength: PSI
 Method to Determine Compressive Strength: measured
 Rock Type: meta graywacke

Qualifying terms to describe rock:
light green graywacke with wispy lenses of black shale discontinuous shear zones characterized by breccia range from 6 in to 3ft.

1. Measured
 2. Assessed

(Moldable by fingers, but retains fabric)
 (Hammer creates rough surface, shales pushed up)
 (Hammer creates smooth dent)
 (Hammer creates rough pit)
 (Hammer rebounds)

ROCK MASS INFORMATION

Fabric: 3
 Block Size: 4 in shear zones
 State of Weathering: 2
 No. of Major Discontinuity Sets: 3
 Failure Mode: wedges
 e.g. Toppling, Wedging

1. Fresh
 2. Slight
 3. Moderate
 4. High
 5. Complete
 6. Residual Soil

1. Blocky
 2. Tabular
 3. Columnar
 4. Shattered

1. Very large (>216ft³ or 6ft cube)
 2. Large (8-216ft³ or 2-6ft cube)
 3. Medium (0.3-7ft³ or 0.67-2ft cube)
 4. Small (12in-10.3ft³ or 2.3in to 0.67ft cube)
 5. Very small (<12 in³ or 2.3in cube)

1. Extremely close (<1 in)
 2. Very close (1-2.5 in)
 3. Close (2.5-8 in)
 4. Moderate (8 in - 2 ft)
 5. Wide (2-6 ft)
 6. Very wide (6-20 ft)
 7. Extremely wide (>20 ft)

LINE SURVEYS TO DETERMINE DISCONTINUITY SPACING (OR DRILL HOLE ORIENTATION)

Line #	Plunge of line / hole	Trend of line / hole	Length of line (m)	No. of Fractures / Spacing	Remarks / True Spacing
Line 1					
Line 2					
Line 3					

Discontinuity spacing

ROCK MASS DESCRIPTION DATA SHEET

Date: 8/27/13
Field Party: DGS
Weather: high clouds, cold, +46°

Project Name: Yukon River bridge
Project No:

GENERAL INFORMATION

Location: Station 6
waypoint 10 N 65°S 2,498'
W 149° 43,700'

Station/Hole No. 6

Locality Type: 1
650' west of bridge to 700'

No. of Sheets of Discontinuity Data: []
Sketch: []
Photograph: []

Slope Length: []
Slope Height: []
Core Size: []

1. Natural Exposure
2. Construction Excavation
3. Trial Pit
4. Trench
5. Adf
6. Tunnel
7. Drill Hole

REMARKS (exposure type/age, stability condition, design issues etc.)

ROCK MATERIAL INFORMATION brownish below high water mark

Color: 1 4 6

Grain Size: 4

Compressive Strength: BS

Method to Determine Compressive Strength: 2

Rock Type: meta gabbro

Qualifying terms to describe rock:
fine grained meta gabbro
quartz veining up to lin. thick
mafic phenocrysts
chlorite along margins of joints
calcite veins

1. Measured
2. Assessed

(Modifiable by fingers, but retains fabric)
(Hammer creates surface, sides pushed up)
(Hammer creates smooth dent)
(Hammer creates rough pit)
(Hammer rebounds)

FSI
 <4
 4-7
 7-15
 15-35
 35-70
 >70
 S1 Very soft clay
 S2 Soft clay
 S3 Firm clay
 S4 Stiff clay
 S5 Very stiff clay
 S6 Hard clay
 R0 Extremely weak rock
 R1 Very weak rock
 R2 Weak rock
 R3 Medium strong rock
 R4 Strong rock
 R5 Very strong rock
 R6 Extremely strong rock

ROCK MASS INFORMATION

Fabric: 1

Block Size: 3

State of Weathering: 1

No. of Major Discontinuity Sets: 4+

Failure Mode: []
e.g. Topping, Wedges

1. Blocky
2. Tabular
3. Columnar
4. Shattered

1. Fresh
2. Slight
3. Moderate
4. High
5. Complete
6. Residual Soil

1. Very large (>216ft³ or 6ft cube)
2. Large (8-216ft³ or 2-6ft cube)
3. Medium (0.3-7ft³ or 0.67-2ft cube)
4. Small (1/8ft³-0.3ft³ or 2.3in to 0.67ft cube)
5. Very small (<1/8ft³ or 2.3in cube)

LINE SURVEYS TO DETERMINE DISCONTINUITY SPACING (OR DRILL HOLE ORIENTATION)

Line	Plunge of line / hole	Trend of line / hole	Length of line (m)	No. of Fractures / True Spacing	Remarks / True Spacing
Line 1					
Line 2					
Line 3					

Discontinuity Spacing

- Extremely close (<1 in)
- Very close (1-2.5 in)
- Close (2.5 - 8 ft)
- Moderate (8 in - 2 ft)
- Wide (2-6 ft)
- Very wide (6-20 ft)
- Extremely wide (>20 ft)

DISCONTINUITY SURVEY DATA SHEET

State of Alaska DOT & PF
Design & Engineering Services
Statewide Materials

Date: 8/27/13
Field Party: DGS
Weather:

Project Name: Waka River bridge landside
Project No:

Station/Hole No.: 6
Location: Station 6 650 ft. west of bridge

Discontinuity Data Sheet No.: 1 of 1

NATURE AND ORIENTATION OF DISCONTINUITY

Station or Depth	Type	Dip	Direction	Persistence	Termination	Aperture/Width	Nature of Filling	Strength of Filling	Surface Roughness	Surface Shape	Waviness Wavelength	Waviness Amplitude	JRC	Water Flow	Strike	Remarks
6	2	75°	355°	3	0	3	1	NA	2-3	1	None	None	6-8	0	85°	close
	2	63°	0°	3	0	3	1	NA	2-3	1	None	None	6-8	0	90°	close
	2	54°	10°	3	0	3	1	NA	2-3	1	None	None	6-8	0	80°	close
	2	80°	70°	3	0	3	1	NA	3	2	2 ft	<0.5 in	8-10	0	160°	close
	2	90°	vertical	3	0	3	1	NA	3	2	2 ft	<0.5 in	8-10	0	175°	close
	2	74°	85°	3	0	3	1	NA	2-3	2	2 ft	<0.5 in	8-10	0	50°	close
	2	58°	140°	2	1	2	1	NA	2-3	2	2 ft	lin	8-10	0	40°	close
	2	68°	130°	2	1	2	1	NA	2-3	2	2 ft	lin	8-10	0	44°	close
	2	46°	134°	2	1	2	1	NA	1	2	2 ft	<0.5 in	6-8	0	50°	close
	2	40°	320°	1	1	5	2.7 ft	R0	1	2	2 ft	<0.5 in	6-8	0	77°	close
	2	35°	348°	1	1	5	2.7 ft	R0	1	2	2 ft	<0.5 in	6-8	0	77°	close
	2	49°	305°	1	1	3	2.9 ft	R0	2	2	1 ft	<0.5 in	6-8	0	35°	close
	2	74°	319°	1	1	3	2.9 ft	R0	2	2	1 ft	<0.5 in	6-8	0	49°	close
	2	47°	170°	2	2	3	9'	R0	2	2	2 ft	<0.5 in	6-8	0	80°	close
	2	50°	172°	2	2	3	9'	R0	2	2	2 ft	<0.5 in	6-8	0	82°	close
	2	81°	235°	1	1	5	2.7 ft	R0	1	2	2 ft	1.4	8-10	0	145°	close
	2	76°	60°	1	1	4	1	—	1	2	2 ft	1.4	8-10	0	150°	close
	2	84°	30°	1	1	4	1	—	2	2	2 ft	1.4	8-10	0	120°	close
	2	82°	74°	2	1	6	2.7 ft	R0	1	2	2 ft	1.4	4-6	0	164°	close
	2	90°	vertical	2	1	6	2.7 ft	R0	1	2	2 ft	1.4	4-6	0	170°	close

WATER FLOW (Q=6)
0. Discontinuity very light and dry, water flow doesn't appear possible
1. Discontinuity dry, no evidence of water flow
2. Discontinuity dry, shows evidence of water flow e.g. rust staining
3. Discontinuity is damp, but no free water present
4. Discontinuity shows seepage, occasional drops of water, no continuous flow
5. Continuous flow of water (Estimate l/min and describe pressure i.e. low medium high)

WATER FLOW (Filled)
6. Filling materials heavily consolidated and dry, significant flow unlikely due to very low permeability
7. Filling materials damp, no free water present
8. Filling material wet, occasional drops of water
9. Filling materials show signs of outwash, continuous flow of water (Estimate l/min)
10. Filling materials locally washed out, considerable water flow along outwash channels (Estimate l/min and describe pressure)

COMPRESSION STRENGTH OF INFILLING
PSI
44
47
7-15
15-35
35-70
>70
35-150
150-725
725-3,500
3,500-7,000
7,000-15,000
15,000-36,000
>36,000

NATURE OF FILLING
1. Clean
2. Surface staining
3. Non-cohesive
4. Inactive clay or clay matrix
5. Swelling clay or clay matrix
6. Cemented
7. Gypsum, talc or gypsum
8. Other - specify
9. calcite thin

APERTURE WIDTH
1. Very tight (<0.04 in)
2. Tight (0.04-0.1 in)
3. Partly Open (0.1-0.2 in)
4. Open (0.2-1 in)
5. Moderately Wide (1-4 in)
6. Wide (>4 in)
7. Very wide (4-4.4 in)
8. Extremely wide (4 in-3 ft)
9. Cavemous (>3 ft)

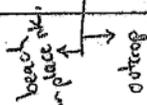
PERSISTENCE
1. Very Low (<3 ft)
2. Low (3-10 ft)
3. Medium (10-30 ft)
4. High (30-60 ft)
5. Very High (>60 ft)

TERMINATION
0. Neither end visible
1. One end visible
2. Both ends visible

SURFACE ROUGHNESS
1. Slickensided
2. Smooth
3. Rough

SURFACE SHAPE
1. Planar
2. Undulating
3. Stepped

JRC (Joint Roughness)
0. Slickensided, planar
5. Undulating
10. Smooth, undulating
15. Rough, stepped
20. Rough, stepped



Date: 8/27/2013
 Field Party: Karri Sicard, Ellie Spangler

ROCK MASS DESCRIPTION DATA SHEET
 Project Name: Yukon Crossing
 Project No: _____

State of Alaska DOT & PF
 Design & Engineering Services
 Statewide Materials



Weather: _____

GENERAL INFORMATION

Location: 730 to 800 West Station/Hole No. #7

Locality Type: _____ No. of Sheets of Discontinuity Data: _____

Slope Length: _____ Sketch: _____

Slope Height: _____ Photograph: _____

Core Size: _____

1. Natural Exposure
 2. Construction Excavation
 3. Trial Pit
 4. Trench
 5. Adit
 6. Tunnel
 7. Drill Hole

REMARKS (exposure type/lage, stability condition, design issues etc.)
Most of the rock examined at this station is located in the upper 1/4 of the slope.

ROCK MATERIAL INFORMATION

Color: 2 6 9 Grain Size: 4 Compressive Strength: A5 Method to Determine Compressive Strength: 2 Rock Type: Diorite to Gabbro (see thin section)

1. Light
 2. Dark

1. Pink
 2. Reddish
 3. Yellowish
 4. Brownish
 5. Olive
 6. Greenish
 7. Blue
 8. White
 9. Grey
 10. Black

1. Very coarse - boulders (>12 in)
 2. Coarse - cobbles (3-12 in)
 3. Medium - gravel (0.2-3 in)
 4. Fine - sand (0.003-0.2 in)
 5. Very fine - silt/clay (<0.003 in)

PSI
 <4
 4-7
 7-15
 15-35
 35-70
 >70
 35-150
 150-725
 725-3,500
 3,500-7,000
 7,000-15,000
 15,000-36,000
 >36,000

S1 Very soft clay
 S2 Soft clay
 S3 Firm clay
 S4 Stiff clay
 S5 Very stiff clay
 S6 Hard clay
 R0 Extremely weak rock
 R1 Very weak rock
 R2 Weak rock
 R3 Medium strong rock
 R4 Strong rock
 R5 Very strong rock
 R6 Extremely strong rock

Qualifying terms to describe rock:
 • Fine grained, phaneritic
 • Quartz, feldspar, biotite amphibole.
 • Some very coarse, quartz
 • Movement along these planes
 • Oxide staining

ROCK MASS INFORMATION

Fabric: 1 Block Size: 3 State of Weathering: 2

1. Blocky
 2. Tabular
 3. Columnar
 4. Shattered

1. Very large (>216ft³ or 6ft cube)
 2. Large (6-216ft³ or 2-6ft cube)
 3. Medium (0.3-7ft³ or 0.67-2ft cube)
 4. Small (12ft³-0.3ft³ or 2.3in to 0.67ft cube)
 5. Very small (<12ft³ or 2.3in cube)

1. Fresh
 2. Slight
 3. Moderate
 4. High
 5. Complete
 6. Residual Soil

Failure Mode: Jointing No. of Major Discontinuity Sets: 5
 e.g. Toppings, Wedges

LINE SURVEYS TO DETERMINE DISCONTINUITY SPACING (OR DRILL HOLE ORIENTATION)

Line	Plunge of line / hole	Trend of line / hole	Length of line (m)	No. of Fractures / True Spacing	Remarks / True Spacing
Line 1					
Line 2					
Line 3					

Discontinuity spacing:
 1. Extremely close (<1 in)
 2. Very close (1-2.5 in)
 3. Close (2.5 - 5 in)
 4. Moderate (5 in - 2 ft)
 5. Wide (2-6 ft)
 6. Very wide (6-20 ft)
 7. Extremely wide (>20 ft)

DISCONTINUITY SURVEY DATA SHEET

State of Alaska DOT & PF Design & Engineering Services Statewide Materials

Date: 8/27/13 Field Party: Ellie Spangler & Kam Seward Weather: Sunny ~ 55°F

Project Name: Yukon Crossing Project No:

Station/Hole No.: 77 of 1

NATURE AND ORIENTATION OF DISCONTINUITY

Table with columns: Station or Depth, Type, Dip, Direction, Persistence, Termination, Aperture/Width, Nature of Filling, Strength of Filling, Surface Roughness, Surface Shape, Waveiness, Waviness, Amplitude, Water Flow, Az, Specimen Remarks. Includes handwritten data for various discontinuity types and orientations.

Handwritten notes: Rake 51' down from N, 12, 505 1/2 steps. 1/2 rake, 1/2 fill w/ clay line. 1/2 rake, 1/2 fill w/ clay line.

Handwritten note: 1/2 rake, 1/2 fill w/ clay line. 1/2 rake, 1/2 fill w/ clay line.

GPS # NUG 52.445 W 149.43.764

Appendix A. Forms Effective October 1, 2003

A-3

Field Rock Classification And Structural Mapping Guide

Date: 8/27/13
 Field Party: Kerr, Sicaard, Ellie Spangale
 Weather: Chilly

ROCK MASS DESCRIPTION DATA SHEET

Project Name: YUKON CROSSING
 Project No: _____

Station/Hole No. #8

Location: 1000' N 05° 52.509' W, 43.527'

Locality Type: 1

No. of Sheets of Discontinuity Data: 1

Slope Length: _____

Slope Height: _____

Core Size: _____

Sketch: _____

Photograph: _____

REMARKS (exposure type/age, stability condition, design issues etc.):

ROCK MATERIAL INFORMATION

Color: 4 6 7 5

Grain Size: 5

Compressive Strength: 24 PSI

Method to Determine Compressive Strength: 2

Rock Type: Chert

Qualifying terms to describe rock:
 Alternating zones of maroon and blue green chert
 Bedding finely parallel to fracture joint set
 fractured at base
 10% of quartz veins left

1. Light
 2. Dark
 3. Pinkish
 4. Reddish
 5. Yellowish
 6. Brownish
 7. Olive
 8. Greenish
 9. Blue
 10. Black

1. Very coarse - boulders (>12 in)
 2. Coarse - cobbles (3-12 in)
 3. Medium - gravel (0.2-3 in)
 4. Fine - sand (0.003-0.2 in)
 5. Very fine - silt/clay (<0.003 in)

S1 Very soft clay
 S2 Soft clay
 S3 Firm clay
 S4 Stiff clay
 S5 Very stiff clay
 S6 Hard clay
 R0 Extremely weak rock
 R1 Very weak rock
 R2 Weak rock
 R3 Medium strong rock
 R4 Strong rock
 R5 Very strong rock
 R6 Extremely strong rock

ROCK MASS INFORMATION

Fabric: 4

Block Size: 5

State of Weathering: 2

No. of Major Discontinuity Sets: 2

Failure Mode: Jointing

e.g. Topping, Wedges

LINE SURVEYS TO DETERMINE DISCONTINUITY SPACING (OR DRILL HOLE ORIENTATION)

Line #	Plunge of line / hole	Trend of line / hole	Length of line (m)	No. of Fractures / Spacing	Remarks / Fracture Spacing
Line 1					
Line 2					
Line 3					

Discontinuity spacing:
 1. Extremely close (<1 in)
 2. Very close (1-2.5 in)
 3. Close (2.5 - 8 in)
 4. Moderate (8 in - 2 ft)
 5. Wide (2-6 ft)
 6. Very wide (6-20 ft)
 7. Extremely wide (>20 ft)

Date: 8/27/2013
 Field Party: Larry Sicard & Ellie Spangler
 Weather: cold

DISCONTINUITY SURVEY DATA SHEET

Project Name: Nikon crossing
 Project No.:



Station/Hole No.: 88 Discontinuity Data Sheet No.: 1 of 1

Location: 1000 West of bridge

NATURE AND ORIENTATION OF DISCONTINUITY

Station # or Depth	Type	Dip	Direction	Persistence	Termination	Aperture/Width	Nature of Filling	Strength of Filling	Surface Roughness	Surface Shape	Waviness Wavelength	Waviness Amplitude	JRC	Water Flow	Specific Remarks	
1	8	2	84	90 (E)	2	0	1	1	2	1	—	—	3	0	018	1
2	1	2	73	90 (E)	2	0	1	1	2	1	—	—	3	0	019	2
3	2	2	76	90 (E)	2	0	1	1	2	1	—	—	3	0	008	2
4	2	2	82	90 (E)	2	0	1	1	2	1	—	—	3	0	005	2
5	2	2	87	90 (E)	2	0	1	1	2	1	—	—	3	0	024	1
6	2	2	88	90 (E)	2	0	1	1	2	1	—	—	3	0	202	1
7	2	2	87	90 (E)	2	0	1	1	2	1	—	—	3	0	011	1
8	2	2	89	90 (E)	2	0	1	1	2	1	—	—	3	0	018	1
9	2	2	72	90 (E)	2	1	1	1	2	1	—	—	2	0	357	3
10	2	2	73	90 (E)	2	1	1	1	2	1	—	—	2	0	359	3
11	2	2	57	90 (E)	2	1	1	1	2	1	—	—	2	0	001	3
12	2	2	54	45 (NE)	2	1	1	1	2	1	—	—	2	0	325	3
13	2	2	60	45 (NE)	2	1	1	1	2	1	—	—	2	0	335	3
14	2	2	74	90 (E)	2	1	1	1	2	1	—	—	2	0	355	3
15	2	2	77	45 (NE)	2	1	1	1	2	1	—	—	2	0	340	3
16	2	2	72	90 (E)	2	1	1	1	2	1	—	—	2	0	001	3
17	2	2	84	0 (N)	1	2	1	1	2	1	—	—	2	0	000	2
18	2	2	85	0 (N)	1	2	1	1	2	1	—	—	2	0	279	2
19	2	2	81	180 (S)	1	2	1	1	2	1	—	—	2	0	123	2
20	2	2	89	225 (SW)	1	2	1	1	2	1	—	—	2	0	138	2

TERMINATION

- Neither end visible
- One end visible
- Both ends visible

SURFACE ROUGHNESS

- Slack-sided
- Smooth
- Rough

SURFACE SHAPE

- Planar
- Undulating
- Stepped

APERTURE/WIDTH

- Very tight (<0.04 ft)
- Tight (0.04-0.1 ft)
- Partly Open (0.1-0.3 ft)
- Open (0.3-1 ft)
- Moderately Wide (1-4 ft)
- Wide (>4 ft)
- Very wide (4-4 ft)
- Extremely wide (4 ft - 3 ft)
- Cavernous (> 3 ft)

NATURE OF FILLING

- Clean
- Surface staining
- Non-cohesive
- Inertive clay or clay matrix
- Swelling clay or clay matrix
- Combed
- Chlorite, talc or gypsum
- Other - specify

COMPRESSIVE STRENGTH OF INFILLING

PSI

- <4
- 4-7
- 7-15
- 15-35
- 35-70
- >70

R0 Extremely weak rock
 R1 Very weak rock
 R2 Weak rock
 R3 Medium strong rock
 R4 Strong rock
 R5 Very strong rock
 R6 Extremely strong rock

WATER FLOW (Open)

- Discontinuity very tight and dry, water flow doesn't appear possible due to very low permeability
- Discontinuity dry, no evidence of water flow
- Discontinuity is damp, but no free water present
- Discontinuity shows seepage, occasional drops of water, no continuous flow
- Continuous flow of water (Estimate flow and describe pressure i.e. low medium high)

WATER FLOW (Filled)

- Filling materials heavily consolidated and dry, significant flow unlikely due to very low permeability
- Filling materials damp, no free water present
- Filling material wet, occasional drops of water
- Filling materials show signs of outwash, continuous flow of water (Estimate flow)
- Filling materials locally washed out; considerable water flow along outwash channels (Estimate flow and describe pressure)



State of Alaska DOT & PF
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Statewide Materials

ROCK MASS DESCRIPTION DATA SHEET

Date: 8/27/2013

Project Name: Yukon Crossing

Field Party: Kari Sicard + Elie Spangler

Project No. _____

Weather: Sunny

GENERAL INFORMATION

REMARKS (exposure type/age, stability condition, design issues etc.)

Location: Station/Hole No. #9

Locality Type: 1 Slope Length: No. of Sheets of Discontinuity Data:

Slope Height: Sketch:

Core Size: Photograph:

1. Natural Exposure
2. Construction Excavation
3. Trial Pit
4. Trench
5. AdR
6. Tunnel
7. Drill Hole

ROCK MATERIAL INFORMATION

Color: 2, 3, 9 Grain Size: 5 Compressive Strength: 84 Method to Determine Compressive Strength: 2 Rock Type: meta basalt

1. Light
2. Dark

1. Pinkish
2. Reddish
3. Yellowish
4. Brownish
5. Olive
6. Greenish
7. Blue
8. Greyish
9. Grey
10. Black

1. Very coarse - boulders (>12 in)
2. Coarse - cobbles (3-12 in)
3. Medium - gravel (0.2-3 in)
4. Fine - sand (0.003-0.2 in)
5. Very fine - silt/clay (<0.003 in)

S1 Very soft clay
S2 Soft clay
S3 Firm clay
S4 Stiff clay
S5 Very stiff clay
S6 Hard clay
R0 Extremely weak rock
R1 Very weak rock
R2 Weak rock
R3 Medium strong rock
R4 Strong rock
R5 Very strong rock
R6 Extremely strong rock

PSI
4-47
7-16
15-35
35-70
>70
35-150
150-725
725-3,500
3,500-7,000
7,000-15,000
15,000-35,000
>35,000

Qualifying terms to describe rock
• Very fine grained
• Grey to green, some tan
• Very fractured
• Wax surfaces reorientation
• Off-z veins
• Deformed, glassy, calcy.

(Modifiable by fingers, but retains fabric)
(Hammer creates surface, sides pushed up)
(Hammer creates smooth dent)
(Hammer creates rough pit)
(Hammer rebounds)

ROCK MASS INFORMATION

Fabric: 1 Block Size: 3 State of Weathering: 2

1. Blocky
2. Tabular
3. Columnar
4. Shattered

1. Very large (>216ft³ or 6ft cube)
2. Large (8-216ft³ or 2-6ft cube)
3. Medium (0.3-7ft³ or 0.67-2ft cube)
4. Small (12ft³-0.3ft³ or 2.3ft to 0.67ft cube)
5. Very small (<12 in³ or 2.3ft cube)

1. Fresh
2. Slight
3. Moderate
4. High
5. Complete
6. Residual Soil

Failure Mode: Jointing No. of Major Discontinuity Sets: 2

e.g. Topping, Wedges

LINE SURVEYS TO DETERMINE DISCONTINUITY SPACING
(OR DRILL HOLE ORIENTATION)

Plunge of line / hole	Trend of line / hole	Length of line (m)	No. of Fractures	Spacing	Remarks / True Spacing
Line 1					
Line 2					
Line 3					

Discontinuity spacing

1. Extremely close (<1 in)
2. Very close (1-2.5 in)
3. Close (2.5 - 8 ft)
4. Moderate (8 in - 2 ft)
5. Wide (2-6 ft)
6. Very wide (6-20 ft)
7. Extremely wide (>20 ft)

Date: 8/27/2013
 Field Party: Yann Sicard & Elen Spangler
 Weather: Sunny

DISCONTINUITY SURVEY DATA SHEET

Project Name: Yukon Crosscut
 Project No.:

Station/Hole No.: # 1 of 1
 Discontinuity Data Sheet No.: 1 of 1

NATURE AND ORIENTATION OF DISCONTINUITY

Station or Depth	Type	Dip Direction	Dip	Persistence	Termination	Aperture/Width	Nature of Filling	Strength of Filling	Surface Roughness	Surface Shape	Waviness Wavelength	Waviness Amplitude	JRC	Water Flow	Remarks	Scale
1	2	50 180(S)	2	1	1	1	1	1	2	1	1	1	7	0	070	3
2	2	34 0(N)	2	1	1	1	1	1	2	1	1	1	7	0	270	3
3	2	30 15(N)	2	1	1	1	1	1	2	1	1	1	7	0	226	3
4	2	45 180(S)	2	1	1	1	1	1	2	1	1	1	7	0	061	3
5	2	80 0(N)	2	1	1	1	1	1	2	1	1	1	7	0	274	3
6	2	61 0(S)	2	1	1	1	1	1	2	1	1	1	7	0	058	3
7	2	10 0(S)	2	1	1	1	1	1	2	1	1	1	7	0	056	3
8	2	50 180(S)	2	1	1	1	1	1	2	1	1	1	7	0	055	3
9	2	48 0(N)	2	1	1	1	1	1	2	1	1	1	7	0	059	3
10	2	74 215(N)	2	1	1	1	1	1	3	1	1	1	13	0	230	3
11	2	12 180(S)	2	1	1	1	1	1	3	1	1	1	13	0	111	3
12	2	34 180(S)	2	1	1	1	1	1	3	1	1	1	13	0	104	3
13	2	50 180(S)	2	1	1	1	1	1	3	1	1	1	13	0	41	3
14	2	50 180(S)	2	1	1	1	1	1	3	1	1	1	13	0	121	3
15	2	53 0(N)	2	1	1	1	1	1	3	1	1	1	13	0	244	3
16	2	45 0(N)	2	1	1	1	1	1	3	1	1	1	13	0	202	3
17	2	51 225(S)	2	1	1	1	1	1	3	1	1	1	13	0	135	3
18	2	85 225(S)	2	1	1	1	1	1	3	1	1	1	13	0	121	3
19	2	76 90(E)	2	1	1	1	1	1	3	1	1	1	5	0	009	3
20	2	37 215(N)	2	1	1	1	1	1	2	1	1	1	9	0	235	3

WATER FLOW (Open)
 0. Discontinuity very tight and dry, water flow doesn't appear possible
 1. Discontinuity dry, no evidence of water flow
 2. Discontinuity dry, shows evidence of water flow e.g. rust staining
 3. Discontinuity is damp, but no free water present
 4. Discontinuity shows seepage, occasional drops of water, no continuous flow.
 5. Continuous flow of water (Estimate l/min and describe pressure i.e. low medium high)

WATER FLOW (Filled)
 6. Filling materials heavily consolidated and dry; significant flow unlikely due to very low permeability
 7. Filling materials damp, no free water present
 8. Filling materials wet, occasional drops of water
 9. Filling materials show signs of outwash, continuous flow of water (Estimate l/min)
 10. Filling materials locally washed out; considerable water flow along outwash channels (Estimate l/min and describe pressure)

COMPRESSION STRENGTH OF INFILLING
 PSI
 S1 Very soft clay <4
 S2 Soft clay 4-7
 S3 Firm clay 7-15
 S4 Stiff clay 15-35
 S5 Very stiff clay 35-70
 S6 Hard clay >70
 R0 Extremely weak rock 35-150
 R1 Very weak rock 150-725
 R2 Weak rock 725-3,500
 R3 Medium strong rock 3,500-7,000
 R4 Strong rock 7,000-15,000
 R5 Very strong rock 15,000-36,000
 R6 Extremely strong rock >36,000

NATURE OF FILLING
 1. Clean
 2. Surface staining
 3. Non-cohesive
 4. Inactive clay or clay matrix
 5. Swelling clay or clay matrix
 6. Cemented
 7. Chloride, talc or gypsum
 8. Other - specify

APERTURE/WIDTH
 1. Very tight (<0.04 in)
 2. Tight (0.04-0.1 in)
 3. Partly Open (0.1-0.2 in)
 4. Open (0.2-1 in)
 5. Moderately Wide (1-4 in)
 6. Wide (>4in)
 7. Very wide (4-4 in)
 8. Extremely wide (4 in-3 ft)
 9. Caveous (>3 ft)

PERSISTENCE
 1. Very Low (<3 ft)
 2. Low (3-10 ft)
 3. Medium (10-30 ft)
 4. High (30-60 ft)
 5. Very High (>60 ft)

SURFACE SHAPE
 1. Planar
 2. Undulating
 3. Stepped

SURFACE ROUGHNESS
 1. Slack-sticked
 2. Smooth
 3. Rough

TERMINATION
 0. Neither end visible
 1. One end visible
 2. Both ends visible

JRC (Joint Roughness)
 0 Slack-sticked, planar
 5
 10 Smooth, undulating
 15
 20 Rough, stepped

Page 1 Station 10

Date: 8/28/2013

Field Party: Karr, Sicard + Elvin Spangler

Weather: Mostly cloudy some sun

ROCK MASS DESCRIPTION DATA SHEET

Project Name: Yukon Crossing

Project No:

State of Alaska DOT & PF
Design & Engineering Services
Statewide Materials

waypoint 14 NUG 52.422' W. 144' 43.350'

GENERAL INFORMATION

Location: 300' to 250' E of bridge

Station/Hole No. #10

Locality Type: 1

No. of Sheets of Discontinuity Data: []

Slope Length: []

Sketch: []

Slope Height: []

Photograph: []

Core Size: []

REMARKS (exposure type/age, stability condition, design issues etc.):

ROCK MATERIAL INFORMATION

Color: 2 6 9

Grain Size: 5

Compressive Strength: 85

Method to Determine Compressive Strength: 2

Rock Type: Greenstone to talus salt

Qualifying terms to describe rock:
Fractured outcrop w/ qtz veins.
Fresh surfaces are greenish gray
qtz-epidote veins w/ slickenlines
tiny black veins, amphibole?

1. Light
2. Dark
3. Yellowish
4. Brown
5. Olive
6. Greenish
7. Bluish
8. Greyish
9. Grey
10. Black

1. Pink
2. Reddish
3. Yellow
4. Brown
5. Olive
6. Greenish
7. Bluish
8. White
9. Grey
10. Black

1. Very coarse - boulders (>12 in)
2. Coarse - cobbles (3-12 in)
3. Medium - gravel (0.2-3 in)
4. Fine - sand (0.003-0.2 in)
5. Very fine - silt/clay (<0.003 in)

SI Very soft clay
S2 Soft clay
S3 Firm clay
S4 Stiff clay
S5 Very stiff clay
S6 Hard clay
R0 Extremely weak rock
R1 Very weak rock
R2 Weak rock
R3 Medium strong rock
R4 Strong rock
R5 Very strong rock
R6 Extremely strong rock

4-1
4-7
7-15
15-35
35-70
>70
35-150
150-725
725-3,500
3,500-7,000
7,000-15,000
15,000-35,000
>35,000

ROCK MASS INFORMATION

Fabric: 1

Block Size: 3

State of Weathering: 2

No. of Major Discontinuity Sets: 4

Failure Mode: Jointing

e.g. Topping, Wedges

LINE SURVEYS TO DETERMINE DISCONTINUITY SPACING (OR DRILL HOLE ORIENTATION)

Line	Plunge of line / hole	Trend of line / hole	Length of line (m)	No. of Fractures	Spacing	Remarks / True Spacing
Line 1						
Line 2						
Line 3						

Discontinuity spacing:
1. Extremely close (<1 in)
2. Very close (1-2.5 in)
3. Close (2.5 - 8 in)
4. Moderate (8 in - 2 ft)
5. Wide (2-6 ft)
6. Very wide (6-20 ft)
7. Extremely wide (>20 ft)

DISCONTINUITY SURVEY DATA SHEET

State of Alaska DOT & PF
Design & Engineering Services
Statewide Materials

Project Name: YUKON RIVER CROSSING
Project No: _____

Date: 8/28/2013
Field Party: KARI SICARD, ELLIE SPANGLER
Weather: _____

GENERAL INFORMATION

Location: BARWEN 205 + 250 E Bridge Station/Hole No.: #10

Discontinuity Data Sheet No.: 1 of 2

NATURE AND ORIENTATION OF DISCONTINUITY

Station # or Depth	Type	Dip	Direction	Persistence	Termination	Aperture/Width	Nature of Filling	Strength of Filling	Surface Roughness	Surface Shape	Waviness Wavelength	Waviness Amplitude	JRC	Water Flow	Remarks	Staining
1	1	87	160 (S)	4	0	7	0	B2	3	3			15	0	Vertical strike slip fault. 50 ft N to top of fault. Vertical strike slip fault. Consists of sandy clayey mudstone.	2
2	2	74	180 (S)	1	2	1	1		2	1			3	0		2
3	2	74	180 (S)	1	2	1	1		2	1			3	0		2
4	2	78	180 (S)	1	2	1	1		2	1			3	0		2
5	2	88	180 (S)	1	2	1	1		2	1			3	0		2
6	2	84	0 (N)	1	2	1	1		2	1			3	0		2
7	2	87	140 (S)	1	2	1	1		2	1			3	0		2
8	2	89	160 (S)	1	2	1	1		2	1			3	0		2
9	2	43	0 (N)	2	1	1	2		2	1			3	0		2
10	2	40	0 (N)	2	1	1	2		2	1			3	0		2
11	2	39	0 (N)	2	1	1	2		2	1			3	0		2
12	2	40	0 (N)	2	1	1	2		2	1			3	0		2
13	2	58	0 (N)	2	1	1	2		2	1			3	0		2
14	2	37	0 (N)	2	1	1	2		2	1			3	0		2
15	2	51	0 (N)	2	1	1	2		2	1			3	0		2
16	2	40	0 (N)	2	1	1	2		2	1			3	0		2
17	2	54	0 (N)	2	1	1	2		2	1			3	0		2
18	2	72	0 (N)	2	1	1	2		2	1			3	0		2
19	2	49	0 (N)	2	1	1	2		2	1			3	0		2
20	2	74	0 (N)	2	1	1	2		2	1			3	0		2

WATER FLOW (Open)
 0. Discontinuity very tight and dry, water flow doesn't appear possible
 1. Discontinuity dry, no evidence of water flow
 2. Discontinuity dry, shows evidence of water flow e.g. rust staining
 3. Discontinuity is damp, but no free water present
 4. Discontinuity shows seepage, occasional drops of water, no continuous flow
 5. Continuous flow of water (Estimate flow and describe pressure i.e. low medium high)

WATER FLOW (Flood)
 6. Filling materials heavily consolidated and dry; significant flow unlikely due to very low permeability
 7. Filling materials damp, no free water present
 8. Filling materials wet, occasional drops of water
 9. Filling materials show signs of outwash, continuous flow of water (Estimate flow)
 10. Filling materials locally washed out; considerable water flow along outwash channels (Estimate flow and describe pressure)

COMPRESSIVE STRENGTH OF INFILLING
 PSI
 S1 Very soft clay 4
 S2 Soft clay 4-7
 S3 Firm clay 7-15
 S4 Stiff clay 15-35
 S5 Very stiff clay 35-70
 S6 Hard clay >70
 R0 Extremely weak rock 35-150
 R1 Very weak rock 150-725
 R2 Weak rock 725-3,500
 R3 Medium strong rock 3,500-7,000
 R4 Strong rock 7,000-15,000
 R5 Very strong rock 15,000-35,000
 R6 Extremely strong rock >35,000

NATURE OF FILLING
 1. Clean
 2. Sandstone staining
 3. Non-cohesive
 4. Inactive clay or clay matrix
 5. Swelling clay or clay matrix
 6. Cemented
 7. Chlorite, talc or gypsum
 8. Other - specify

APERTURE WIDTH
 1. Very tight (<0.04 in)
 2. Tight (0.04-0.1 in)
 3. Partly Open (0.1-0.2 in)
 4. Open (0.2-1 in)
 5. Moderately Wide (1-4 in)
 6. Wide (>4 in)
 7. Very wide (4-4 in)
 8. Extremely wide (4 in - 3 ft)
 9. Cavernous (> 3 ft)

PERSISTENCE
 1. Very Low (<3 ft)
 2. Low (3-10 ft)
 3. Medium (10-30 ft)
 4. High (30-60 ft)
 5. Very High (>60 ft)

SURFACE ROUGHNESS
 1. Smooth
 2. Smooth
 3. Rough

SURFACE SHAPE
 1. Planar
 2. Undulating
 3. Stepped

JRC (Joint Roughness)
 0. Slickensided, planar
 5
 10. Smooth, undulating
 15
 20. Rough, stepped

Page 2 Station 10

Date: 8/28/2013

Field Party: Kam Sillard + Ellen Spangler

Weather: Cloudy

ROCK MASS DESCRIPTION DATA SHEET

Project Name: Yukon River Crossing

Project No:

REMARKS (exposure type/age, stability condition, design issues etc.)

GENERAL INFORMATION

Location: 201 to 250' E of Indiff Station/Hole No. #10 continued

Locality Type: 1

Slope Length:

No. of Sheets of Discontinuity Data:

Slope Height:

Sketch:

Core Size:

Photograph:

1. Natural Exposure
2. Construction Excavation
3. Trial Pit
4. Trench
5. Adk
6. Tunnel
7. Drill Hole

ROCK MATERIAL INFORMATION

Color:

Grain Size:

Compressive Strength:

Method to Determine Compressive Strength:

Rock Type:

Qualifying terms to describe rock:

PSI

4-7
4-7
7-15
15-35
35-70
>70
35-150
150-725
725-3,500
3,500-7,000
7,000-15,000
15,000-36,000
>36,000

S1 Very soft clay
S2 Soft clay
S3 Firm clay
S4 Stiff clay
S5 Very stiff clay
S6 Hard clay
R0 Extremely weak rock
R1 Very weak rock
R2 Weak rock
R3 Medium strong rock
R4 Strong rock
R5 Very strong rock
R6 Extremely strong rock

(Measurable by fingers, but retains fabric)
(Hammer creates surface, sides pushed up)
(Hammer creates smooth dent)
(Hammer creates rough pit)
(Hammer rebounds)

LINE SURVEYS TO DETERMINE DISCONTINUITY SPACING (OR DRILL HOLE ORIENTATION)

ROCK MASS INFORMATION

Fabric:

Block Size:

State of Weathering:

No. of Major Discontinuity Sets:

Failure Mode:

e.g. Toppling, Wedges

Line	Plunge of line / hole	Trend of line / hole	Length of line (m)	No. of Fractures / True Spacing	Remarks / True Spacing
Line 1					
Line 2					
Line 3					

Discontinuity spacing

1. Extremely close (<1 in)
2. Very close (1-2.5 in)
3. Close (2.5 - 8 in)
4. Moderate (8 in - 2 ft)
5. Wide (2-6 ft)
6. Very wide (6-20 ft)
7. Extremely wide (>20 ft)

State of Alaska DOT & PF Design & Engineering Services Statewide Materials



Field Rock Classification and Structural Mapping Guide

A-2

DISCONTINUITY SURVEY DATA SHEET

State of Alaska DOT & PF Design & Engineering Services Statewide Materials

Date: 8/23/2013 Field Party: Kari Sicaud + Ellie Spangler Weather: Cloudy

Project Name: Yukon River Crossing Project No:

Location: Section 200 - 2 - 250 Station/Hole No.: #10 Contained Discontinuity Data Sheet No.: 2 of 2

NATURE AND ORIENTATION OF DISCONTINUITY

Table with columns: Station or Depth, Type, Dip, Direction, Persistence, Termination, Aperture/Width, Nature of Filling, Strength of Filling, Surface Roughness, Surface Shape, Waveiness Wavelength, Waveiness Amplitude, Water Flow, JRC, PSI, and Notes. Includes detailed handwritten data for 20 stations and various geological notes.

- APERTURE WIDTH, PERSISTENCE, SURFACE ROUGHNESS, SURFACE SHAPE, TERMINATION, WATER FLOW (FREQ), COMPRESSIVE STRENGTH OF INFILLING, NATURE OF FILLING, JRC (Joint Roughness), and other classification codes and descriptions.



State of Alaska DOT & PF
Design & Engineering Services
Statewide Materials

ROCK MASS DESCRIPTION DATA SHEET

Date: 8/28/2013
Field Party: Kari + Ellie
Weather: Cloudy, but warm

Project Name: Yukon Crossing

Project No:

waypoint 15 N 65° S 2.363
149° 43.287

GENERAL INFORMATION

Location: 650' E of bridge 025' + 475' Station/Hole No. #11

Locality Type: () No. of Sheets of Discontinuity Data: ()

Slope Length: () Sketch: ()

Slope Height: () Photograph: ()

Core Size: ()

1. Natural Exposure
2. Construction Excavation
3. Trial Pit
4. Trench
5. Adit
6. Tunnel
7. Drill Hole

REMARKS (exposure type/age, stability condition, design issues etc.)
Outcrop examined across W cliff at top of slope

ROCK MATERIAL INFORMATION

Color: 2 8 10 Grain Size: 4 Compressive Strength: AS Method to Determine Compressive Strength: 2 Rock Type: Gabbro

1. Light
2. Dark
3. Yellowish
4. Brownish
5. Olive
6. Greenish
7. Blue
8. White
9. Grey
10. Black

1. Very coarse - boulders (>12 in)
2. Coarse - cobbles (8-12 in)
3. Medium - gravel (0.2-3 in)
4. Fine - sand (0.003-0.2 in)
5. Very fine - silt/clay (<0.003 in)

S1 Very soft clay
S2 Soft clay
S3 Firm clay
S4 Stiff clay
S5 Very stiff clay
S6 Hard clay
R0 Extremely weak rock
R1 Very weak rock
R2 Weak rock
R3 Medium strong rock
R4 Strong rock
R5 Very strong rock
R6 Extremely strong rock

PSI
<4
4-7
7-15
15-35
35-70
>70
35-150
150-725
725-3,500
3,500-7,000
7,000-15,000
15,000-36,000
>36,000

Qualifying terms to describe rock:
Greenish black, fine grained gabbro, quartz veins, very fractured, trace black oxide on wk surfaces.
• Amphibole and plagioclase present
• Very diagenetic growth w/ submicron scale fibrous & trails.
• Scales color from tan to grey, resistant to weathering.

ROCK MASS INFORMATION

Fabric: 1 Block Size: 3 State of Weathering: 3

1. Blocky
2. Tabular
3. Columnar
4. Shattered

1. Very large (>216ft³ or 6ft cube)
2. Large (8-216ft³ or 2-6ft cube)
3. Medium (0.3-7ft³ or 0.67-2ft cube)
4. Small (12in³-0.3ft³ or 2.3in to 0.67ft cube)
5. Very small (<12 in³ or 2.3in cube)

1. Fresh
2. Slight
3. Moderate
4. High
5. Complete
6. Residual Soil

Failure Mode: Jointal No. of Major Discontinuity Sets: 3

e.g. Topping, Wedges

LINE SURVEYS TO DETERMINE DISCONTINUITY SPACING (OR DRILL HOLE ORIENTATION)

Line	Plunge of line / hole	Trend of line / hole	Length of line (m)	No. of Fractures	Spacing	Remarks / True Spacing
Line 1						
Line 2						
Line 3						

Discontinuity spacing:
1. Extremely close (<1 in)
2. Very close (1-2.5 in)
3. Close (2.5 - 8 in)
4. Moderate (8 in - 2 ft)
5. Wide (2-6 ft)
6. Very wide (6-20 ft)
7. Extremely wide (>20 ft)

DISCONTINUITY SURVEY DATA SHEET

State of Alaska DOT & PF Design & Engineering Services Statewide Materials

Date: 8/28/2013 Field Party: Kari Scard + Ellie Spangle Weather: Cloudy but warm-ish.

Project Name: Yukon Crossing Project No:

GENERAL INFORMATION Location: 6501, Highway 625+433 Station/Hole No.: # 11 Discontinuity Data Sheet No.: 1 of 1

NATURE AND ORIENTATION OF DISCONTINUITY

Table with columns: Station or Depth, Type, Dip, Direction, Persistence, Termination, Aperture/Width, Nature of Filling, Strength of Filling, Surface Roughness, Surface Shape, Waviness Wavelength, Waviness Amplitude, Water Flow, JRC, A2, Remarks, Spacing. Includes detailed data for 18 stations and various classification legends for PSI, FILLING, NATURE OF FILLING, APERTURE/WIDTH, SURFACE ROUGHNESS, SURFACE SHAPE, and TERMINATION.



State of Alaska DOT & PF
Design & Engineering Services
Statewide Materials

ROCK MASS DESCRIPTION DATA SHEET

Date: 8/28/2013
Field Party: Kami & Ellen
Weather: Sunny + cloudy

Project Name: Yukon crossing
Project No: 16. N 65° 52.338' W 149.43.223

REMARKS (exposure type/age, stability condition, design issues etc.)

GENERAL INFORMATION

Location: Near 850 E - between 550 + 900 Station/Hole No. #12

Locality Type: 1 Slope Length: No. of Sheets of Discontinuity Data:

1. Natural Exposure
2. Construction Excavation
3. Trial Pit
4. Trench
5. AUL
6. Tunnel
7. Drill Hole

Slope Height: Sketch:

Core Size: Photograph:

ROCK MATERIAL INFORMATION

Color: 2 Grain Size: 4 Compressive Strength: R5 Method to Determine Compressive Strength: 2 Rock Type: Diorite

1. Light
2. Dark

1. Pink
2. Reddish
3. Yellowish
4. Brownish
5. Olive
6. Greenish
7. Blue
8. Greyish
9. Grey
10. Black

1. Very coarse - boulders (>12 in)
2. Coarse - cobbles (3-12 in)
3. Medium - gravel (0.2-3 in)
4. Fine - sand (0.005-0.2 in)
5. Very fine - silt/clay (<0.005 in)

S1 Very soft clay
S2 Soft clay
S3 Firm clay
S4 Stiff clay
S5 Very stiff clay
S6 Hard clay
S7 Extremely weak rock
R0 Very weak rock
R1 Weak rock
R2 Medium strong rock
R3 Strong rock
R4 Very strong rock
R5 Extremely strong rock

PSI
<4
4-7
7-15
15-35
35-70
>70
35-150
150-725
725-3,500
3,500-7,000
7,000-15,000
15,000-35,000
>35,000

Qualifying terms to describe rock:
- Qtz, Feldspar, Amphibole
- fine-grained
- Qtz veins
- fractured (nearby)
- hypidiomorphic granular
- sub-hedral amphibole

1. Measured
2. Assessed

(Modifiable by fingers, but retains fabric)
(Hammer creates surface, sides pushed up)
(Hammer creates smooth dent)
(Hammer creates rough pit)
(Hammer rebounds)

ROCK MASS INFORMATION

Fabric: 1 Block Size: 4 State of Weathering:

1. Blocky
2. Tabular
3. Columnar
4. Shattered

1. Very large (>216ft³ or 6ft cube)
2. Large (8-216ft³ or 2-6ft cube)
3. Medium (0.3-7ft³ or 0.67-2ft cube)
4. Small (12in-0.3ft³ or 2.3in to 0.67ft cube)
5. Very small (<12 in³ or 2.3in cube)

1. Fresh
2. Slight
3. Moderate
4. High
5. Complete
6. Residual Soil

Failure Mode: Jointed No. of Major Discontinuity Sets: 3

e.g. Topping, Wedges

LINE SURVEYS TO DETERMINE DISCONTINUITY SPACING (OR DRILL HOLE ORIENTATION)

Line	Plunge of line / hole	Length of line (m)	No. of Fractures	Spacing	Remarks / True Spacing
Line 1					
Line 2					
Line 3					

Discontinuity spacing

1. Extremely close (<1 in)
2. Very close (1-2.5 in)
3. Close (2.5 - 8 in)
4. Moderate (8 in - 2 ft)
5. Wide (2-8 ft)
6. Very wide (6-20 ft)
7. Extremely wide (>20 ft)

Date: 8/28/2013
Field Party: Karri S. rated.
Weather: Cloudy

DISCONTINUITY SURVEY DATA SHEET

Project Name: Yukon Crossing
Project No:

GENERAL INFORMATION

Location: 850 - Barton 850+900'

Station/Hole No.: #12

Discontinuity Data Sheet No.: 1 of 1

NATURE AND ORIENTATION OF DISCONTINUITY

Station # or Depth	Type	Dip	Direction	Persistence	Termination	Aperture/Width	Nature of Filling	Strength of Filling	Surface Roughness	Surface Shape	Waviness Wavelength	Waviness Amplitude	JRC	Water Flow	Az	Remarks
1	2	68	315(NW)	2	1	1	1	1	2	1	1	1	11	0	209	Seepage
2	2	63	0(N)	2	1	1	1	1	2	1	1	1	11	6	212	1
3	2	63	315(NW)	2	1	1	1	1	2	1	1	1	11	0	204	3
4	2	84	270(W)	2	1	1	1	1	2	1	1	1	11	0	225	3
5	2	31	180(S)	2	1	1	1	1	2	1	1	1	11	0	100	3
6	2	41	0(N)	2	1	1	1	1	2	1	1	1	11	0	201	3
7	2	76	0(N)	2	1	1	1	1	2	1	1	1	11	0	266	3
8	2	35	0(N)	2	1	1	1	1	2	1	1	1	11	0	237	3
9	2	30	315(NW)	2	1	1	1	1	2	1	1	1	11	0	120	3
10	2	73	0(N)	2	1	1	1	1	2	1	1	1	11	0	313	3
11	2	84	180(S)	2	1	1	1	1	2	1	1	1	11	0	147	3
12	2	88	180(S)	2	1	1	1	1	2	1	1	1	11	0	135	3
13	2	87	0(N)	2	1	1	1	1	2	1	1	1	11	0	250	3
14	2	101	0(N)	2	1	1	1	1	2	1	1	1	11	0	264	Plane of 42° dip from 8°
15	2	89	180(S)	2	1	1	1	1	2	1	1	1	11	0	167	3
16	2	47	315(NW)	2	1	1	1	1	2	1	1	1	11	0	224	3
17	2	50	315(NW)	2	1	1	1	1	2	1	1	1	11	0	220	3
18	2	22	180(S)	2	1	1	1	1	2	1	1	1	11	0	086	134° 80° 8° 2
19	2	47	270(W)	2	1	1	1	1	2	1	1	1	11	0	195	Plane 50° down to ME
20	2	77	180(S)	2	1	1	1	1	2	1	1	1	11	0	070	Plane

TYPE	PERFORMANCE	APERTURE/WIDTH	NATURE OF FILLING	COMPRESSIVE STRENGTH OF INFILLING	WATER FLOW (Open)
0. Fault Zone	1. Very Low (<5 ft)	1. Very tight (<0.04 in)	1. Clean	S1 Very soft clay	0. Discontinuity very tight and dry, water flow doesn't appear possible
1. Fault	2. Low (5-10 ft)	2. Tight (0.04-0.1 in)	2. Surface staining	S2 Soft clay	1. Discontinuity dry, no evidence of water flow
2. Joint	3. Medium (10-30 ft)	3. Partly Open (0.1-0.2 in)	3. Non-cohesive	S3 Firm clay	2. Discontinuity dry, shows evidence of water flow e.g. rust staining
3. Cleavage	4. High (30-60 ft)	4. Open (0.2-1 in)	4. Incohesive clay or clay matrix	S4 Silty clay	3. Discontinuity is damp, but no free water present
4. Schistosity	5. Very High (>60 ft)	5. Moderately Wide (1-4 in)	5. Swelling clay or clay matrix	S5 Very stiff clay	4. Discontinuity shows seepage, occasional drops of water, no continuous flow
5. Shear		6. Wide (>4 in)	6. Cemented	S6 Hard clay	5. Continuous flow of water (Estimate flow and describe pressure i.e. low medium high)
6. Fracture		7. Very wide (4-4 in)	7. Chlorite, talc or gypsum	R0 Extremely weak rock	6. Filling materials heavily consolidated and dry; significant flow unlikely due to very low permeability
7. Tension Crack		8. Extremely wide (4 in-3 ft)	8. Other - specify	R1 Very weak rock	7. Filling materials damp, no free water present
8. Foliation		9. Cavernous (> 3 ft)		R2 Medium strong rock	8. Filling materials wet, occasional drops of water
9. Bedding				R3 Strong rock	9. Filling materials show signs of outwash, continuous flow of water (Estimate flow)
TERMINATION				R4 Very strong rock	10. Filling materials locally washed out; considerable water flow along outwash channels (Estimate flow and describe pressure)
0. Neither end visible				R5 Extremely strong rock	
1. One end visible					
2. Both ends visible					

Sheet: Station 13

State of Alaska DOT & PF
Design & Engineering Services
Statewide Materials

ROCK MASS DESCRIPTION DATA SHEET

Date: 8/29/13
Field Party: Kamin Sicaud

Project Name: Yukon Crossing

Weather:

Project No:

GENERAL INFORMATION

Location: Station 13 Station/Note No. 13 No. of Sheets of Discontinuity Data: 1

Locality Type: 1 Slope Length: Sketch: Photograph: Slope Height: Core Size: Core Size: Photograph: Photograph:

1. Natural Exposure 2. Construction Excavation 3. Tidal Pit 4. Trench 5. A/R 6. Tunnel 7. Drill Hole

REMARKS (exposure type/age, stability condition, design issues etc.)
At point (bedrock) west of bridge

ROCK MATERIAL INFORMATION

Color: 2 6 10 Grain Size: 4 Compressive Strength: RS Method to Determine Compressive Strength: 2 Rock Type: meta basalt greenstone

1. Light 2. Dark 1. Pink 2. Reddish 3. Yellowish 4. Brownish 5. Olive 6. Greenish 7. Blue 8. Greyish 9. Grey 10. Black

1. Very coarse - boulders (>12 in)
2. Coarse - cobbles (5-12 in)
3. Medium - gravel (0.2-3 in)
4. Fine - sand (0.003-0.2 in)
5. Very fine - silt/clay (<0.003 in)

S1 Very soft clay S2 Soft clay S3 Firm clay S4 Stiff clay S5 Very stiff clay S6 Hard clay S7 Extremely weak rock S8 Extremely weak rock S9 Very weak rock R1 Weak rock R2 Medium strong rock R3 Strong rock R4 Very strong rock R5 Extremely strong rock

Qualifying terms to describe rock:
1. Measured 2. Assessed
(Measurable by fingers, but retains fabric)
(Hammer creates surface, sides pushed up)
(Hammer creates smooth dent)
(Hammer creates rough pit)
(Hammer rebounds)

ROCK MASS INFORMATION

Fabric: 1 Block Size: H State of Weathering: 2 No. of Major Discontinuity Sets: 4

1. Blocky 2. Tabular 3. Columnar 4. Shattered 1. Fresh 2. Slight 3. Moderate 4. High 5. Complete 6. Residual Soil

Failure Mode: jointing e.g. Topping, Wedges

LINE SURVEYS TO DETERMINE DISCONTINUITY SPACING (OR DRILL HOLE ORIENTATION)

Line	Plunge of line / hole	Trend of line / hole	Length of line (m)	No. of Fractures Spacing	Remnants / True Spacing
Line 1					
Line 2					
Line 3					

Discontinuity spacing:
1. Extremely close (<1 in)
2. Very close (1-2.5 in)
3. Close (2.5 - 8 in)
4. Moderate (8 in - 2 ft)
5. Wide (2-6 ft)
6. Very wide (6-20 ft)
7. Extremely wide (>20 ft)

Sheet 2 Station 13
DISCONTINUITY SURVEY DATA SHEET
 Project Name: Yukon Crossing
 Project No:

State of Alaska DOT & PF
 Design & Engineering Services
 Statewide Materials

Date: 8/29/13
 Field Party: Karri Seward
 Weather: overcast ~ 55°F

Location: VV2-#18 - GFS Station/Hole No.: #13 continued Discontinuity Data Sheet No.: 1 of 2

NATURE AND ORIENTATION OF DISCONTINUITY

Station or Depth	Type	Dip	Dip Direction	Persistence	Termination	Aperture/Width	Nature of Filling	Strength of Filling	Surface Roughness	Surface Shape	Wavelength	Waviness Amplitude	JRC	Water Flow	Remarks	
13	1	89	E	2	1	.6	8 Ep	R4	1	3	—	—	9	0	015	spacing oblique rate of 40 dft/yr overp. by 88 dft/yr not in overp.
	1	86	W	2	1	.6	8 Ep	R4	3	2	8"	.5"	9	0	182	
	1	83	W	2	1	.6	8 Ep	R4	3	2	8"	.5"	9	0	183	
	1	83	E	2	1	.6	8 Ep	R4	3	2	8"	.5"	9	0	355	
	1	82	E	2	1	.6	8 Ep	R4	3	2	8"	.5"	9	0	354	
	1	88	E	2	1	.6	8 Ep	R4	3	2	8"	.5"	9	0	354	
	1	86	SE	2	1	.6	8 Ep	R4	3	2	8"	.5"	9	0	341	
	2	68	NE	2	1	1	2	—	2	1	—	—	3	0	038	
	2	74	NE	2	1	1	2	—	2	1	—	—	3	0	331	
	2	70	NE	2	1	1	2	—	2	2	16"	1"	3	0	328	
	2	84	E	2	1	1	2	—	2	2	16"	1"	3	0	328	
	2	87	W	2	1	1	2	—	2	2	16"	1"	3	0	016	
	2	86	E	2	1	1	2	—	2	2	16"	1"	3	0	160	
	2	27	SE	2	1	1	1	—	3	1	—	—	15	0	025	
	2	53	E	2	1	1	1	—	3	1	—	—	17	0	064	
	2	25	S	2	1	1	1	—	3	2	—	—	15	0	013	
	2	70	SE	1	2	1	2	—	2	1	—	—	3	0	111	
	2	40	SE	1	2	1	2	—	2	1	—	—	3	0	062	
	2	76	NE	1	2	1	2	—	2	1	—	—	3	0	310	
	2	76	S	1	2	1	2	—	2	1	—	—	3	0	115	

TERMINATION
 0. Neither end visible
 1. One end visible
 2. Both ends visible

APERTURE/WIDTH
 1. Very tight (<0.04 in)
 2. Tight (0.04-0.1 in)
 3. Partly Open (0.1-0.2 in)
 4. Open (0.2-1 in)
 5. Moderately Wide (1-4 in)
 6. Wide (>4 in)
 7. Very wide (4-4 in)
 8. Extremely wide (4 in - 3 ft)
 9. Cavernous (> 3 ft)

PERSISTENCE
 1. Very Low (<3 ft)
 2. Low (3-10 ft)
 3. Medium (10-30 ft)
 4. High (30-60 ft)
 5. Very High (>60 ft)

NATURE OF FILLING
 1. Clean
 2. Surface staining
 3. Non-cohesive
 4. Inactive clay or clay matrix
 5. Swelling clay or clay matrix
 6. Cemented
 7. Chlorite, talc or gypsum
 8. Other - specify

COMPRESSIVE STRENGTH OF INFILLING
 S1 Very soft clay
 S2 Soft clay
 S3 Firm clay
 S4 Stiff clay
 S5 Very stiff clay
 S6 Hard clay
 R0 Extremely weak rock
 R1 Very weak rock
 R2 Weak rock
 R3 Medium strong rock
 R4 Strong rock
 R5 Very strong rock
 R6 Extremely strong rock

PSI
 <4
 4-7
 7-15
 15-35
 35-70
 >70

WATER FLOW (Open)
 0. Discontinuity very tight and dry, water flow doesn't appear possible
 1. Discontinuity dry, no evidence of water flow
 2. Discontinuity dry, shows evidence of water flow e.g. rust staining
 3. Discontinuity is damp, but no free water present
 4. Discontinuity shows seepage, occasional drops of water, no continuous flow
 5. Continuous flow of water (Estimate l/min and describe pressure i.e. low medium high)

WATER FLOW (Filled)
 6. Filling materials heavily consolidated and dry, significant flow unlikely due to very low permeability
 7. Filling materials damp, no free water present
 8. Filling materials wet, occasional drops of water
 9. Filling materials show signs of outwash, continuous flow of water (Estimate l/min)
 10. Filling materials locally washed out; considerable water flow along outwash channels (Estimate l/min and describe pressure)

Sheet 3 Station 13
DISCONTINUITY SURVEY DATA SHEET
 Project Name: Yukon Crossing
 Project No:

State of Alaska DOT & PF
 Design & Engineering Services
 Statewide Materials

Date: 8/29/13
 Field Party: Kari Sicard
 Weather: overcast ~55°F

Location: WPT # 18 - GPS Station/Note No.: # 13 Discontinuity Data Sheet No.: 2 of 2

NATURE AND ORIENTATION OF DISCONTINUITY

Station or Depth	Type	Dip	Dip Direction	Persistence	Termination	Aperture/Width	Nature of Filling	Strength of Filling	Surface Roughness	Surface Shape	Waviness Wavelength	Waviness Amplitude	JRC	Water Flow	Az	Remarks
13	2	82	S	1	2	1	-2	—	2	2	8"	5"	3	0	085	
	2	58	NE	1	2	1	2	—	2	2	—	—	3	0	320	
	2	55	NW	1	2	1	1	—	2	1	—	—	3	0	215	
	2	47	NW	1	2	1	1	—	2	1	—	—	3	0	215	
	2	58	W	1	2	1	1	—	2	1	—	—	3	0	198	
	2	45	W	1	2	1	1	—	2	1	—	—	3	0	197	
	2	45	W	1	2	1	1	—	2	1	—	—	3	0	200	

GENERAL INFORMATION

PERFORMANCE
 1. Very Low (<3 ft)
 2. Low (3-10 ft)
 3. Medium (10-30 ft)
 4. High (30-60 ft)
 5. Very High (>60 ft)

APERTURE/WIDTH
 1. Very tight (<.004 in)
 2. Tight (.004-.01 in)
 3. Partly Open (.01-.02 in)
 4. Open (.02-.1 in)
 5. Moderately Wide (.1-.4 in)
 6. Wide (>.4in)
 7. Very wide (.4-.4 in)
 8. Extremely wide (.4 in - 3 ft)
 9. Cavemous (> 3 ft)

NATURE OF FILLING
 1. Clean
 2. Surface staining
 3. Non-cohesive
 4. Inactive clay or clay matrix
 5. Swelling clay or clay matrix
 6. Cemented
 7. Chlorite, talc or gypsum
 8. Other - specify

COMPRESSION STRENGTH OF INFILLING
 PSI
 <4
 4-7
 7-15
 15-35
 35-70
 >70

WATER FLOW (Open)
 0. Discontinuity very tight and dry, water flow doesn't appear possible
 1. Discontinuity dry, no evidence of water flow
 2. Discontinuity dry, shows evidence of water flow e.g. rust staining
 3. Discontinuity is damp, but no free water present
 4. Discontinuity shows seepage, occasional drops of water, no continuous flow.
 5. Continuous flow of water (Estimate l/min and describe pressure i.e. low medium high)

WATER FLOW (Filled)
 6. Filling materials heavily consolidated and dry, significant flow unlikely due to very low permeability
 7. Filling materials damp, no free water present
 8. Filling material wet, occasional drops of water
 9. Filling materials show signs of outwash, continuous flow of water (Estimate l/min)
 10. Filling materials locally washed out, considerable water flow along outwash channels (Estimate l/min and describe pressure)

TERMINATION
 0. Neither end visible
 1. One end visible
 2. Both ends visible

SURFACE ROUGHNESS
 1. Planar
 2. Undulating
 3. Stepped

SURFACE SHAPE
 1. Planar
 2. Undulating
 3. Stepped

JRC (Joint Roughness)
 0. Slickensided, planar
 5. Slightly rough
 10. Smooth, undulating
 15. Rough, stepped
 20. Rough, stepped

COMPRESSION STRENGTH OF INFILLING
 S1 Very soft clay
 S2 Soft clay
 S3 Firm clay
 S4 Stiff clay
 S5 Very stiff clay
 S6 Hard clay
 R0 Extremely weak rock
 R1 Very weak rock
 R2 Weak rock
 R3 Medium strong rock
 R4 Strong rock
 R5 Very strong rock
 R6 Extremely strong rock